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# PERFORMANCE EVALUATION OF NEW JERSEY'S PORTABLE CONCRETE BARRIER WITH A TRAFFIC-SIDE PINNED CONFIGURATION AND GROUTED TOES – TEST NO. NJPCB-7

Submitted by

Surajkumar K. Bhakta, M.S.M.E. Former Graduate Research Assistant Karla A. Lechtenberg, M.S.M.E., E.I.T. Research Engineer

Ronald K. Faller, Ph.D., P.E. Research Professor MwRSF Director John D. Reid, Ph.D. Professor

Robert W. Bielenberg, M.S.M.E., E.I.T. Research Engineer Erin L. Urbank, B.A. Research Communication Specialist

# MIDWEST ROADSIDE SAFETY FACILITY

Nebraska Transportation Center University of Nebraska-Lincoln

Main Office

Prem S. Paul Research Center at Whittier School Room 130, 2200 Vine Street Lincoln, Nebraska 68583-0853 (402) 472-0965 **Outdoor Test Site** 4630 N.W. 36<sup>th</sup> Street Lincoln, Nebraska 68524

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| <ul> <li>Prepared in cooperation with U.S. Department of Transportation, Federal Highway Administration.</li> <li>16. Abstract <ul> <li>This report documents a full-scale crash test conducted in support of a study to investigate the performance of New Jersey Department of Transportation's (NJDOT) Precast Concrete Curb, Construction Barrier, which will be referred to as portable concrete barrier (PCB) in various configurations. This represents the seventh system as part of this study.</li> <li>The primary objective of this research effort was to evaluate the safety performance of the NJDOT PCB, Type 4 (Alternative B) with a traffic-side pinned configuration and grouted toes. Barrier nos. 1 and 10 were anchored on both sides, and barrier nos. 2 through 9 were anchored only to the concrete tarmac through the traffic-side pin anchor recesses with 1-in. (25-mm) diameter by 15-in. (381-mm) long, ASTM A36 steel pins inserted into 1¼-in. (32-mm) diameter holes drilled in the concrete tarmac. Non-shrink grout wedges were placed at the toe of each barrier segment in every joint between adjacent barrier segments. The barrier was evaluated according to the Test Level 3 (TL-3) criteria set forth in the <i>Manual for Assessing Safety Hardware, Second Edition</i> (MASH 2016). The research study included one full-scale vehicle crash test with a 2270P pickup truck. Following the successful redirection of the pickup truck, the safety performance of the system was determined to be acceptable according to the test designation no. 3-11 evaluation criteria specified in MASH 2016. TL-3 criteria. This report set was deemed unnecessary due to previous testing. The barrier successfully met MASH 2016 TL-3 criteria. This report is the seventh of nine documents in the nine-test series.</li> </ul> </li> </ul> |                     |                 |  |  |  |
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#### UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

## INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority (IAA) for the data contained herein was Dr. Jennifer Schmidt, Research Assistant Professor.

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## Midwest Roadside Safety Facility

J.C. Holloway, M.S.C.E., E.I.T., Assistant Director – Physical Testing Division
J.D. Schmidt, Ph.D., P.E., Research Assistant Professor
C.S. Stolle, Ph.D., Research Assistant Professor
S.K. Rosenbaugh, M.S.C.E., E.I.T., Research Engineer
M. Asadollahi Pajouh, Ph.D., former Post-Doctoral Research Associate
S.A. Ranjha, Ph.D., former Post-Doctoral Research Associate
A.T. Russell, B.S.B.A., Testing and Maintenance Technician II
E.W. Krier, B.S., Construction and Testing Technician II
S.M. Tighe, Construction and Testing Technician I
D.S. Charroin, Construction and Testing Technician I
M.A. Rasmussen, Construction and Testing Technician I
M.T. Ramel, B.S.C.M., former Construction and Testing Technician I
J.E. Kohtz, B.S.M.E., CAD Technician
Undergraduate and Graduate Research Assistants

# New Jersey Department of Transportation

Dave Bizuga, former Senior Executive Manager, Roadway Design Group 1 Giri Venkiteela, Research Project Manager, NJDOT Bureau of Research Hung Tang, Design Standards Bureau, Roadway Standards Unit Lee Steiner, Project Engineer, Bureau of Traffic Engineering

# **TABLE OF CONTENTS**

| TECHNICAL REPORT DOCUMENTATION PAGE  | i                                |
|--|----------------------------------|
| DISCLAIMER STATEMENT   | ii                               |
| UNCERTAINTY OF MEASUREMENT STATEMENT   | ii                               |
| INDEPENDENT APPROVING AUTHORITY  | ii                               |
| ACKNOWLEDGEMENTS   | iii                              |
| TABLE OF CONTENTS  | iv                               |
| LIST OF FIGURES  | vi                               |
| LIST OF TABLES   | ix                               |
| 1 INTRODUCTION<br>1.1 Background<br>1.2 Objective<br>1.3 Scope   |                                  |
| 2 TEST REQUIREMENTS AND EVALUATION CRITERIA<br>2.1 Test Requirements<br>2.2 Evaluation Criteria                      |                                  |
| 3 DESIGN DETAILS   | 6                                |
| <ul> <li>4 TEST CONDITIONS</li></ul>   | 25<br>25<br>25<br>25<br>29<br>29 |
| <ul> <li>4.5.1 Accelerometers</li></ul>  |                                  |
| <ul><li>4.5.1 Accelerometers</li><li>4.5.2 Rate Transducers</li><li>4.5.3 Retroreflective Optic Speed Trap</li></ul> | 29<br>                           |

| 7 COMPARISON TO TEST NO. NYTCB-5 |  |  |  |  |
|----------------------------------|--|--|--|--|
| 8 MASH IMPLEME                   | NTATION                                      |  |  |  |
| 9 REFERENCES                     |  |  |  |  |
| 10 APPENDICES                    |  |  |  |  |
| Appendix A.                      | NJDOT PCB Standard Plans                     |  |  |  |
|                                  | Material Specifications                      |  |  |  |
| Appendix C.                      | Concrete Tarmac Strength                     |  |  |  |
| Appendix D.                      | Vehicle Center of Gravity Determination      |  |  |  |
| Appendix E.                      | Vehicle Deformation Records                  |  |  |  |
| Appendix F.                      | Accelerometer and Rate Transducer Data Plots |  |  |  |

# LIST OF FIGURES

| Figure 1. Test Installation Layout, Test No. NJPCB-7                                 | 7  |
|--|----|
| Figure 2. PCB Pin Anchor Details, Test No. NJPCB-7                                   |    |
| Figure 3. PCB Pin Anchor Locations, Test No. NJPCB-7                                 |    |
| Figure 4. PCB Details, Test No. NJPCB-7  | 10 |
| Figure 5. PCB Reinforcement Details, Test No. NJPCB-7                                | 11 |
| Figure 6. PCB Reinforcement Details - End View, Test No. NJPCB-7                     | 12 |
| Figure 7. PCB Connection Key Assembly Details, Test No. NJPCB-7                      |    |
| Figure 8. PCB Connection Key Component Details, Test No. NJPCB-7                     | 14 |
| Figure 9. PCB Connection Socket Details, Test No. NJPCB-7                            | 15 |
| Figure 10. PCB Connection Socket Component Details, Test No. NJPCB-7                 | 16 |
| Figure 11. Connection Key Placement Details, Test No. NJPCB-7                        | 17 |
| Figure 12. PCB Reinforcement Details, Test No. NJPCB-7                               | 18 |
| Figure 13. General Notes, Test No. NJPCB-7   |    |
| Figure 14. Bill of Materials, Test No. NJPCB-7                                       | 20 |
| Figure 15. NJDOT PCB with Traffic-Side Pinned Configuration and Grouted Toes Test    |    |
| Installation, Test No. NJPCB-7   |    |
| Figure 16. PCB Connection Key and Connection Socket, Test No. NJPCB-7                | 22 |
| Figure 17. PCB Traffic-Side Pin Anchor Recesses, Test No. NJPCB-7                    |    |
| Figure 18. Grout at Toes between PCBs, Test No. NJPCB-7                              | 24 |
| Figure 19. Test Vehicle, Test No. NJPCB-7  |    |
| Figure 20. Vehicle Dimensions, Test No. NJPCB-7                                      | 27 |
| Figure 21. Target Geometry, Test No. NJPCB-7   | 28 |
| Figure 22. Camera Locations, Speeds, and Lens Settings, Test No. NJPCB-7             | 31 |
| Figure 23. Permanent Set Deflection, Dynamic Deflection, and Working Width, Test No. |    |
| NJPCB-7  |    |
| Figure 24. Summary of Test Results and Sequential Photographs, Test No. NJPCB-7      | 38 |
| Figure 25. Additional Sequential Photographs, Test No. NJPCB-7                       |    |
| Figure 26. Additional Sequential Photographs, Test No. NJPCB-7                       |    |
| Figure 27. Documentary Photographs, Test No. NJPCB-7                                 |    |
| Figure 28. Documentary Photographs, Test No. NJPCB-7                                 | 42 |
| Figure 29. Documentary Photographs, Test No. NJPCB-7                                 |    |
| Figure 30. Documentary Photographs, Test No. NJPCB-7                                 |    |
| Figure 31. Impact Location, Test No. NJPCB-7   |    |
| Figure 32. Vehicle Final Position and Trajectory Marks, Test No. NJPCB-7             | 46 |
| Figure 33. System Damage – Front, Back, Upstream and Downstream Views, Test No.      |    |
| NJPCB-7  |    |
| Figure 34. Barrier No. 3 – Traffic and Back Side Damage, Test No. NJPCB-7            |    |
| Figure 35. Barrier Nos. 4 and 5 Damage, Test No. NJPCB-7                             |    |
| Figure 36. Barrier No. 4 – Traffic and Back Side Damage, Test No. NJPCB-7            |    |
| Figure 37. Barrier No. 5 - Traffic and Back Side Damage, Test No. NJPCB-7            |    |
| Figure 38. Barrier No. 6 – Traffic and Back Side Damage, Test No. NJPCB-7            |    |
| Figure 39. Vehicle Damage, Test No. NJPCB-7  |    |
| Figure 40. Vehicle Damage on Impact Side, Test No. NJPCB-7                           |    |
| Figure 41. Vehicle Windshield Damage, Test No. NJPCB-7                               |    |
| Figure 42. Occupant Compartment Deformation, Test No. NJPCB-7                        |    |

| Figure 43. Undercarriage Damage, Test No. NJPCB-7  | 57       |
|--|----------|
| Figure 44. Deflection Comparisons – Test Nos. NJPCB-7, NJPCB-6 and NYTCB-5   |          |
| Figure A-1. NJDOT PCB Standard Plans   |          |
| Figure A-2. NJDOT PCB Standard Plans   |          |
| Figure A-3. NJDOT PCB Standard Plans   |          |
| Figure A-4. NJDOT PCB Standard Plans   |          |
| Figure A-5. NJDOT PCB Standard Plans   | 13<br>76 |
| Figure B-2. Concrete Barrier Segment – Concrete Strength, Test No. NJPCB-7<br>Figure B-3. Anchor Pins Material Certificate, Test No. NJPCB-7   |          |
| Figure B-3. Alchor Phils Material Certificate, Test No. NJPCB-7  |          |
| Figure B-5. Rebar No. 4 Material Certificate, Test No. NJPCB-7   |          |
| Figure B-6. Rebar No. 4 Material Certificate, Test No. NJPCB-7   |          |
| Figure B-7. Rebar No. 6 Material Certificate, Test No. NJPCB-7   |          |
| Figure B-8. Rebar No. 6 Material Certificate, Test No. NJPCB-7   | 82       |
| Figure B-9. Rebar No. 6 Material Certificate, Test No. NJPCB-7   |          |
| Figure B-10. Rebar No. 6 Material Certificate, Test No. NJPCB-7  |          |
| Figure B-11. Rebar No. 6 Material Certificate, Test No. NJPCB-7  |          |
| Figure B-12. Steel Tube Material Certificate, Test No. NJPCB-7   |          |
| Figure B-13. Steel Tube Material Certificate, Test No. NJPCB-7   |          |
| Figure B-14. 2-in. × <sup>1</sup> / <sub>4</sub> -in. (51-mm × 6-mm) Bent Steel Plate, Test No. NJPCB-7  |          |
| Figure B-15. <sup>1</sup> / <sub>2</sub> -in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7                                 |          |
| Figure B-16. <sup>1</sup> / <sub>2</sub> -in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7                                 |          |
| Figure B-17. <sup>1</sup> / <sub>2</sub> -in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7                                 |          |
| Figure B-18. Non-Shrink Grout Specifications, Test No. NJPCB-7   |          |
| Figure B-19. Non-Shrink Grout Specifications, Test No. NJPCB-7<br>Figure B-20. Non-shrink Grout Compressive Test Certificate, Test No. NJPCB-7 |          |
| Figure C-1. Concrete Tarmac Strength Test  |          |
| Figure C-2. Concrete Tarmac Strength Test  |          |
| Figure D-1. Vehicle Mass Distribution, Test No. NJPCB-7  |          |
| Figure E-1. Floor Pan Deformation Data – Set 1, Test No. NJPCB-7   |          |
| Figure E-2. Floor Pan Deformation Data – Set 2, Test No. NJPCB-7   |          |
| Figure E-3. Occupant Compartment Deformation Data – Set 1, Test No. NJPCB-7  |          |
| Figure E-4. Occupant Compartment Deformation Data – Set 2, Test No. NJPCB-7  |          |
| Figure E-5. Exterior Vehicle Crush (NASS) - Front, Test No. NJPCB-7  | 105      |
| Figure E-6. Exterior Vehicle Crush (NASS) - Side, Test No. NJPCB-7   |          |
| Figure F-1. 10-ms Average Longitudinal Deceleration (SLICE-2), Test No. NJPCB-7  |          |
| Figure F-2. Longitudinal Occupant Impact Velocity (SLICE-2), Test No. NJPCB-7  |          |
| Figure F-3. Longitudinal Occupant Displacement (SLICE-2), Test No. NJPCB-7   |          |
| Figure F-4. 10-ms Average Lateral Deceleration (SLICE-2), Test No. NJPCB-7   |          |
| Figure F-5. Lateral Occupant Impact Velocity (SLICE-2), Test No. NJPCB-7   |          |
| Figure F-6. Lateral Occupant Displacement (SLICE-2), Test No. NJPCB-7<br>Figure F-7. Vehicle Angular Displacements (SLICE-2), Test No. NJPCB-7 |          |
| Figure F-7. Venicle Angular Displacements (SLICE-2), Test No. NJPCB-7<br>Figure F-8. Acceleration Severity Index (SLICE-2), Test No. NJPCB-7   |          |
| Figure F-9. 10-ms Average Longitudinal Deceleration (SLICE-1), Test No. NJPCB-7  |          |
| Figure F-10. Longitudinal Occupant Impact Velocity (SLICE-1), Test No. NJPCB-7   |          |
| Figure F-11. Longitudinal Occupant Displacement (SLICE-1), Test No. NJPCB-7  |          |
| Figure F-12. 10-ms Average Lateral Deceleration (SLICE-1), Test No. NJPCB-7  |          |
|  |          |

| Figure F-13. Lateral Occupant Impact Velocity (SLICE-1), Test No. NJPCB-7 |  |
|---|--|
| Figure F-14. Lateral Occupant Displacement (SLICE-1), Test No. NJPCB-7    |  |
| Figure F-15. Vehicle Angular Displacements (SLICE-1), Test No. NJPCB-7    |  |
| Figure F-16. Acceleration Severity Index (SLICE-1), Test No. NJPCB-7      |  |

# LIST OF TABLES

| Table 1. 2013 NJDOT Roadway Design Manual PCB Guidance [1]                | 1  |
|---|----|
| Table 2. Current 2015 NJDOT Roadway Design Manual PCB Guidance [2]        |    |
| Table 3. MASH 2016 TL-3 Crash Test Conditions for Longitudinal Barriers   | 3  |
| Table 4. MASH 2016 Evaluation Criteria for Longitudinal Barrier           | 5  |
| Table 5. Weather Conditions, Test No. NJPCB-7                             | 32 |
| Table 6. Sequential Description of Impact Events, Test No. NJPCB-7        | 32 |
| Table 7. Maximum Occupant Compartment Deformations by Location            | 36 |
| Table 8. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. NJPCB-7 | 37 |
| Table 9. Summary of Safety Performance Evaluation                         | 59 |
| Table 10. Comparison of Pinned Systems on One Side Only                   | 61 |
| Table B-1. Bill of Materials, Test No. NJPCB-7                            | 75 |

# **1 INTRODUCTION**

## **1.1 Background**

The New Jersey Department of Transportation (NJDOT) currently uses a New Jersey shape, Precast Concrete Curb, Concrete Barrier, which will be referred to as portable concrete barrier (PCB), with a vertical, I-beam connection pin to attach barriers end to end within their work zones and construction areas. The 2013 NJDOT *Roadway Design Manual* [1] provides guidance on allowable barrier deflections for various classes of PCB joint treatments, as shown in Table 1. The current 2015 NJDOT *Roadway Design Manual* [2] provides guidance on allowable deflections for various connection types, as shown in Table 2.

| Table 1 2013 NIDOT Roady  | way Design Manual PCB Guidance [1]  |
|---------------------------|-------------------------------------|
| Table 1. 2015 NJDOT Koauv | way Design Manual I CD Ouldance [1] |

| Joint Class | Use   | Joint Treatment   |
|-------------|---|---|
| А           | Allowable movement over 16 to 24 inches         | Connection Key only   |
| В           | Allowable movement over 11 to 16 inches         | Connection Key and grout in every joint   |
| С           | Allowable movement of 11 inches                 | Connection Key and grout in every joint and pin<br>every other unit. In units to be anchored, pin<br>should be required in every recess |
| D           | No allowable movement<br>(i.e., bridge parapet) | Connection Key and grout in every joint and bolt<br>every anchor pocket hole in every unit  |

Table 2. Current 2015 NJDOT Roadway Design Manual PCB Guidance [2]

| Connection<br>Type | Use   | Joint Treatment*  |
|--------------------|---|---|
| А                  | Maximum allowable deflection of 41 inches   | Connection Key and barrier end sections fully pinned  |
| В                  | Maximum allowable deflection of 28 inches (Cannot be used with traffic on both sides of the barrier.) | Connection Key, 6" by 6" box beam, and barrier end sections fully pinned                              |
| C                  | Maximum allowable deflection of 11 inches   | Connection Key, construction side of all<br>sections pinned, and barrier end sections<br>fully pinned |

\* Barrier end sections fully pinned – first and last barrier segments of the entire run regardless of connection type have pins in every anchor recess on both sides.

The guidance provided in both the 2013 and 2015 *Roadway Design Manual* was based on test data obtained from previous testing standards, which needs to be updated to be consistent with current crash testing standards and a changing vehicle fleet. Crash testing of other PCB systems under the Test Level 3 (TL-3) criteria of the *Manual for Assessing Safety Hardware, Second Edition* (MASH 2016) [3] has indicated that dynamic barrier deflections can increase significantly

when compared to dynamic deflections based on older crash test data. Thus, a need exists to investigate the performance of the NJDOT PCB system in various configurations in order to provide updated design guidance. The NJDOT PCB standard plans are shown in Appendix A.

# **1.2 Objective**

The objective of this research effort included an evaluation of the safety performance of NJDOT's PCB, Type 4 (Alternative B) with a traffic-side pinned configuration and grouted toes. The system was evaluated according to the Test Level 3 (TL-3) criteria set forth in the *Manual for Assessing Safety Hardware, Second Edition* (MASH 2016) [3].

## 1.3 Scope

The research objective was achieved through completion of several tasks. One full-scale crash test was conducted on the PCB system according to MASH 2016 test designation no. 3-11. Next, the full-scale vehicle crash test results were analyzed, evaluated, and documented. Conclusions and recommendations were then made pertaining to the safety performance of the PCB system.

## 2 TEST REQUIREMENTS AND EVALUATION CRITERIA

#### **2.1 Test Requirements**

Longitudinal barriers, such as PCBs, must satisfy impact safety standards in order to be declared eligible for federal reimbursement by the Federal Highway Administration (FHWA) for use on the National Highway System (NHS). For new hardware, these safety standards consist of the guidelines and procedures published in MASH 2016 [3]. Note that there is no difference between MASH 2009 [4] and MASH 2016 for most longitudinal barriers, such as the PCB system tested in this project, except that additional occupant compartment deformation measurements are required by MASH 2016. According to TL-3 of MASH 2016, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests, as summarized in Table 3. However, only the 2270P crash test was deemed necessary as other prior small car tests were used to support a decision to deem the 1100C crash test not critical.

|                 | Test               |                 | Vehicle               | Impact C                | onditions      |                                     |
|-----------------|--------------------|-----------------|-----------------------|-------------------------|----------------|-------------------------------------|
| Test<br>Article | Designation<br>No. | Test<br>Vehicle | Weight,<br>lb<br>(kg) | Speed,<br>mph<br>(km/h) | Angle,<br>deg. | Evaluation<br>Criteria <sup>1</sup> |
| Longitudinal    | 3-10               | 1100C           | 2,420<br>(1,100)      | 62<br>(100)             | 25             | A,D,F,H,I                           |
| Barrier         | 3-11               | 2270P           | 5,000<br>(2,268)      | 62<br>(100)             | 25             | A,D,F,H,I                           |

 Table 3. MASH 2016 TL-3 Crash Test Conditions for Longitudinal Barriers

<sup>1</sup> Evaluation criteria explained in Table 4.

In test no. 7069-3, a rigid, F-shape, concrete bridge rail was successfully impacted by a small car weighing 1,800 lb (816 kg) at 60.1 mph (96.7 km/h) and 21.4 degrees according to the American Association of State Highway and Transportation Officials (AASHTO) *Guide Specifications for Bridge Railings* [5-6]. In the same manner, test nos. CMB-5 through CMB-10, CMB-13, and 4798-1 showed that rigid, New Jersey, concrete safety shape barriers struck by small cars have been shown to meet safety performance standards [7-8]. In addition, in test no. 2214NJ-1, a rigid, New Jersey, <sup>1</sup>/<sub>2</sub>-section, concrete safety shape barrier was impacted by a passenger car weighing 2,579 lb (1,170 kg) at 60.8 mph (97.8 km/h) and 26.1 degrees according to the TL-3 standards set forth in MASH 2009 [9]. Furthermore, temporary, New Jersey safety shape, concrete median barriers have experienced only slight barrier deflections when impacted by small cars and behave similarly to rigid barriers as seen in test no. 47 [10]. As such, the 1100C passenger car test was deemed not critical for testing and evaluating this PCB system.

It should be noted that the test matrix detailed herein represents the researchers' best engineering judgement with respect to the MASH 2016 safety requirements and their internal evaluation of critical tests necessary to evaluate the crashworthiness of the barrier system. However, the recent switch to new vehicle types as part of the implementation of the MASH 2016 criteria and the lack of experience and knowledge regarding the performance of the new vehicle types with certain types of hardware could result in unanticipated barrier performance. Thus, any

tests within the evaluation matrix deemed non-critical may eventually need to be evaluated based on additional knowledge gained over time or revisions to the MASH 2016 criteria.

## **2.2 Evaluation Criteria**

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the PCB system to contain and redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 4 and defined in greater detail in MASH 2016. The full-scale vehicle crash test documented herein was conducted and reported in accordance with the procedures provided in MASH 2016.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported. Additional discussion on PHD, THIV and ASI is provided in MASH 2016.

| Table 4. MASH 2016 Evaluation | Criteria for | Longitudinal Barrier |
|-------------------------------|--------------|----------------------|
| Table 4. MASH 2010 Evaluation |              | Longituumai Darrier  |

| Structural<br>Adequacy | A. | Test article should contain and redirect the vehicle or bring the vehicle<br>to a controlled stop; the vehicle should not penetrate, underride, or<br>override the installation although controlled lateral deflection of the<br>test article is acceptable.   |                      |                       |  |
|------------------------|----|--|----------------------|-----------------------|--|
|                        | D. | Detached elements, fragments or other debris from the test article<br>should not penetrate or show potential for penetrating the occupant<br>compartment, or present an undue hazard to other traffic, pedestrians,<br>or personnel in a work zone. Deformations of, or intrusions into, the<br>occupant compartment should not exceed limits set forth in Section<br>5.2.2 and Appendix E of MASH 2016. |                      |                       |  |
|                        | F. | The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.  |                      |                       |  |
| Occupant               | H. | Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits:  |                      |                       |  |
| Risk                   |    | Occupant Impact Velocity Limits  |                      |                       |  |
|                        |    | Component  | Preferred            | Maximum               |  |
|                        |    | Longitudinal and Lateral   | 30 ft/s<br>(9.1 m/s) | 40 ft/s<br>(12.2 m/s) |  |
|                        | I. | The Occupant Ridedown Acceleration (ORA) (see Appendix A<br>Section A5.2.2 of MASH 2016 for calculation procedure) should<br>satisfy the following limits:   |                      |                       |  |
|                        |    | Occupant Ridedown Acceleration Limits  |                      |                       |  |
|                        |    | Component  | Preferred            | Maximum               |  |
|                        |    | Longitudinal and Lateral   | 15.0 g's             | 20.49 g's             |  |

#### **3 DESIGN DETAILS**

The test installation consisted of ten 20-ft (6.1-m) long NJDOT PCBs with a traffic-side pinned configuration and grouted toes, as shown in Figures 1 through 14. This system uses NJDOT barriers, Type 4 (Alternative B). Photographs of the test installation are shown in Figures 15 through 18. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix B.

The concrete mix for the barrier sections required a minimum 28-day compressive strength of 3,700 psi (25.5 MPa). A minimum concrete cover of 1½ in. (38 mm) was used along all rebar in the barrier. All of the steel reinforcement in the barrier was ASTM A615 Grade 60 rebar and consisted of four No. 6 longitudinal bars, eight No. 4 bars for the vertical stirrups, four No. 6 lateral bars, and nine No. 4 bars for the anchor hole reinforcement loops. The section reinforcement details are shown in Figures 5 and 6.

The barrier sections connected were with connection keys, as shown in Figures 7 through 11 and 16. The connection key assembly consisted of ½-in. (13-mm) thick, ASTM A36 steel plates welded together to form the key shape. A connection socket was configured at each end of the PCB section, as shown in Figures 2, 15, and 16. The connection socket consisted of three ASTM A36 steel plates welded on the sides of an ASTM A500 Grade B or C steel tube, as shown in Figures 9 and 10. The connection key was inserted into the steel tubes of two adjoining PCBs to form the connection, as shown in Figure 11.

Barrier nos. 1 and 10 were anchored to the concrete tarmac on both the traffic side and the back side, while barrier nos. 2 through 9 were anchored to the concrete tarmac only on the traffic side through the pin anchor recesses with 1-in. (25-mm) diameter by 15-in. (381-mm) long, ASTM A36 steel pins inserted into 1<sup>1</sup>/<sub>4</sub>-in. (32-mm) diameter holes drilled in the concrete tarmac, as shown in Figures 12 and 17. The steel pins were embedded to a depth of 5 in. (127 mm), as shown in Figure 1. During installation, the barrier segments were pulled in a direction parallel to their longitudinal axes, and slack was removed from all joints. After slack was removed from all the joints, the 1<sup>1</sup>/<sub>4</sub>-in. (32-mm) diameter holes were drilled for the pin anchors at pin recess locations. Five samples of concrete tarmac were tested from five different locations of MwRSF's Outdoor Test Site. The concrete tarmac had a compressive strength ranging between 5,970 and 7,040 psi (41.2 and 48.5 MPa), as shown in Appendix C. Non-shrink grout wedges were placed at the toe of each barrier segment in every joint between adjacent barrier segments on both traffic and back sides, as shown in Figures 1, 2, and 18. The grout wedges consisted of a grout mix with a minimum 1-day compressive strength of 1,000 psi (6.9 MPa).

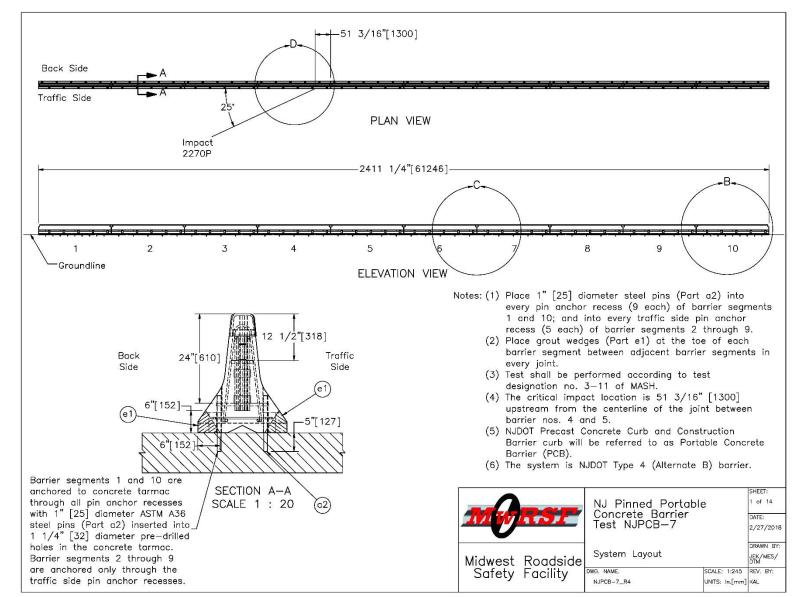


Figure 1. Test Installation Layout, Test No. NJPCB-7

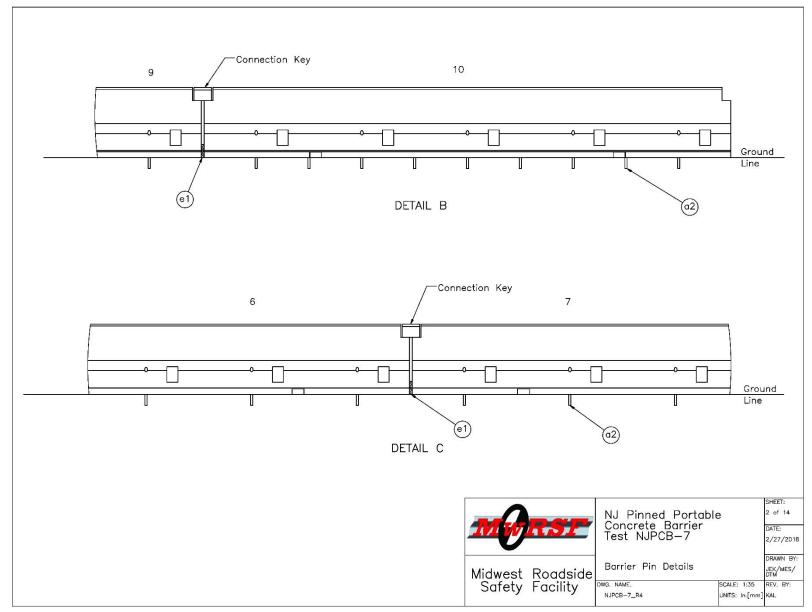


Figure 2. PCB Pin Anchor Details, Test No. NJPCB-7

 $\infty$ 

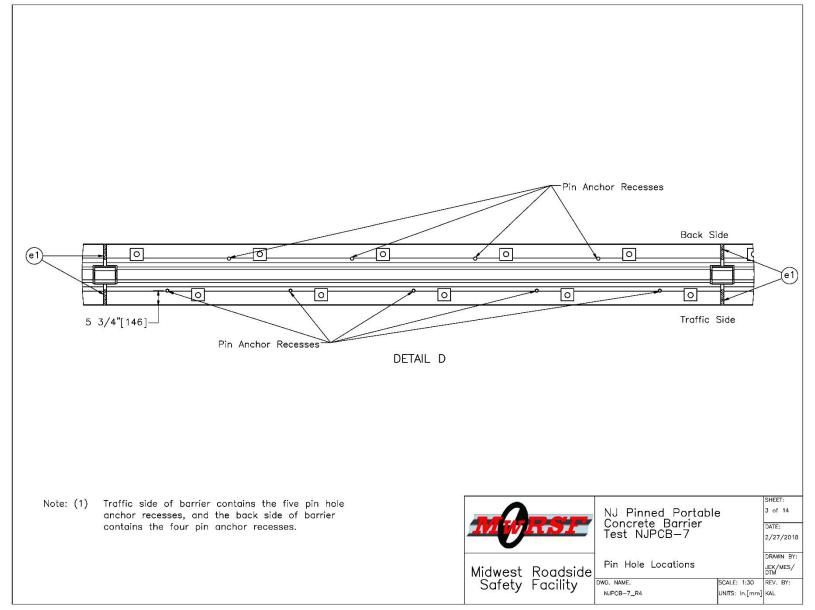


Figure 3. PCB Pin Anchor Locations, Test No. NJPCB-7

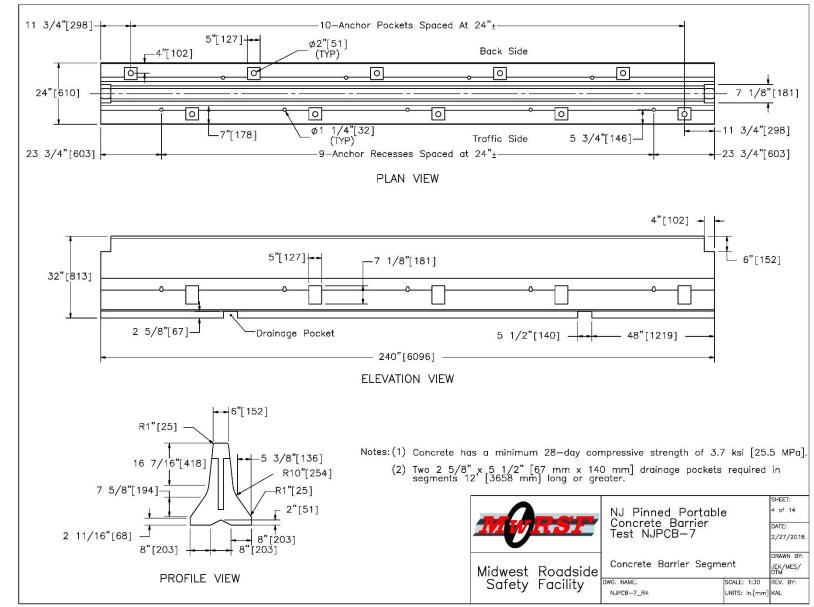


Figure 4. PCB Details, Test No. NJPCB-7

10

December 18, 2018 MwRSF Report No. TRP-03-374-18

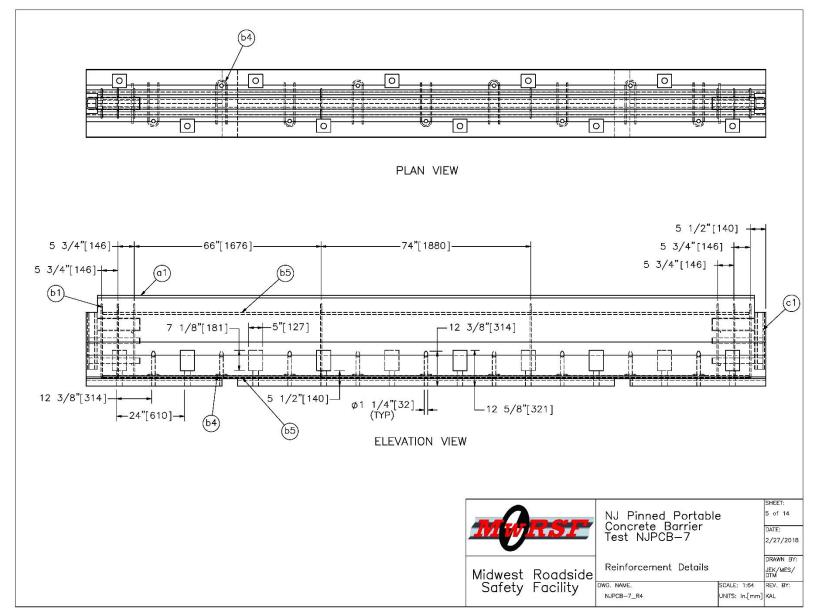


Figure 5. PCB Reinforcement Details, Test No. NJPCB-7

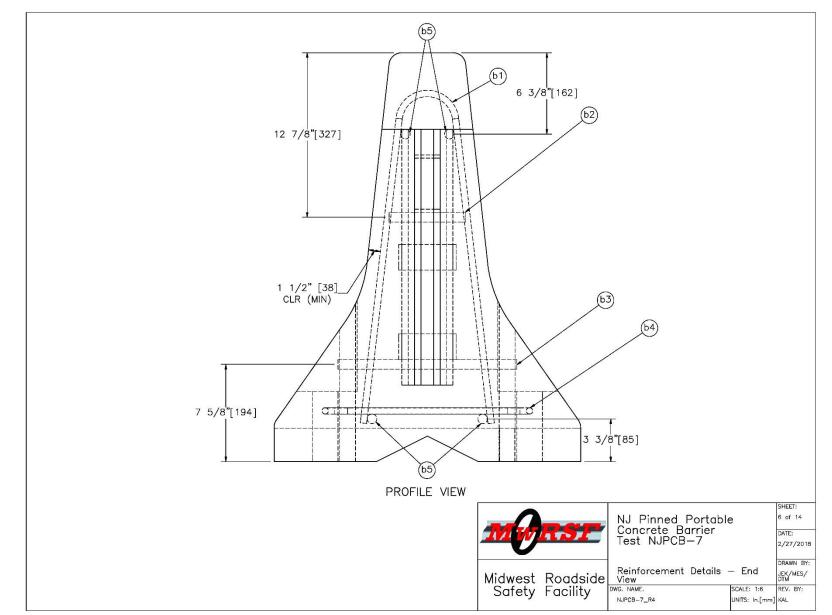


Figure 6. PCB Reinforcement Details – End View, Test No. NJPCB-7

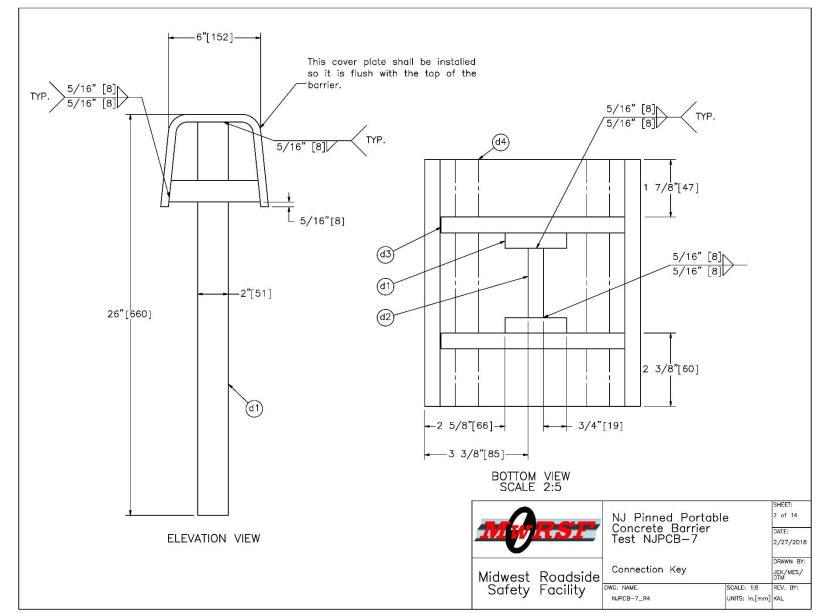


Figure 7. PCB Connection Key Assembly Details, Test No. NJPCB-7

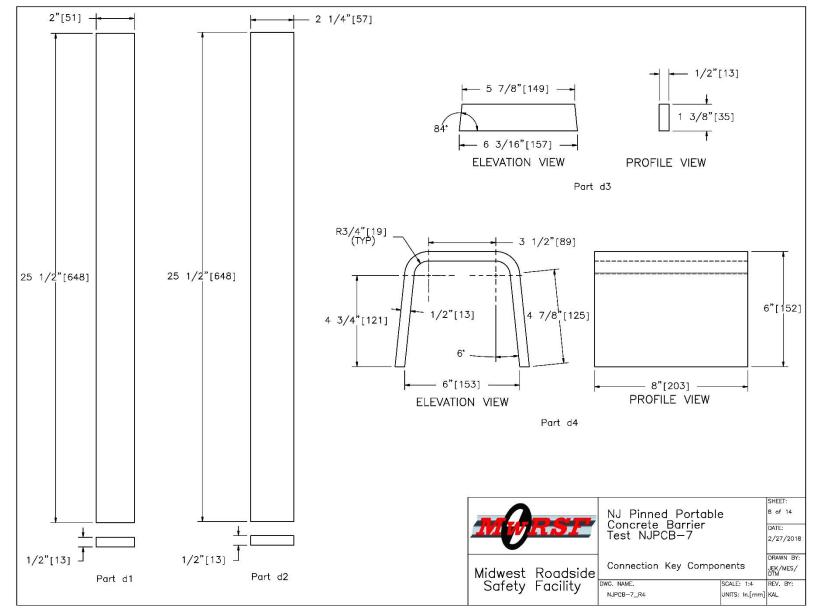


Figure 8. PCB Connection Key Component Details, Test No. NJPCB-7

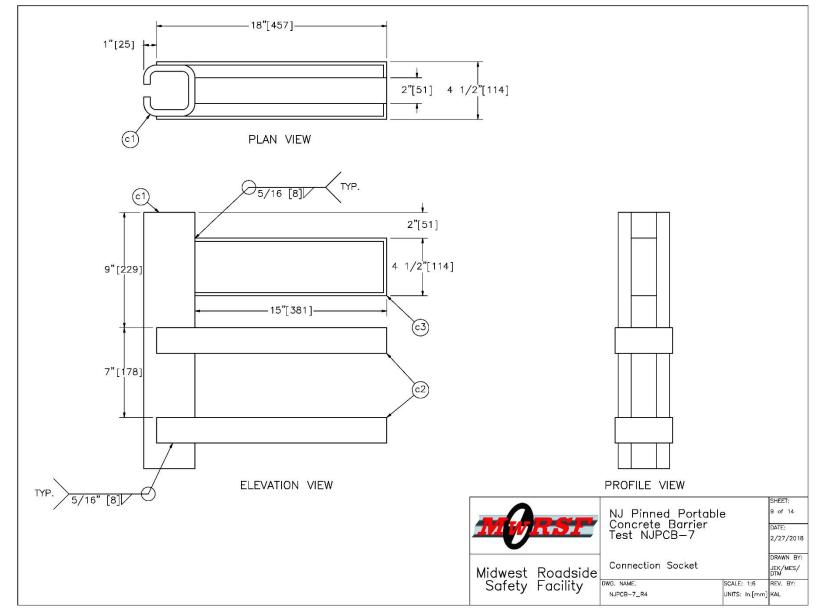


Figure 9. PCB Connection Socket Details, Test No. NJPCB-7

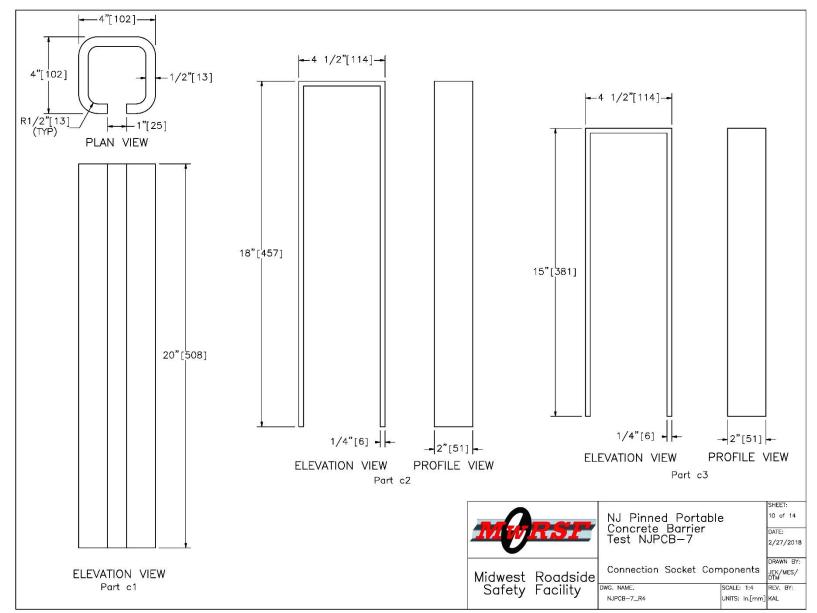


Figure 10. PCB Connection Socket Component Details, Test No. NJPCB-7

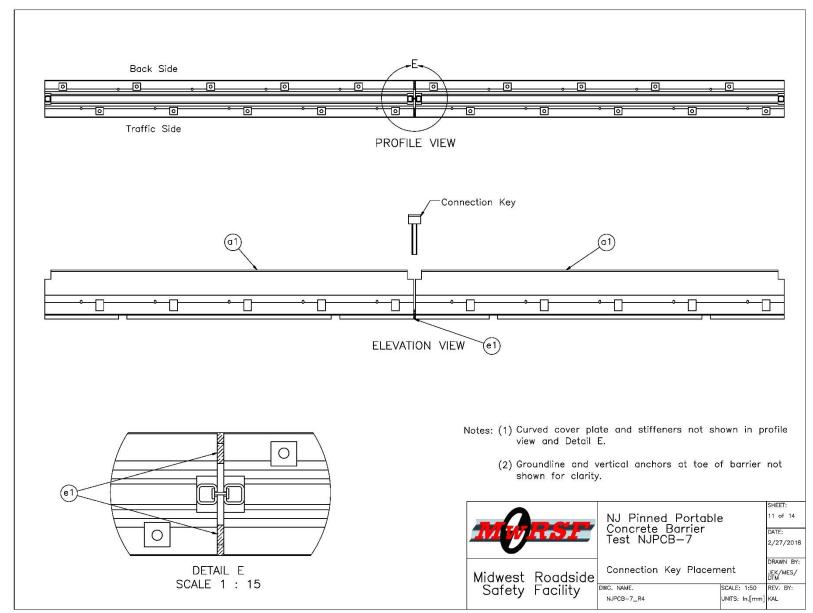


Figure 11. Connection Key Placement Details, Test No. NJPCB-7

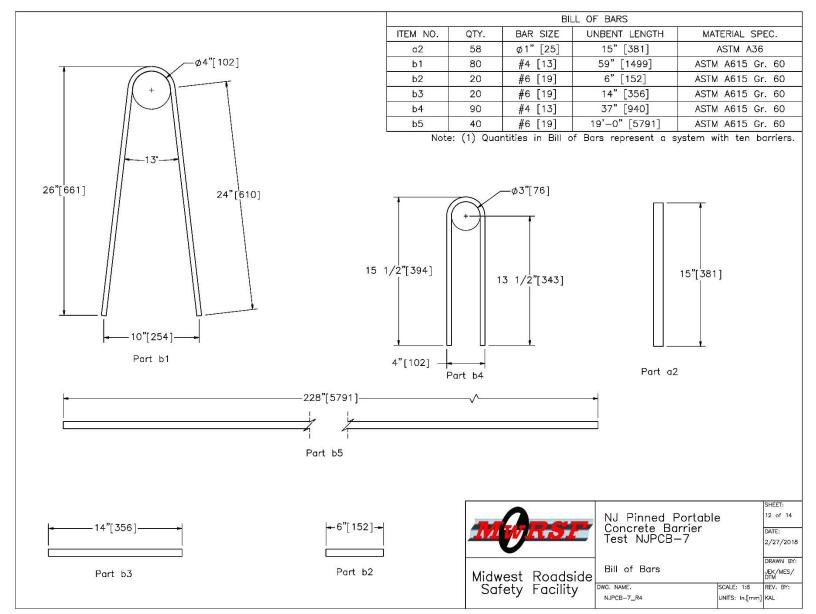


Figure 12. PCB Reinforcement Details, Test No. NJPCB-7

- (1) Minimum concrete clear cover for reinforcement steel shall be 1 1/2" [38 mm].
- (2) All end segments shall be pinned.
- (3) After a segment has been placed and the connection key inserted, pull the unit in a direction parallel to its longitudinal axis to remove any slack in the joint.
- (4) The portable concrete barrier shall be cast in steel forms.
- (5) The portable concrete barrier shall be barrier segments of 20 feet [6,096 mm]. However, other lengths may be used to meet field conditions. The number and placement of the b2 and b3 reinforcement steel will vary with the length of the barrier segment as shown on the table of variable reinforcement steel. The b5 reinforcement steel shall be 10" [254 mm] shorter than the nominal length of the barrier segments.
- (6) Reinforcing shown is the minimum required. Additional reinforcing necessary for handling shall be the option and responsibility of the contractor.
- (7) Welding and fabrication of steel structures shall be in accordance with sections 1 thru 6 of the ANSI/AASHTO/AWS D1.5 bridge welding code and section 10 of the ANSI/AWS D1 structural welding code. Surfaces to be welded shall be free of scale, slag, rust, moisture, grease or any other material that will prevent proper welding or produce objectional furnes. Welding shall be shielded metal arc welding using properly dried 5/32" [4 mm] dia. E7018 electrodes.
- (8) The length of the pins shall be such that a minimum embedment length of 5" [127 mm] is obtained when embedded into concrete pavement. When anchor pins are in place, they shall not project above the plane of the concrete surface of the barrier. Holes in bridge decks shall be 1 1/4" [32 mm] diameter maximum and made with a core drill or any other approved rotary drilling device that does not impart an impact force.
- (9) Use non-shrink grout of a plastic consistency that is listed on the QPL and conforms to ASTM C 1107 with the following amendments:
   1. Ensure that the grout has a working time of at least 30 minutes from the time the water is added.
  - 2. Match the color of the hardened grout, where visible, to the color of the adjacent hardened concrete.
  - 3. Include 1-day strength tests as part of the performance requirements of ASTM C 1107.
  - 4. Ensure that the grout contains no more than 0.05 percent chlorides or 5.0 percent sulfates by weight.
  - 5. Minimum 1-day compressive strength of 1,000 psi [7.0 MPa].
- (10) Use connection key in every joint. Grout is placed at the toe of each barrier segment between adjacent barrier segments in every joint. Pin every segment in all traffic side anchor pin recesses, and pin both end segments in every anchor pin recess.

| MURSE            | NJ Pinned Portable<br>Concrete Barrier<br>Test NJPCB-7 | e                             | SHEET:<br>13 of 14<br>DATE:<br>2/27/2018 |
|------------------|--|-------------------------------|--|
| Midwest Roadside | General Notes  |                               | DRAWN BY:<br>JEK/MES/<br>DTM             |
| Safety Facility  | DWG. NAME.<br>NJPCB-7_R4                               | SCALE: None<br>UNITS: In.[mm] | REV. BY:<br>KAL                          |

Figure 13. General Notes, Test No. NJPCB-7

| ltern<br>No. | QTY. | Description   | Material Spec  | Galvanization Spec |
|--------------|------|---|--|--------------------|
| a1           | 10   | Concrete Barrier Segment — NJDOT Type 4 Barrier (Alternate B) | f'c = 3,700 psi [25.5 MPa]                             |                    |
| a2           | 58   | 1" [25] Dia., 15" [381] Long Steel Anchor Pin                 | ASTM A36   | ASTM A123*         |
| b1           | 80   | 1/2" [13] Dia., 59" [1499] Long Bent Rebar                    | ASTM A615 Gr. 60                                       | ( <u>)</u> (       |
| b2           | 20   | 3/4" [19] Dia., 6" [152] Long Rebar                           | ASTM A615 Gr. 60                                       |                    |
| b3           | 20   | 3/4" [19] Dia., 14" [356] Long Rebar                          | ASTM A615 Gr. 60                                       | -                  |
| b4           | 90   | 1/2" [13] Dia., 37" [940] Long Bent Rebar                     | ASTM A615 Gr. 60                                       | -                  |
| b5           | 40   | 3/4" [19] Dia., 228" [5791] Long Rebar                        | ASTM A615 Gr. 60                                       | -                  |
| c1           | 20   | 4"x4"x1/2" [102x102x13] x 20" [508] Long Tube                 | ASTM A500 Gr. B or C                                   |                    |
| c2           | 40   | 40 1/2"x2"x1/4" [1,029x51x6] Bent Steel Plate                 | ASTM A36   | -                  |
| c3           | 20   | 34 1/2"x2"x1/4" [876x51x6] Bent Steel Plate                   | ASTM A36   | -                  |
| <b>d</b> 1   | 18   | 25 1/2"x2"x1/2" [648x51x13] Steel Plate                       | ASTM A36   | -                  |
| d2           | 9    | 25 1/2"x2 1/4"x1/2" [648x57x13] Steel Plate                   | ASTM A36   | -                  |
| d3           | 18   | 6 3/16"x1 3/8"x1/2" [157x35x13] Steel Plate - Stiffener       | ASTM A36   |                    |
| d4           | 9    | 17"x8"x1/2" [432x203x13] Bent Steel Plate - Top Plate         | ASTM A36   |                    |
| e1           | 1    | Non-Shrink Grout  | Min. 1—day Compressive Strength<br>1,000 psi [7.0 MPa] |                    |

\* Component does not need to be galvanized for testing purposes.

| MURSE            | NJ Pinned Portable<br>Concrete Barrier<br>Test NJPCB-7 | 9                             | SHEET:<br>14 of 14<br>DATE:<br>2/27/2018 |
|------------------|--|-------------------------------|--|
| Midwest Roadside | Bill of Materials                                      |                               | DRAWN BY:<br>JEK/MES/<br>DTM             |
| Safety Facility  | DWG. NAME.<br>NJPCB-7_R4                               | SCALE: None<br>UNITS: In.[mm] | REV. BY:<br>KAL                          |

Figure 14. Bill of Materials, Test No. NJPCB-7



Figure 15. NJDOT PCB with Traffic-Side Pinned Configuration and Grouted Toes Test Installation, Test No. NJPCB-7



Figure 16. PCB Connection Key and Connection Socket, Test No. NJPCB-7





Figure 17. PCB Traffic-Side Pin Anchor Recesses, Test No. NJPCB-7



Figure 18. Grout at Toes between PCBs, Test No. NJPCB-7

#### **4 TEST CONDITIONS**

#### 4.1 Test Facility

The Outdoor Test Site is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles (8.0 km) northwest of the University of Nebraska-Lincoln.

#### 4.2 Vehicle Tow and Guidance System

A reverse-cable, tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [11] was used to steer the test vehicle. A guide flag, attached to the right-front wheel and the guide cable, was sheared off before impact with the barrier system. The  $\frac{3}{8}$ -in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.5 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

## 4.3 Test Vehicle

For test no. NJPCB-7, a 2010 Dodge Ram 1500 quad cab pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,053 lb (2,292 kg), 5,000 lb (2,268 kg), and 5,155 lb (2,338 kg), respectively. The test vehicle is shown in Figure 19, and vehicle dimensions are shown in Figure 20. Note that pre-test photographs of the vehicle's interior floorboards and undercarriage are not available.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [12] was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The location of the final c.g. is shown in Figures 20 and 21. Data used to calculate the location of the c.g. and ballast information are shown in Appendix D.

Square, black- and white-checkered targets were placed on the vehicle for reference to be viewed from the high-speed digital video cameras and aid in the video analysis, as shown in Figure 21. Round, checkered targets were placed on the c.g. on the left-side door, the right-side door, and the roof of the vehicle. The front wheels of the test vehicle were aligned to vehicle standards except the toe-in value was adjusted to zero such that the vehicles would track properly along the guide cable. A 5B flash bulb was mounted under the vehicle's left-side windshield wiper and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on

the high-speed digital videos. A remote-controlled brake system was installed in the test vehicle to bring the vehicle safely to a stop after the test.





Figure 19. Test Vehicle, Test No. NJPCB-7

| Date:                  | Date: 6/9/2017 Test Name:           |                  |       |       | NJP              | CB-7                  | VIN No: | 1D7R                | 1D7RB1GP7AS162701   |   |                                  |                          |                     |
|------------------------|-------------------------------------|------------------|-------|-------|------------------|-----------------------|---------|---------------------|---------------------|---|----------------------------------|--------------------------|---------------------|
| Year:                  |                                     | 2010             |       |       |                  | Mak                   | ke:     | Do                  | dge                 | Model:  |                                  | Ram 1500                 |                     |
| Tire Size:             | P                                   | 265/70R1         | 7     | Ti    | ire Infla        | tion Pressu           | re:     | 40                  | Psi                 | Odometer:                                     |                                  | 207988                   |                     |
|                        |                                     | -[]              |       |       |                  |                       |         |                     | 1                   |   | eometry - in<br>as listed below  | n. (mm)                  |                     |
| <br>t Wheel<br>  Track |                                     |                  |       |       |                  |                       |         | m<br>Wheel<br>Track | a<br>               | a: 77 1/2<br><sub>78±2 (1</sub><br>c: 228 3/4 | 950±50)                          | b: 74 3/8<br>d: 47 5/8   | (1889)<br>(1210)    |
|                        |                                     |                  |       |       |                  |                       |         | <b>i</b>            | ļ                   | e: 140 1/4                                    | 6020±325)<br>(3562)<br>3760±300) |                          | (1022)<br>(1000±75) |
| le                     | est Ine                             | rtial C.M        | I.—   |       |                  | a                     | T       | IRE DIA             |                     | g: <u>28 1/16</u><br>min: 2                   |                                  | h: <u>62</u> 1/8         |                     |
| 1                      |                                     |                  | _     |       | Ŵ                | +  r  +               | v<br>   | HEEL DIA            |                     | i: <u>12 3/8</u>                              | (314)                            | j: <u>24 1/4</u>         | (616)               |
|                        | []                                  |                  |       |       |                  |                       |         |                     | _                   | k: <u>22 5/8</u>                              | (575)                            | l: <u>28 1/2</u>         | (724)               |
|                        |                                     | $(\mathbf{Q})$   | s     |       |                  | $= (\phi)$            |         |                     | _                   | m: <u>68 3/8</u><br>67±1.5 (                  | (1737)<br>1700±38)               | n: 68 1/4<br>67±1.5      | (1734)<br>(1700±38) |
|                        |                                     |                  |       |       |                  | n ———                 |         | T                   |                     | <b>o: <u>46 1/8</u></b><br>43±4 (1            | (1172)<br>100±75)                | p: <u>3 5/8</u>          | (92)                |
| -                      | - d -                               |                  | rear  | e -   |                  | Wfront                | f —     |                     |                     | q: <u>32 3/8</u>                              | (822)                            | r: <u>18 5/8</u>         | (473)               |
| -                      |                                     |                  |       | — c — |                  |                       | -       |                     |                     | s: <u>14 3/8</u>                              | (365)                            | t: <u>79 1/4</u>         | (2013)              |
| Mass Distrib           | ution Ib                            | o (kg)           |       |       |                  |                       |         |                     |                     |   |                                  | nt): 15 1/4              | (387)               |
| Gross Static           | LF <u>1</u>                         | 459 (            | (662) | RF_   | 1412             | (640)                 |         |                     |                     |   |                                  | ar): <u>15 1/4</u>       | (387)               |
|                        | LR _ 1                              | 146              | (520) | RR_   | 1138             | (516)                 |         |                     |                     | Cl  | Wheel W<br>earance (Fro          |                          | (895)               |
|                        |                                     |                  |       |       |                  |                       |         |                     |                     | с   | Wheel W<br>learance (Rea         |                          | (956)               |
| Weights<br>Ib (kg)     |                                     | Curb             |       |       | Test             | nertial               |         | Gross               | Static              |   | Bottom Fra<br>Height (Fro        | me<br>nt): 18 1/8        | (460)               |
| W-front                | 2                                   | 825 (            | 1281) |       | 2786             | (1264)                |         | 2871                | (1302)              |   | Bottom Fra<br>Height (Rea        | me<br>ar): <u>25 3/8</u> | (645)               |
| W-rear                 | 2                                   | 228 (            | 1011) |       | 2214             | (1004)                |         | 2284                | (1036)              |   | Engine Typ                       | be: Ga                   | soline              |
| W-total                | 5                                   | i <b>053 (</b> i | 2292) |       | 5000<br>5000±110 | (2268)<br>0 (2270±50) |         | 5155<br>5165±110    | (2338)<br>(2343±50) |   | Engine Siz                       | ze: 4.7                  | 7L V8               |
|                        |                                     |                  |       |       |                  | ( )                   |         |                     | ( ,                 | Trans   | mission Typ                      | be: Aut                  | omatic              |
| GVWR Rating            | gs Ib                               |                  |       | Du    | ummy l           | Data                  |         |                     |                     |   | Drive Typ                        | be: R                    | WD                  |
| Front                  | 360                                 | 00               |       |       |                  | Type:                 |         | Hybrid              | 11                  |   | Cab Sty                          | le: Qua                  | ad Cab              |
| Rear                   | 390                                 | 00               |       |       |                  | Mass:                 |         | 155 II              | )                   |   | Bed Leng                         | th:                      | 76"                 |
| Total                  | 680                                 | 00               |       |       | Sea              | Position:             |         | Drive               | r                   |   |                                  |                          |                     |
| Note ar                | Note any damage prior to test: NONE |                  |       |       |                  |                       |         |                     |                     |   |                                  |                          |                     |

Figure 20. Vehicle Dimensions, Test No. NJPCB-7

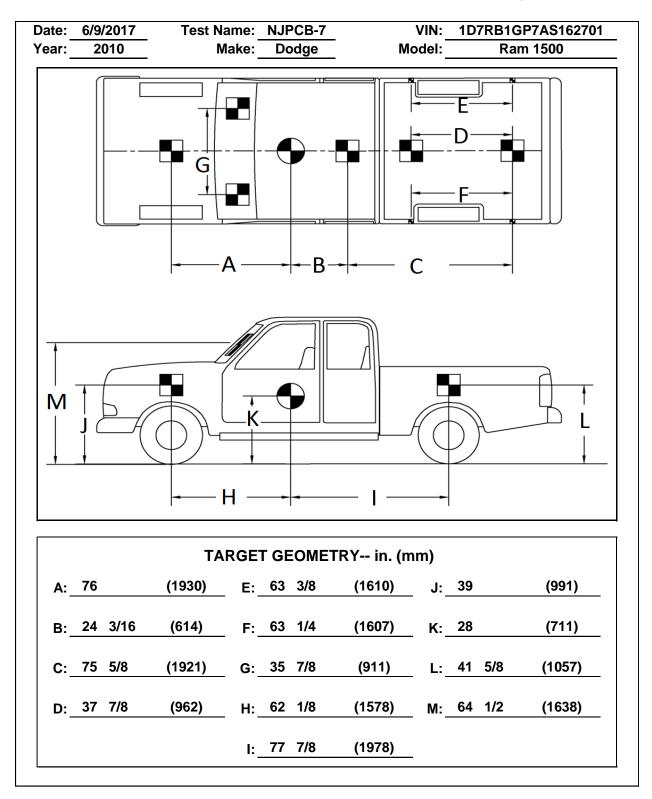


Figure 21. Target Geometry, Test No. NJPCB-7

# 4.4 Simulated Occupant

For test no. NJPCB-7, A Hybrid II 50<sup>th</sup>-Percentile, Adult Male Dummy, equipped with clothing and footwear, was placed in the left-front seat of the test vehicle with the seat belt fastened. The dummy, which had a final weight of 155 lb (70 kg), was represented by model no. 572, serial no. 451, and was manufactured by Android Systems of Carson, California. As recommended by MASH 2016, the dummy was not included in calculating the c.g. location.

# 4.5 Data Acquisition Systems

# 4.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. Both accelerometers were mounted near the c.g. of the test vehicle. The electronic accelerometer data obtained in testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filter conforming to the SAE J211/1 specifications [13].

The two systems, the SLICE-1 and SLICE-2 units, were modular data acquisition systems manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. The SLICE-2 unit was designated as the primary system, based on mounting location. The acceleration sensors were mounted inside the bodies of custom-built, SLICE 6DX event data recorders and recorded data at 10,000 Hz to the onboard microprocessor. Each SLICE 6DX was configured with 7 GB of non-volatile flash memory, a range of  $\pm 500$  g's, a sample rate of 10,000 Hz, and a 1,650 Hz (CFC 1000) anti-aliasing filter. The "SLICEWare" computer software programs and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

# 4.5.2 Rate Transducers

Two identical angular rate sensor systems, which were mounted inside the bodies of the SLICE-1 and SLICE-2 event data recorders, measured the rates of rotation of the test vehicle. Each SLICE MICRO Triax ARS had a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) and recorded data at 10,000 Hz to the onboard microprocessors. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The "SLICEWare" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

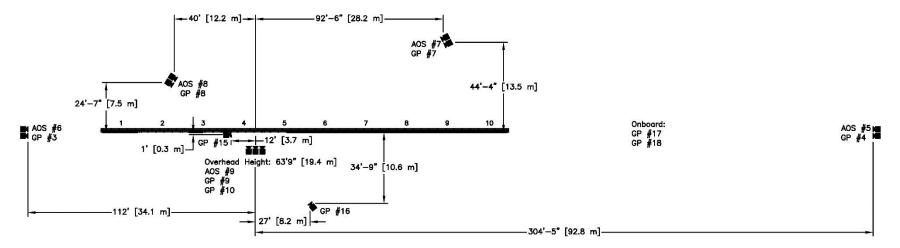
# 4.5.3 Retroreflective Optic Speed Trap

The retroreflective optic speed trap was used to determine the speed of the test vehicle before impact. Five retroreflective targets, spaced at approximately 18-in. (457-mm) intervals, were applied to the side of the vehicle. When the emitted beam of light was reflected by the targets and returned to the Emitter/Receiver, a signal was sent to the data acquisition computer, recording at 10,000 Hz, as well as the external LED box activating the LED flashes. The speed was then calculated using the spacing between the retroreflective targets and the time between the signals. LED lights and high-speed digital video analysis are only used as a backup in the event that vehicle speeds cannot be determined from the electronic data.

# **4.5.4 Digital Photography**

Five AOS high-speed digital video cameras and ten GoPro digital video cameras were utilized to film test no. NJPCB-7. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 22.

The high-speed digital videos were analyzed using TEMA Motion and RedLake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed digital videos. A Nikon digital still camera was also used to document pre- and post-test conditions for the test.



| No.   | Туре              | Operating Speed<br>(frames/sec) | Lens                | Lens Setting |
|-------|-------------------|---------------------------------|---------------------|--------------|
| AOS-5 | AOS X-PRI Gigabit | 500                             | VIVITAR 135mm Fixed | -            |
| AOS-6 | AOS X-PRI Gigabit | 500                             | Fujinon 50mm Fixed  | -            |
| AOS-7 | AOS X-PRI Gigabit | 500                             | Fujinon 35mm Fixed  | -            |
| AOS-8 | AOS S-VIT 1531    | 500                             | KOWA 25mm Fixed     | -            |
| AOS-9 | AOS TRI-VIT 2236  | 1000                            | KOWA 12mm Fixed     | -            |
| GP-3  | GoPro Hero 3+     | 120                             |                     |              |
| GP-4  | GoPro Hero 3+     | 120                             |                     |              |
| GP-7  | GoPro Hero 4      | 240                             |                     |              |
| GP-8  | GoPro Hero 4      | 240                             |                     |              |
| GP-9  | GoPro Hero 4      | 120                             |                     |              |
| GP-10 | GoPro Hero 4      | 240                             |                     |              |
| GP-15 | GoPro Hero 4      | 240                             |                     |              |
| GP-16 | GoPro Hero 4      | 240                             |                     |              |
| GP-17 | GoPro Hero 4      | 120                             |                     |              |
| GP-18 | GoPro Hero 4      | 120                             |                     |              |

Figure 22. Camera Locations, Speeds, and Lens Settings, Test No. NJPCB-7

# 5 FULL-SCALE CRASH TEST NO. NJPCB-7

# **5.1 Weather Conditions**

Test no. NJPCB-7 was conducted on July 12, 2017 at approximately 11:30 a.m. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 5.

 Table 5. Weather Conditions, Test No. NJPCB-7

| Temperature                  | 83° F                |
|------------------------------|----------------------|
| Humidity                     | 71%                  |
| Wind Speed                   | 5 mph                |
| Wind Direction               | 180° from True North |
| Sky Conditions               | Overcast             |
| Visibility                   | 10 Statute Miles     |
| Pavement Surface             | Dry                  |
| Previous 3-Day Precipitation | 0.01 in.             |
| Previous 7-Day Precipitation | 0.01 in.             |

# **5.2 Test Description**

The 5,000-lb (2,268-kg) pickup truck impacted the NJDOT PCB, Type 4 (Alternative B) with a traffic-side pinned configuration and grouted toes at a speed of 62.8 mph (101.0 km/h) and at an angle of 25.2 degrees. A summary of the test results and sequential photographs are shown in Figure 24. Additional sequential photographs are shown in Figures 25 and 26. Documentary photographs of the crash test are shown in Figures 27 through 30.

Initial vehicle impact was to occur 4 ft  $-3^{3}/_{16}$  in. (1.3 m) upstream from the centerline of the joint between barrier nos. 4 and 5, as shown in Figure 31, which was selected using Table 2.7 of MASH 2016. The actual point of impact was  $4^{7}_{8}$  in. (124 mm) downstream from the target location. A sequential description of the impact events is contained in Table 6. The vehicle came to rest 229 ft -11 in. (70.1 m) downstream from the impact point and 34 ft -3 in. (10.4 m) laterally away from the traffic side of the barrier, after brakes were applied. The vehicle trajectory and final position are shown in Figures 24 and 32.

| TIME  | EVENT   |
|-------|---|
| (sec) |   |
| 0.000 | Vehicle's left-front corner impacted barrier no. 4 at 3 ft $-10^{5/16}$ in. (1.2 m) upstream from centerline of joint between barrier nos. 4 and 5. |
| 0.003 | Left-front corner of bumper deformed inward.  |
| 0.010 | Vehicle's left fender contacted barrier no. 4 and deformed. Vehicle's left headlight contacted top of barrier no. 4.                                |

| 0.014 | Vehicle's left headlight deformed.   |
|-------|--|
| 0.024 | Downstream end of barrier no. 4 rolled backward. Vehicle's grille contacted barrier no. 4.   |
| 0.028 | Vehicle's grille deformed.   |
| 0.034 | Vehicle's front bumper contacted barrier no. 5. Upstream end of barrier no. 5 rolled backward.   |
| 0.036 | Vehicle yawed away from system. Vehicle's grille contacted barrier no. 5.<br>Barrier no. 5 rotated clockwise.                              |
| 0.042 | Vehicle pitched upward.  |
| 0.044 | Vehicle rolled away from system.   |
| 0.046 | Vehicle's airbags deployed. Vehicle's left-front door contacted barrier no. 4 and deformed. Vehicle's left fender contacted barrier no. 5. |
| 0.055 | Downstream end of barrier no. 5 spalled.   |
| 0.068 | Midspan of barrier no. 4 fractured.  |
| 0.084 | Vehicle's left-front door contacted barrier no. 5.   |
| 0.100 | Barrier nos. 6 and 7 rolled backward.  |
| 0.114 | Vehicle's right-front tire became airborne.  |
| 0.126 | Midspan of barrier no. 5 fractured.  |
| 0.144 | Vehicle's left-rear tire contacted barrier no. 4.  |
| 0.197 | Vehicle was parallel to system at a speed of 50.5 mph (81.3 km/h).   |
| 0.200 | Vehicle's left-rear quarter panel contacted barrier no. 4, and left taillight deformed.  |
| 0.240 | Vehicle pitched downward.  |
| 0.244 | Vehicle's right-rear tire became airborne.   |
| 0.257 | Barrier no. 4 rolled forward.  |
| 0.268 | Vehicle's left-front tire became airborne.   |
| 0.290 | Vehicle exited system at a speed of 50.3 mph (80.9 km/h) and at an angle of 7.1 degrees.   |
| 0.330 | Barrier nos. 6 and 7 rolled forward.   |
| 0.616 | Vehicle's right-front tire regained contact with ground.   |
| 0.658 | Vehicle's front bumper contacted ground.   |
| 0.680 | Vehicle rolled toward system.  |
| 0.716 | Vehicle's left headlight disengaged.   |
| 0.740 | Vehicle's left-front tire regained contact with ground.  |
| 0.794 | Vehicle pitched upward.  |
| 1.002 | Vehicle's left-rear tire regained contact with ground.   |
| 1.104 | Vehicle rolled away from system.   |

#### **5.3 Barrier Damage**

Damage to the barrier was moderate, as shown in Figures 33 through 37. Barrier damage consisted of contact and gouge marks on the front face of PCB segments, spalling of the concrete, and concrete cracking and fracture. The length of vehicle contact along the barrier was approximately 22 ft –  $\frac{3}{8}$  in. (6.7 m), which spanned from 5 ft –  $\frac{87}{8}$  in. (1.7 m) upstream from the center of the joint between barrier nos. 4 and 5 through 16 ft –  $\frac{31}{2}$  in. (5.0 m) downstream from the center of the joint between barrier nos. 4 and 5.

Tire marks were visible on the front face of barrier nos. 4 and 5. Scrape marks were also found on the front and top faces of barrier nos. 4 and 5. Grout between barrier nos. 3 and 4 and barrier nos. 4 and 5 crumbled. A 31<sup>1</sup>/<sub>2</sub>-in. (800-mm) long vertical crack was found on the front face of barrier no. 4 that started 56<sup>7</sup>/<sub>8</sub> in. (1,445 mm) downstream from the upstream end and 4<sup>1</sup>/<sub>8</sub> in. (105 mm) from the bottom. A 33<sup>3</sup>/4-in. (857-mm) long vertical crack was found on the front face of barrier no. 4 that started 89<sup>3</sup>/<sub>4</sub> in. (2,280 mm) downstream from the upstream end. A 45-in. (1,143-mm) long crack was found on the front face of barrier no. 4 located 12<sup>7</sup>/<sub>8</sub> in. (327 mm) downstream from the midspan of the barrier. A 36<sup>5</sup>/<sub>8</sub>-in. (930-mm) long crack was found on the front face of barrier no. 4 located 701/4 in. (1,784 mm) upstream from the downstream end of the barrier. A 26<sup>1</sup>/<sub>2</sub>-in. (673-mm) long crack was found on the back face of barrier no. 4 located 21<sup>1</sup>/<sub>2</sub> in. (546 mm) downstream from the midspan of the barrier. A 38<sup>1</sup>/<sub>4</sub>-in. (972-mm) long crack was found on the front face of barrier no. 5 located 35<sup>3</sup>/<sub>4</sub> in. (908 mm) upstream from the midspan of the barrier. A 38<sup>1</sup>/<sub>2</sub>-in. (978-mm) long crack was found on the front face of barrier no. 5 located 11<sup>1</sup>/<sub>4</sub> in. (286 mm) downstream from the midspan of the barrier. A 23<sup>1</sup>/<sub>2</sub>-in. (597-mm) long vertical crack was found on the back face of barrier no. 5 starting 62 in. (1,575 mm) downstream from the upstream end and 2 in. (51 mm) from the bottom. A 46-in. (1,168-mm) long crack was found on the back face of barrier no. 5 located 13<sup>1</sup>/<sub>8</sub> in. (333 mm) upstream from the midspan of the barrier. Minor cracks were found on the traffic side of barrier nos. 3, 6, and 7. A  $35\frac{1}{2}$ -in. long  $\times\frac{1}{2}$ -in. wide (902-mm  $\times$  13-mm) gouge was found 23<sup>1</sup>/<sub>2</sub> in. (597 mm) upstream from the downstream end on the front face of barrier no. 5.

Concrete spalling occurred on barrier nos. 4 through 6. The front side of barrier no. 4 experienced 57 in.  $\times 11^{3}$ /4 in.  $\times 9$  in. (1,448 mm  $\times 298$  mm  $\times 229$  mm) concrete spalling at the lower downstream corner. A 17<sup>1</sup>/4-in.  $\times 13^{1}/_{2}$ -in.  $\times 3^{1}/_{2}$ -in. (438-mm  $\times 343$ -mm  $\times 89$ -mm) concrete piece disengaged from barrier no. 4 at the lower-upstream corner on the back face. A 29-in.  $\times 5^{3}/_{4}$ -in. (737-mm  $\times 146$ -mm  $\times 102$ -mm) concrete piece disengaged from the front face of barrier no. 5, 57<sup>1</sup>/<sub>2</sub> in. (1,461 mm) downstream from the upstream end of the barrier. A 4<sup>1</sup>/<sub>4</sub>-in.  $\times 9^{1}/_{8}$ -in.  $\times 3^{1}/_{4}$ -in. (108-mm  $\times 232$ -mm  $\times 83$ -mm) concrete piece disengaged from the back face of barrier no. 5 at the lower-upstream corner. A 22<sup>3</sup>/<sub>4</sub>-in.  $\times 9^{1}/_{2}$ -in.  $\times 3^{3}/_{4}$ -in. (578-mm  $\times 241$ -mm  $\times 95$ -mm) concrete piece disengaged from the back face of barrier no. 5 at the lower-upstream corner. A 21<sup>3</sup>/<sub>4</sub>-in.  $\times 3^{1}/_{4}$ -in. (137-mm  $\times 51$ -mm  $\times 6$ -mm) concrete piece disengaged from the front face of barrier no. 6 at the lower-upstream corner. A 7<sup>1</sup>/<sub>4</sub>-in.  $\times 3^{1}/_{4}$ -in. (184-mm  $\times 83$ -mm) concrete piece disengaged from the front face of barrier no. 6 at the lower-upstream corner. A 7<sup>1</sup>/<sub>4</sub>-in.  $\times 3^{1}/_{4}$ -in. (184-mm  $\times 83$ -mm) concrete piece piece disengaged from the front face of barrier no. 6 at the lower-upstream corner. A 7<sup>1</sup>/<sub>4</sub>-in.  $\times 3^{1}/_{4}$ -in. (184-mm  $\times 83$ -mm) concrete piece p

The maximum permanent set deflection of the barrier system was 6<sup>1</sup>/<sub>4</sub> in. (159 mm) at the downstream end of barrier no. 4, as measured in the field. The maximum lateral dynamic barrier deflection, including tipping of the barrier along the top surface, was 11.4 in. (290 mm) at the

upstream end of barrier no. 5, as determined from high-speed digital video analysis. The working width of the system was found to be 35.4 in. (899 mm), also determined from high-speed digital video analysis. A schematic of the permanent set deflection, dynamic deflection, and working width is shown in Figure 23. In addition, NJDOT identifies the clear space behind the barrier, which is defined as the maximum deflection of the back of the barrier from its original position. For this test, the clear space behind the barrier was 11.4 in. (290 mm).

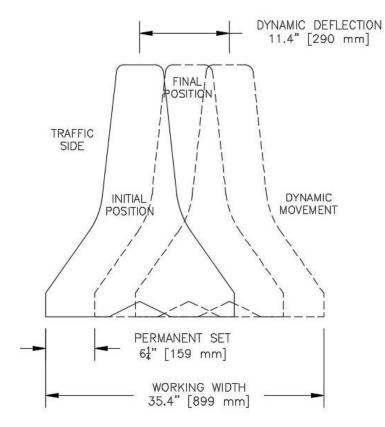


Figure 23. Permanent Set Deflection, Dynamic Deflection, and Working Width, Test No. NJPCB-7

# 5.4 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 39 through 43. The maximum occupant compartment deformations are listed in Table 7 along with the deformation limits established in MASH 2016 for various areas of the occupant compartment. Note that none of the MASH 2016 established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix E.

The majority of the damage was concentrated on the left-front corner and left side of the vehicle where the impact had occurred. The left side of the bumper crushed inward. The engine hood separated from the left fender. The left-front fender was deformed inward toward the engine compartment. The left corner of the front bumper was bent inward from the left side. The left-front corner of the frame rail buckled inward. A 2-in. (51-mm) gap occurred between the fender and the front bumper. Kinks and scrapes were observed on the entire front bumper. Denting, scraping, and gouging were observed on the entire left side of the cab. Gouging and contact marks were found

at the bottom of the left-front door, starting at the front of the door and extending across the entire cab and quarter panel. A 13-in.  $\times$  10-in. (330-mm  $\times$  254-mm) dent was found on the rear of the left-front door. The left headlight disengaged away from the vehicle.

The lower-left control arm was scraped and bent. The left-front upper control arm was bent 2 in. (51 mm) upward. The left-front wheel and hub partially disengaged. Tears were found in the left-front tire extending from the outer wall through the tread, and the rim buckled. Scrapes were found on the left-rear tire. The right-side engine cross member was bent. The right side of the windshield had 14-in. (356-mm) diameter spider-web cracking from the deployment of the right-side airbag. A crack extended from the spider-web crack to the lower-left corner, and two additional cracks were found in the lower-left corner of the windshield. The roof and the remaining window glass were undamaged.

| LOCATION                                | MAXIMUM<br>DEFORMATION<br>in. (mm) | MASH 2016 ALLOWABLE<br>DEFORMATION<br>in. (mm)                                 |
|---|------------------------------------|--|
| Wheel Well & Toe Pan                    | 31/4 (83)                          | ≤ 9 (229)  |
| Floor Pan & Transmission Tunnel         | 3/8 (10)                           | ≤ 12 (305)   |
| A-Pillar                                | 23/8 (60)                          | ≤ 5 (127)  |
| A-Pillar (Lateral)                      | 15/8 (41)                          | <i>≤</i> 3 (76)  |
| B-Pillar                                | 23/8 (60)                          | ≤ 5 (127)  |
| B-Pillar (Lateral)                      | 3/8 (10)                           | <i>≤</i> 3 (76)  |
| Side Front Panel (in Front of A-Pillar) | 2 (51)                             | ≤ 12 (305)   |
| Side Door (Above Seat)                  | 7/8 (22)                           | ≤ 9 (229)  |
| Side Door (Below Seat)                  | 13/8 (35)                          | ≤ 12 (305)   |
| Roof                                    | 1/8 (3)                            | ≤4 (102)   |
| Windshield                              | 0 (0)                              | ≤ 3 (76)   |
| Side Window                             | Intact                             | No shattering resulting from contact<br>with structural member of test article |
| Dash                                    | 11/2 (38)                          | N/A  |

Table 7. Maximum Occupant Compartment Deformations by Location

N/A - Not applicable

# 5.5 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 8. Note that the OIVs and ORAs were within suggested limits, as provided in MASH 2016. The calculated THIV, PHD, and ASI values are also shown in Table 8. The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 24. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix F.

|                   |                | Trans          | ducer                | MASH 2016    |  |
|-------------------|----------------|----------------|----------------------|--------------|--|
| Evaluat           | ion Criteria   | SLICE-1        | SLICE-2<br>(Primary) | Limits       |  |
| OIV               | Longitudinal   | -14.34 (-4.37) | -14.09 (-4.30)       | ± 40 (12.2)  |  |
| ft/s (m/s)        | Lateral        | 19.23 (5.86)   | 21.56 (6.57)         | ± 40 (12.2)  |  |
| ORA               | Longitudinal   | -3.39          | -3.65                | ± 20.49      |  |
| g's               | Lateral        | 9.52           | 7.98                 | $\pm 20.49$  |  |
| MAX.              | Roll           | -33.7          | -29.2                | ± 75         |  |
| ANGULAR<br>DISPL. | Pitch          | -17.0          | -18.6                | ±75          |  |
| deg.              | Yaw            | 41.2           | 40.2                 | not required |  |
|                   | HIV<br>s (m/s) | 24.31 (7.41)   | 26.81 (8.17)         | not required |  |
|                   | PHD<br>g's     | 9.64           | 8.08                 | not required |  |
|                   | ASI            | 1.25           | 1.41                 | not required |  |

Table 8. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. NJPCB-7

#### **5.6 Discussion**

The analysis of the test results showed that the system adequately contained and redirected the 2270P vehicle with controlled lateral displacements of the barrier. Detached elements, fragments, or other debris from the test article did not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or work-zone personnel. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix F, were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After impact, the vehicle exited the barrier at an angle of 7.1 degrees, and its trajectory did not violate the bounds of the exit box. Therefore, test no. NJPCB-7 was determined to be acceptable according to the MASH 2016 safety performance criteria for test designation no. 3-11.

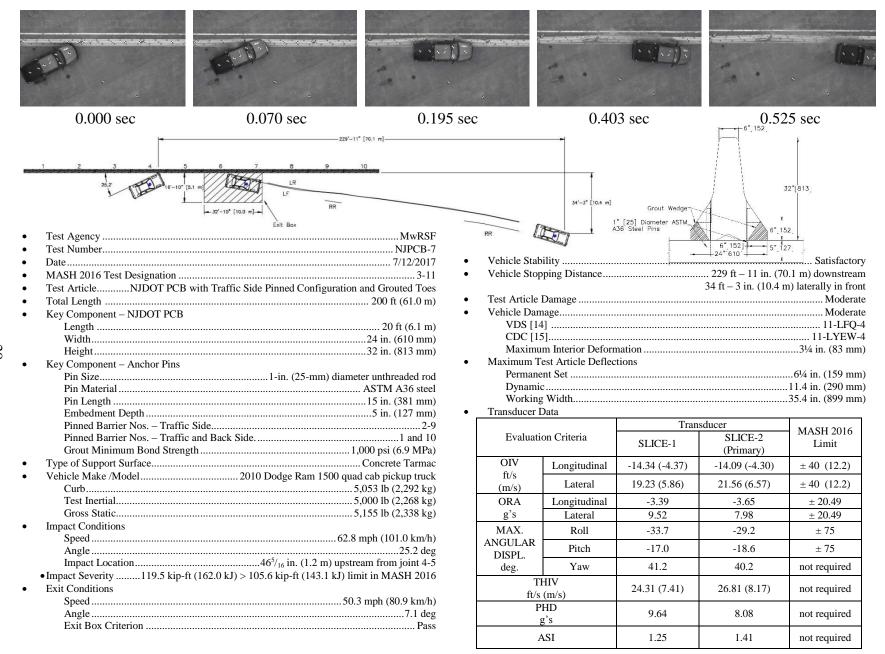


Figure 24. Summary of Test Results and Sequential Photographs, Test No. NJPCB-7

38



0.000 sec



0.084 sec



0.198 sec



0.330 sec



0.526 sec



0.658 sec



0.000 sec



0.144 sec



0.206 sec



0.290 sec

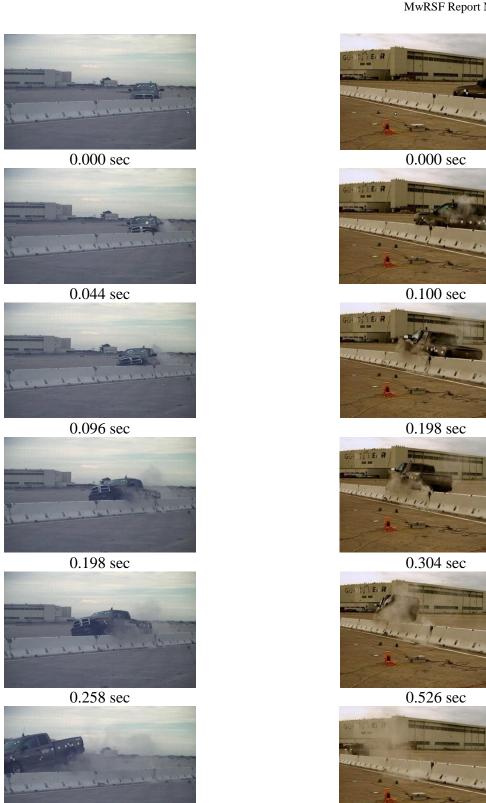


0.722 sec



0.830 sec

Figure 25. Additional Sequential Photographs, Test No. NJPCB-7



0.526 sec

1.326 sec





Figure 27. Documentary Photographs, Test No. NJPCB-7



Figure 28. Documentary Photographs, Test No. NJPCB-7



Figure 29. Documentary Photographs, Test No. NJPCB-7

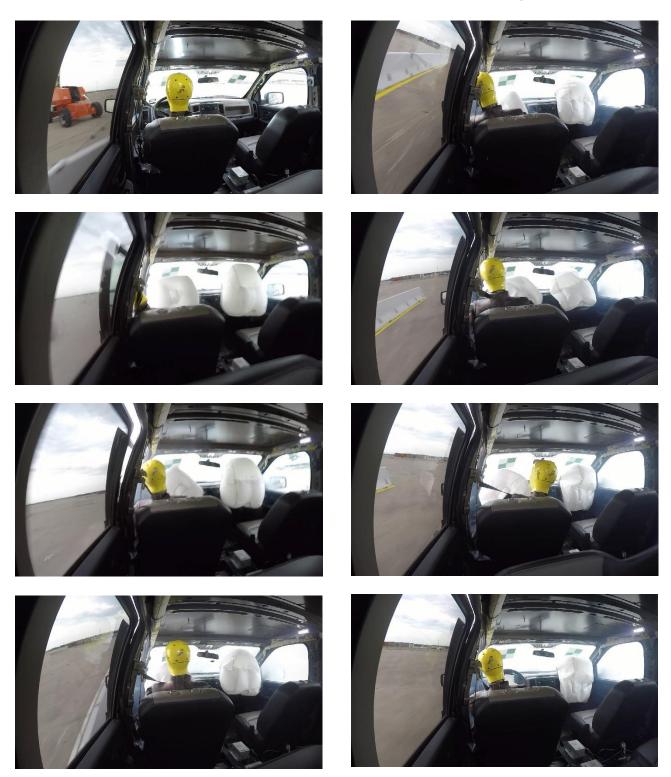


Figure 30. Documentary Photographs, Test No. NJPCB-7

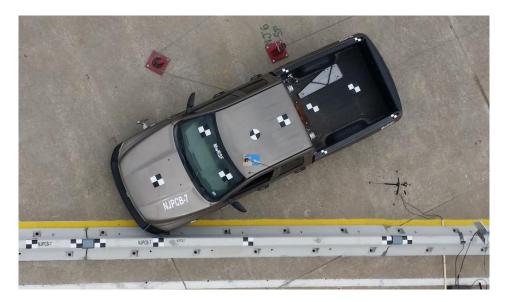






Figure 31. Impact Location, Test No. NJPCB-7



Figure 32. Vehicle Final Position and Trajectory Marks, Test No. NJPCB-7



Figure 33. System Damage - Front, Back, Upstream and Downstream Views, Test No. NJPCB-7





Figure 34. Barrier No. 3 – Traffic and Back Side Damage, Test No. NJPCB-7

December 18, 2018 MwRSF Report No. TRP-03-374-18





Figure 35. Barrier Nos. 4 and 5 Damage, Test No. NJPCB-7





(a) Traffic Side





(b) Back Side Figure 36. Barrier No. 4 – Traffic and Back Side Damage, Test No. NJPCB-7



(a) Traffic Side



(b) Back Side

Figure 37. Barrier No. 5 - Traffic and Back Side Damage, Test No. NJPCB-7



(b) Back Side

Figure 38. Barrier No. 6 – Traffic and Back Side Damage, Test No. NJPCB-7



Figure 39. Vehicle Damage, Test No. NJPCB-7



Figure 40. Vehicle Damage on Impact Side, Test No. NJPCB-7



Figure 41. Vehicle Windshield Damage, Test No. NJPCB-7



Figure 42. Occupant Compartment Deformation, Test No. NJPCB-7

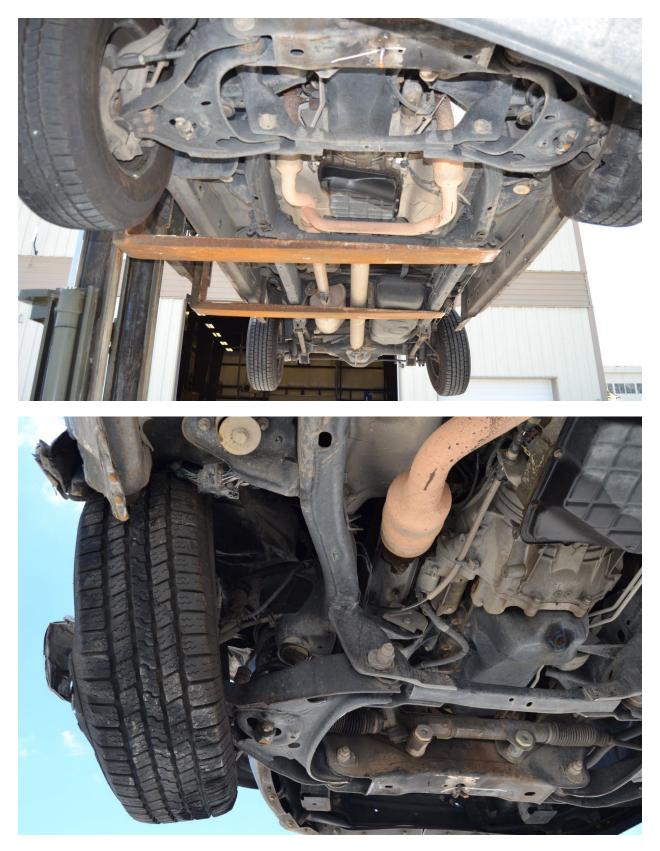


Figure 43. Undercarriage Damage, Test No. NJPCB-7

# 6 SUMMARY AND CONCLUSIONS

Test no. NJPCB-7 was conducted on the NJDOT PCB system with a traffic-side pinned configuration and grouted toes according to MASH 2016 test designation no. 3-11. This system uses NJDOT barriers, Type 4 (Alternative B). Barrier nos. 1 and 10 were anchored on both sides, and barrier nos. 2 through 9 were anchored to the concrete tarmac on the traffic side through pin anchor recesses with 1-in. (25-mm) diameter by 15-in. (381-mm) long, ASTM A36 steel pins. Non-shrink grout wedges were placed at the toe of each barrier segment in every joint between adjacent barrier segments on the traffic and back sides.

During test no. NJPCB-7, the 5,000-lb (2,268 kg) pickup truck impacted the NJDOT PCB system at a speed of 62.8 mph (101.0 km/h) and at an angle of 25.2 degrees, resulting in an impact severity of 119.5 kip-ft (162.0 kJ). After impacting the barrier system, the vehicle exited the system at a speed of 50.3 mph (80.9 km/h) and at an angle of 7.1 degrees. The vehicle was successfully contained and smoothly redirected with moderate damage to both the barrier and the vehicle. Barrier nos. 3, 4, 5, and 6 experienced spalling and cracking. A dynamic deflection of 11.4 in. (290 mm) and working width of 35.4 in. (899 mm) were observed during the test, as shown in Figure 23. All occupant risk values were found to be within limits, and the occupant compartment deformations were also deemed acceptable. Subsequently, test no. NJPCB-7 was determined to satisfy the safety performance criteria for MASH test designation no. 3-11. A summary of the test evaluation is shown in Table 9.

| Evaluation<br>Factors  |    | Evaluation Criteria  |                           |                    |      |  |  |  |  |
|------------------------|----|--|---------------------------|--------------------|------|--|--|--|--|
| Structural<br>Adequacy | А. | Test article should contain and redirect the vehicle or bring the vehicle<br>to a controlled stop; the vehicle should not penetrate, underride, or<br>override the installation although controlled lateral deflection of the test<br>article is acceptable. |                           |                    |      |  |  |  |  |
|                        | D. | 1. Detached elements, fragments or other debris from the test article<br>should not penetrate or show potential for penetrating the occupant<br>compartment, or present an undue hazard to other traffic, pedestrians,<br>or personnel in a work zone.       |                           |                    |      |  |  |  |  |
|                        |    | 2. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH 2016.  |                           |                    |      |  |  |  |  |
|                        | F. | The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.  |                           |                    |      |  |  |  |  |
| Occupant<br>Risk       | Н. | Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits:  |                           |                    |      |  |  |  |  |
|                        |    | Occupa   | nt Impact Velocity Limits | 5                  | S    |  |  |  |  |
|                        |    | Component  | Preferred                 | Maximum            |      |  |  |  |  |
|                        |    | Longitudinal and Lateral   | 30 ft/s (9.1 m/s)         | 40 ft/s (12.2 m/s) |      |  |  |  |  |
|                        | I. | The Occupant Ridedown<br>Section A5.2.2 of MAS<br>satisfy the following limit  | H 2016 for calculation    |                    |      |  |  |  |  |
|                        |    | Occupant R   | Ridedown Acceleration Li  | mits               | S    |  |  |  |  |
|                        |    | Component  | Preferred                 | Maximum            |      |  |  |  |  |
|                        |    | Longitudinal and Lateral   | 15.0 g's                  | 20.49 g's          |      |  |  |  |  |
|                        |    | MASH 2016 Test   | t Designation No.         |                    | 3-11 |  |  |  |  |
|                        |    | Final Evaluatio  | n (Pass or Fail)          |                    | Pass |  |  |  |  |
|                        | ç  | – Satisfactory U – I   | Insatisfactory NA - 1     | Not Applicable     | I    |  |  |  |  |

Table 9. Summary of Safety Performance Evaluation

S – Satisfactory U – Unsatisfactory NA - Not Applicable

#### 7 COMPARISON TO TEST NO. NYTCB-5

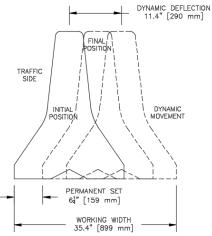
A summary of full-scale crash testing on the two pinned configurations with only one side of the NJ PCB system pinned, joint slack removed, and grouted toes is shown in Table 10. Test no. NJPCB-7 evaluated the use of steel pins placed through the front side of every barrier segment in order to anchor the PCBs and reduce barrier deflections. This test was compared to the NJ PCB system with only the back side pinned, joint slack removed, and grouted toes, corresponding to connection type C in the 2015 NJDOT *Roadway Design Manual* (test no. NJPCB-6) [16] and a similar New York PCB system also with only the back side pinned and without removal of joint slack or grouted toes (test no. NYTCB-5) [17]. Results from these tests included the actual impact conditions and impact severity as well as dynamic barrier deflection, permanent set barrier deflection, working width (as measured from the original front face of the barrier), and the clear space behind the barrier. The clear space behind the barrier is used by NJDOT to define the maximum deflection of the back of the barrier from its original position. In addition, the schematic diagrams shown in Figure 44 indicate how the dynamic deflection, permanent set deflection, and working width for each crash test was defined.

A review of the results from test nos. NJPCB-6, NJPCB-7, and NYTCB-5 would suggest that pinning the barriers on the front of the PCB segments provides two benefits as compared to pinning on only the back side. First, pinning the front of the PCBs produced lower deflections for test no. NJPCB-7 as compared to test no. NJPCB-6. Second, in both tests of the back-side pinned barriers, the impacting vehicle climbed the barrier face significantly and rolled away from the barrier face as it was redirected. This finding was due to the back-side pins providing increased constraint to the back of the PCB segments, thus causing increased barrier rotation, which promotes vehicle climb and instability. Test no. NJPCB-7 with the barrier pinned on the front face of the barrier showed improved vehicle stability with less roll and vehicle climb, while the vehicle was in contact with the barrier. Previous research by CALTRANS and MwRSF has noted that anchoring of PCB segments on the front side of the barrier improved stability as well. Thus, pinning the front side versus the back side of NJ PCB segments seems to be slightly more effective in reducing barrier deflections while providing improved vehicle stability.

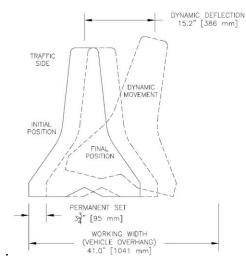
| Test No.        | Connection<br>Type [2] | System Details   | Permanent<br>Set   | Dynamic<br>Deflection<br>(DD) | Working<br>Width<br>(WW)          | Clear<br>Space<br>Behind<br>Barrier | Vehicle<br>Roll<br>(deg) | Vehicle<br>Pitch<br>(deg) | Vehicle<br>Mass<br>lb (kg) | Impact<br>Speed<br>mph<br>(km/h) | Impact<br>Angle<br>(deg) | Impact<br>Severity<br>kip-ft<br>(kJ) |
|-----------------|------------------------|--|--------------------|-------------------------------|-----------------------------------|-------------------------------------|--------------------------|---------------------------|----------------------------|----------------------------------|--------------------------|--------------------------------------|
| NJPCB-6<br>[16] | С                      | Barriers 1 and 10 pinned,<br>Barriers 2-9 pinned back<br>side only, remove slack,<br>grouted toes  | 3¾ in.<br>(95 mm)  | 15.2 in.<br>(386 mm)          | 41.0 in.<br>(1,041 mm)<br>Vehicle | 15.2 in.<br>(386 mm)                | 28.9                     | -12.2                     | 5,000<br>(2,268)           | 62.9<br>(101.3)                  | 25.1                     | 119.0<br>(161.3)                     |
| NYTCB-5<br>[17] | N/A                    | Barriers 1-10 pinned<br>back side only, slack not<br>removed, no grouted toes                      | 9 in.<br>(229 mm)  | 20.5 in.<br>(521 mm)          | 35.0 in.<br>(889 mm)              | 11 in.<br>(279 mm)                  | 41.8                     | -21.2                     | 4,953<br>(2247)            | 64.3<br>(103.5)                  | 26.2                     | 133.4<br>(180.9)                     |
| NJPCB-7         | N/A                    | Barriers 1 and 10 pinned,<br>Barriers 2-9 pinned front<br>side only, remove slack,<br>grouted toes | 6¼ in.<br>(159 mm) | 11.4 in.<br>(290 mm)          | 35.4 in.<br>(899 mm)              | 11.4 in.<br>(290 mm)                | -29.2                    | -18.6                     | 5,000<br>(2,268)           | 62.8<br>(101.0)                  | 25.2                     | 119.5<br>(162.0)                     |

# Table 10. Comparison of Pinned Systems on One Side Only

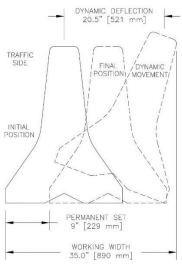
N/A = Not Applicable



NJPCB-7 - Only Front Side Pinned, Joint Slack Removed, Grouted Toes



NJPCB-6 - Only Back Side Pinned, Joint Slack Removed, Grouted Toes



NYTCB-5 - Only Back Side Pinned, Joint Slack Not Removed, No Grouted Toes

Figure 44. Deflection Comparisons - Test Nos. NJPCB-7, NJPCB-6 and NYTCB-5

### **8 MASH IMPLEMENTATION**

The objective of this research was to evaluate the safety performance of NJDOT's PCB system with a traffic-side pinned configuration and grouted toes. The NJDOT barriers, Type 4 (Alternative B), consisted of NJDOT PCBs joined with a connection key. Barrier nos. 1 and 10 were anchored to the concrete roadway surface through the nine pin anchor recesses with 1-in. (25-mm) diameter by 15-in. (381-mm) long, ASTM A36 steel pins. Barrier nos. 2 through 9 were anchored to the concrete surface through only the five traffic-side pin anchor recesses. The barrier segments were pulled in a direction parallel to their longitudinal axes, and slack was removed from all joints prior to installation of the steel anchor pins. A wedge of grout was placed at the toe of each joint on both the traffic side and back side of the system.

According to TL-3 evaluation criteria in MASH 2016, two tests are required for evaluation of longitudinal barrier systems: (1) test designation no. 3-10 - an 1100C small car and (2) test designation no. 3-11 - a 2270P pickup truck. However, only the 2270P crash test was deemed necessary as other prior small car tests were used to support a decision to deem the 1100C crash test not critical.

In test no. 7069-3, a rigid, F-shape bridge rail was successfully impacted by a small car weighing 1,800 lb (816 kg) at 60.1 mph (96.7 km/h) and 21.4 degrees according to the American Association of State Highway and Transportation Officials (AASHTO) *Guide Specifications for Bridge Railings* [5-6]. In the same manner, test nos. CMB-5 through CMB-10, CMB-13, and 4798-1 showed that rigid, New Jersey, concrete safety shape barriers struck by small cars have been shown to meet safety performance standards [7-9]. In addition, in test no. 2214NJ-1, a rigid, New Jersey, <sup>1</sup>/<sub>2</sub>-section, concrete safety shape barrier was impacted by a passenger car weighing 2,579 lb (1,170 kg) at 60.8 mph (97.8 km/h) and 26.1 degrees according to the TL-3 standards set forth in MASH 2009 [9]. Furthermore, temporary, New Jersey safety shape, concrete median barriers have experienced only slight barrier deflections when impacted by small cars and behave similarly to rigid concrete barriers as seen in test no. 47 [10]. Therefore, the 1100C passenger car test was deemed not critical for testing and evaluating this PCB system. It should be noted that any tests within the evaluation matrix deemed not critical may eventually need to be evaluated based on additional knowledge gained over time or additional FHWA eligibility letter requirements.

During test no. NJPCB-7, a 5,000-lb (2,268 kg) pickup truck with a simulated occupant seated in the left-front seat impacted the NJDOT PCB system at a speed of 62.8 mph (101.0 km/h) and at an angle of 25.2 degrees, resulting in an impact severity of 119.5 kip-ft (162.0 kJ). At 0.197 sec after impact, the vehicle became parallel to the system with a speed of 50.5 mph (81.3 km/h). At 0.290 sec, the vehicle exited the system at a speed of 50.3 mph (80.9 km/h) and at an angle of 7.1 degrees. The vehicle was successfully contained and smoothly redirected.

Exterior vehicle damage was moderate. Interior occupant compartment deformations were moderate with a maximum of 3¼ in. (83 mm), which did not violate the limits established in MASH 2016. Damage to the barrier was also moderate, consisting of contact and gouge marks on the front face of the PCB segments as well as concrete spalling, cracking, and fracture on barrier nos. 4 and 5. The maximum dynamic barrier deflection was 11.4 in. (290 mm), which included minor tipping of the barrier at the top surface. The working width of the PCB system was 35.4 in. (899 mm). All occupant risk measures were within the recommended limits, and the occupant compartment deformations were also deemed acceptable. Therefore, the NJDOT barriers, Type 4

(Alternative B) pinned only on the traffic side, successfully met all the safety performance criteria of MASH 2016 test designation no. 3-11.

The NJDOT barriers, Type 4 (Alternative B), consisting of NJDOT PCB barriers joined with a connection key, joint slack removed, grouted toes, barrier nos. 1 and 10 pinned on both the traffic side and back side, and barrier nos. 2 through 9 pinned only on the traffic side, were successfully crash tested and evaluated according to the AASHTO MASH 2016 TL-3 criteria. This barrier successfully met all the requirements of MASH 2016 test designation no. 3-11. In addition, the researchers consider the system MASH 2016 compliant based on the successful test designation no. 3-11 test and the previous justification for test designation no. 3-10 being deemed not critical.

A comparison of similar PCB systems with only one side of the system pinned included three systems: (1) a NJ PCB system with barrier nos. 1 and 10 pinned on both front and back sides, pin anchors only on the traffic side of barrier nos. 2 through 9, joint slack removed, and grouted toes (test no. NJPCB-7); (2) a NJ PCB system with barrier nos. 1 and 10 pinned on both front and back sides, pin anchors only on the back side of barrier nos. 2 through 9, joint slack removed, and grouted toes (test no. NJPCB-6) [16]; and (3) a New York PCB system with pin anchors only on the back side of all barriers and without removal of joint slack or grouted toes (test no. NYTCB-5) [17]. A review of these test results (test nos. NJPCB-6, NJPCB-7, and NYTCB-5) revealed benefits to pinning the barriers on the traffic side of the PCB segments when compared to pinning only n the back side. First, pinning the traffic side of the PCBs produced lower deflections for test no. NJPCB-7 as compared to test no. NJPCB-6. Second, in both tests of the back-side pinned barriers, the impacting vehicle climbed the barrier face significantly and rolled away from the traffic-side face of the barrier as it was redirected. This finding is primarily due to the back-side pins providing increased constraint to the back of the PCB segments, thus causing increased barrier rotation and subsequently, promotes vehicle climb and instability. In test no. NJPCB-7, the vehicle showed improved vehicle stability with less climb and roll when in contact with the pinned only on the traffic-side barrier. In addition, previous research by CALTRANS and MwRSF has noted that anchoring of PCB segments on the traffic side of the barrier improved stability as well. Thus, pinning only the traffic side of NJ PCB segments appears to be slightly more effective in reducing barrier deflections while providing improved vehicle stability.

Barrier system behavior and associated barrier deflections can vary from test to test due to the natural variability of a wide variety of factors involved in full-scale crash testing. These factors would include slight differences in impact conditions, differing test vehicle model years, slight variations in steel and concrete strengths, and variation of the cracking and damage observed on the barrier segments, among others. Thus, some variability would be expected in barrier performance even for basically identical systems.

In both the 2013 and 2015 NJDOT *Roadway Design Manual*, the allowable deflection is determined by the clear space behind the barrier, which is defined as the maximum deflection of the back of the barrier from its original position. For this test, the clear space behind the barrier was 11.4 in. (290 mm).

### **9 REFERENCES**

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### **10 APPENDICES**

## Appendix A. NJDOT PCB Standard Plans

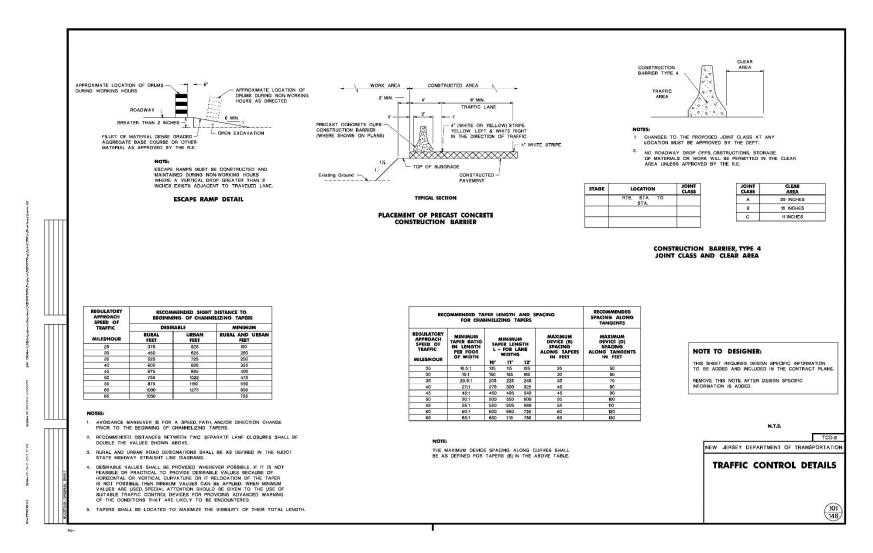


Figure A-1. NJDOT PCB Standard Plans

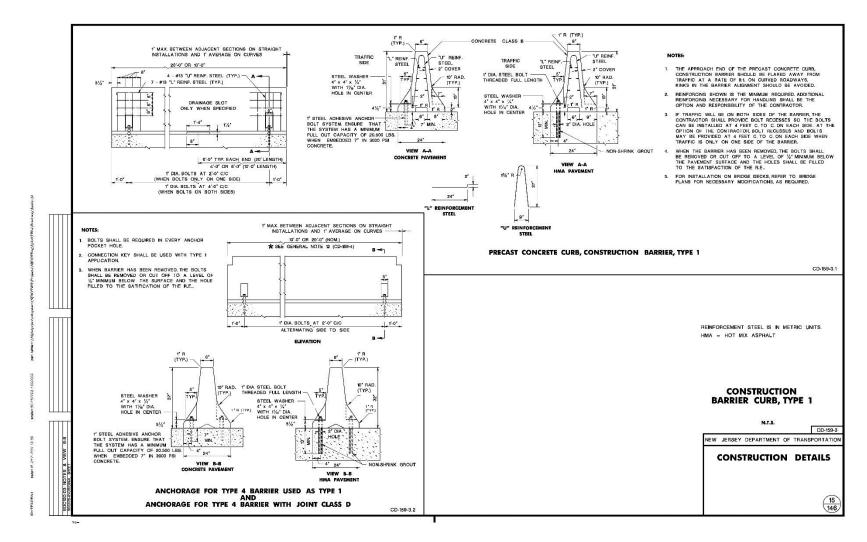


Figure A-2. NJDOT PCB Standard Plans

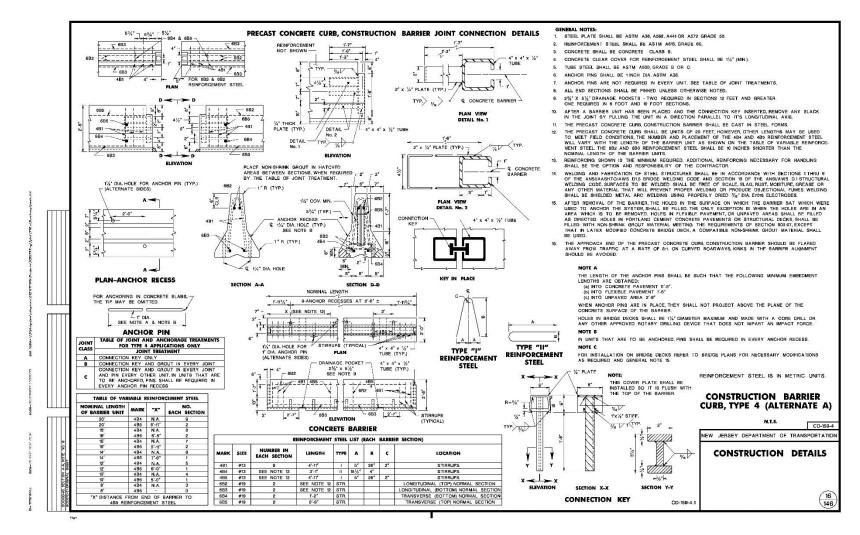
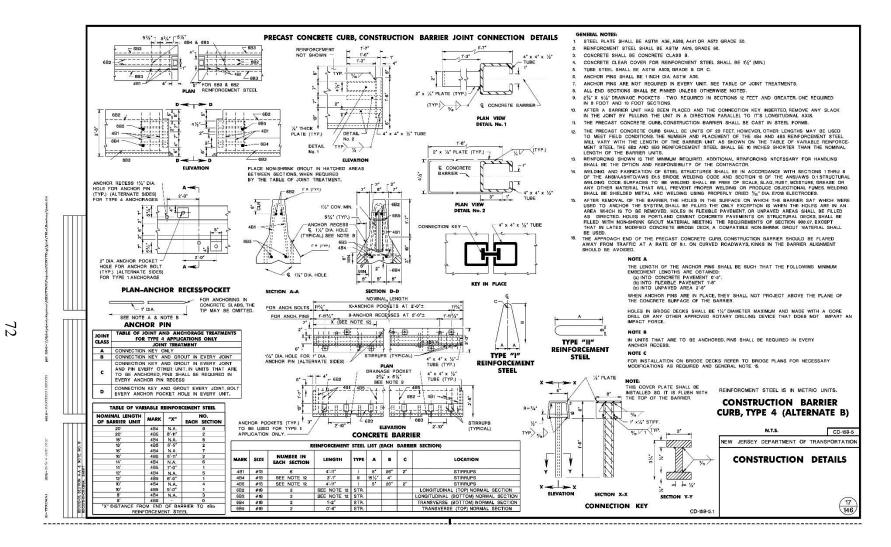


Figure A-3. NJDOT PCB Standard Plans





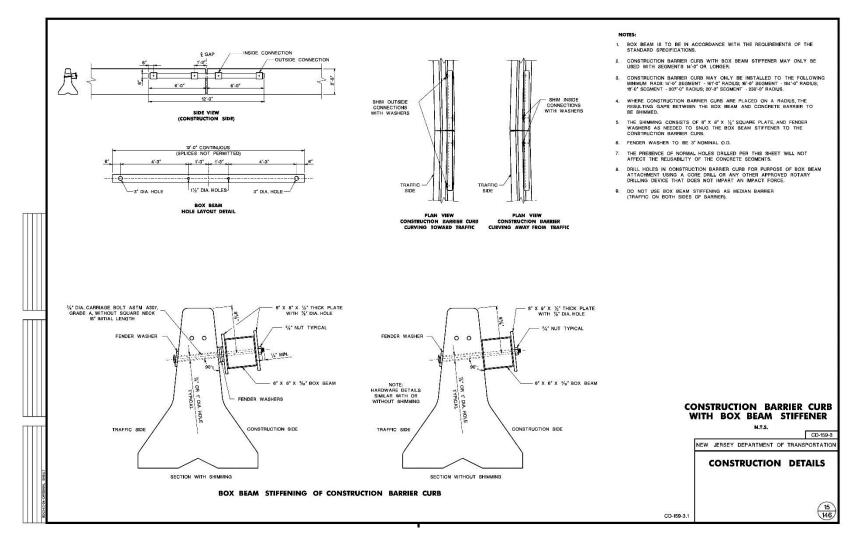


Figure A-5. NJDOT PCB Standard Plans

## Appendix B. Material Specifications

| Table B-1. Bill of Materials, Test No. NJPCB-7 |
|--|
|--|

| Item No. | Description  | Material Specification                                 | Reference   |
|----------|--|--|---|
| A1       | Concrete Barrier Segment   | Min. f 'c = 3,700 psi (25.5 MPa)                       | KU3325  |
| A2       | Anchor Steel Pin   | ASTM A36   | Heat #54153853  |
| B1       | Rebar - #4 Vertical Stirrup  | ASTM A615 Gr. 60                                       | Heat #JL1000, JK9068, 61108687                                  |
| B2, B3   | Rebar - #6 Longitudinal Bar  | ASTM A615 Gr. 60                                       | Heat #61110285, 61110265, JL3511,<br>JL3506, JL3505             |
| B4       | Rebar - #4 Horizontal Anchor Recess,<br>Reinforcement Stirrup                    | ASTM A615 Gr. 60                                       | Heat #JL1000, JK9068, 61108687                                  |
| B5       | Rebar - #6 Top and Bottom Cross Bar  | ASTM A615 Gr. 60                                       | Heat #61110285, 61110265, JL3511,<br>JL3506, JL3505             |
| C1       | Steel Tube $-4"\times4"\times1_{2}"$<br>(102×102×12.7) thick × 20" (508)<br>long | ASTM A500 Gr. B and C                                  | Heat #SF1424, SF4193  |
| C2       | Bent Steel Plate 1, 2"×1/4"  | ASTM A36   | Heat #269878  |
| C3       | Bent Steel Plate 2, 2"×1/4"  | ASTM A36   | Heat #269878  |
| D1       | Steel Plate 1, 2"×1/2"   | ASTM A36   | Heat #54148807  |
| D2       | Steel Plate 2, 2 <sup>1</sup> / <sub>4</sub> "× <sup>1</sup> / <sub>2</sub> "    | ASTM A36   | Heat #54148805  |
| D3       | <sup>1</sup> / <sub>2</sub> " (13) Steel Plate – Stiffener                       | ASTM A36   | Heat #SF2550  |
| D4       | <sup>1</sup> / <sub>2</sub> " (13) Steel Plate – Top Plate                       | ASTM A36   | Heat #SF2550  |
| E1       | Non-Shrink Grout   | Min. 1-day Compressive Strength<br>1,000 psi (6.9 MPa) | Advantage Grout ASTM C1107<br>Product Code: 67435, R#2147369273 |

# KU3325 Midwest Roadside Safety University of Nebraska

# 20' Temporary Barrier with socket and key connection

| Production<br>date | Quantity<br>to ship | Cylinder Breaks<br>3 Day Results |
|--------------------|---------------------|----------------------------------|
| 5-1-17B            | 3                   | 5199                             |
| 4-13-17B           | 1                   | 5130                             |
| 4-28-17B           | 3                   | 5024                             |
| 4-27-17B           | 3                   | 4834                             |
| 4-27-17A           | 3                   | 4697                             |
| 4-26-17A           | 3                   | 5134                             |
| 4-25-17B           | 3                   | 5516                             |
| 4-25-17A           | 1                   | 5223                             |

Figure B-2. Concrete Barrier Segment – Concrete Strength, Test No. NJPCB-7

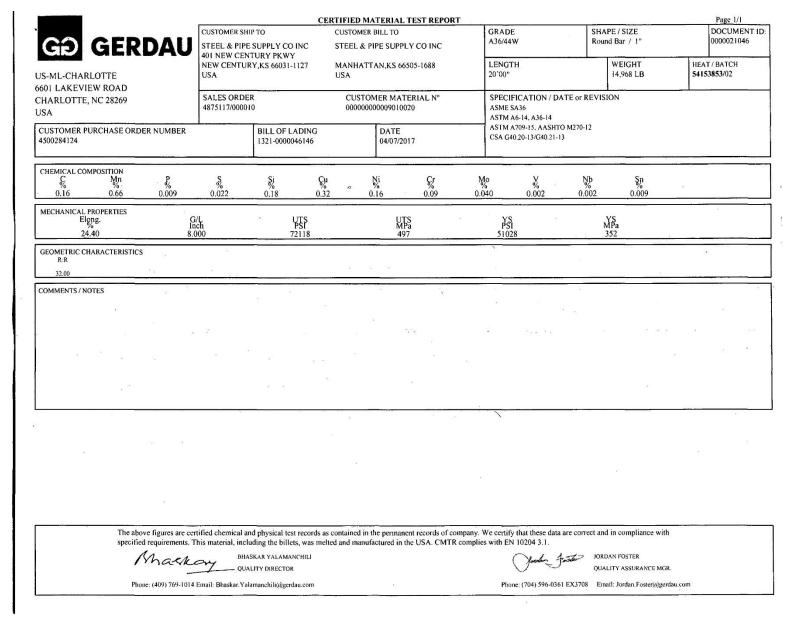


Figure B-3. Anchor Pins Material Certificate, Test No. NJPCB-7



P.O. Box 13948 Roanoke, VA 24038-3934

Office: (540) 342-1831 (800) 753-3532 Fax: (540) 342-9437 www.roanokesteel.com

### PRODUCT CERTIFICATION

 MFG LOT NBR
 HEAT NUMBER

 JL1000-376202
 JL1000

 BILL OF LADING
 SALES ORDER/LINE

 00514980
 121669 / 001

 CERT ID / REV
 00049973 / 01

SOLD TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA SHIP TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA

| CUSTOMER P.O.<br>8495 |                           | CUSTOMER PART<br>N/A |                                | RT                           | QUANTITY<br>25,956     | BUNDI<br>3                    |              |           | PIECES       | GRADE<br>A615-6 | 0           | SHIPMENT DAT<br>12/12/2016  |  |
|-----------------------|---------------------------|----------------------|--------------------------------|------------------------------|------------------------|-------------------------------|--------------|-----------|--------------|-----------------|-------------|---|--|
| PART NUMB             | ER: R                     | B01979               | 6000CA                         |                              | DESCRIPTION            | N: I                          | Rebar #      | 06 (1     | 9) 60'0      | " A615-60       | )           |   |  |
|                       | Alternation of the second |                      |                                |                              | A                      | It Certs                      |              |           |              |                 |             |   |  |
| STM A615/             | A615M-16                  | GR60                 | AASHTO                         | M31/M31                      | M-15 GR60              |                               |              |           |              |                 |             |   |  |
|                       |                           |                      |                                |                              | C                      | hemical                       |              |           |              |                 |             |   |  |
| C<br>0.42             | Mn<br>1.02                | S<br>0.043           | P<br>0.012                     | Si<br>0.26                   |                        | Ni<br>0.10                    | Мо<br>0.03   | 0.2       | Cu<br>26 0.  | V<br>003 0.0    | Nb<br>001   | CE<br>0.68  |  |
|                       |                           |                      |                                |                              | Yield Ten              | sile Elo                      | ngation      |           |              |                 |             |   |  |
| ample-1               | Yld-1                     | (KSI)<br>64.8        | ¥ld-1                          | (MPa)<br>447                 | Ultimate-1             | (KSI)<br>103.4                | Ultima       | ate-1     | (MPa)<br>713 | Elong8'         | ' (%)<br>18 |   |  |
| ample-2               | Yld-2                     | (KSI)<br>64.3        | ¥ld-2                          | (MPa)<br>443                 | Ultimate-2             | (KSI)<br>102.2                | Ultima       | ate-2     | (MPa)<br>705 | Elong8'         | (%)<br>16.6 |   |  |
|                       |                           |                      |                                |                              | Me                     | chanica                       | I            |           |              |                 |             |   |  |
| EST                   |                           |                      |                                | RESU                         | JLT                    | Weige the second              |              |           |              |                 |             |   |  |
|                       |                           |                      |                                |                              |                        |                               |              |           |              |                 |             |   |  |
| ordered" Grade        | Mercury, Radi             | units or SI L        | Alpha source<br>mits are to be | materials in a regarded as a | any form have not be   | en used in th<br>n the ASTM s | e production | of this n | naterial. No | Weld repair has | s been per  | mace process(es) to mee<br>rformed. Any tensile valu<br>less a metric specification |  |
| his is to certify     | the above to be           | a true and           | accurate ropo                  | rt as containe               | d in the records of th | nis company.                  |              |           |              |                 |             | A Carlo Martine San                             |  |
| END OF                | CERTIFIC                  | CATION               |                                | 7                            | . 2. 1                 | the f                         | 1            | [         | Enginee      | er of Tests:    | Lev         | vis E. Leftwich J   |  |
| c302 (v6.0)           |                           |                      |                                |                              |                        | Page 1 of                     | 1            |           |              |                 | Da          | te Printed: 12/12/  |  |

Figure B-4. Rebar No. 4 Material Certificate, Test No. NJPCB-7



Metal Partners International

55 South Main Street

Naperville, IL 60540

SOLD TO

Suite 304

USA

P.O. Box 13948 Roanoke, VA 24038-3934

Office: (540) 342-1831 (800) 753-3532 Fax: (540) 342-9437 www.roanokesteel.com PRODUCT CERTIFICATION

MFG LOT NBR HEAT NUMBER JK9068-171121 JK9068 BILL OF LADING SALES ORDER/LINE 00505081 105043 / 002 CERT ID / REV 00014678 / 01

SHIP TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA

CUSTOMER P.O. CUSTOMER PART QUANTITY BUNDLE(S) TOTAL PIECES GRADE SHIPMENT DATE 5410 17,304 192 A615-60 05/05/2016 N/A 2 PART NUMBER RB019796000CA DESCRIPTION Rebar # 06 (19) 60'0" A615-60 Alt Certs ASTM A615/A615M-16 GR60 | AASHTO M31/M31M-15 GR60 Chemical C Mn S P Si Cr Ni Mo Cu V Nb 0.44 1.02 0.028 0.015 0.24 0.16 0.09 0.02 0.36 0.003 0.002 CE 0.71 Yield Tensile Elongation Yld-1 (KSI) Ultimate-1 (KSI) Yld-1 (MPa) Ultimate-1 (MPa) % Elong (%) Sample-1 69.5 479 109.3 754 17.5 Yld-2 (KSI) Yld-2 (MPa) Ultimate-2 (KSI) Ultimate-2 (MPa) % Elong (%) Sample-2 68.8 475 109.5 755 16.3 Mechanical TEST RESULT **Bend Test** Pass Approved ABS QA Mill. Certificate No. 12-MMPQA-676. This Material was melted and manufactured in our plant located in Roanoke, VA, USA, by basic Electric Furnace process(es) to meet the "ordered" Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weld repair has been performed. Any tensile values stated herein either inch-pound units or SI units are to be regarded as separate as defined in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is ordered, this material has been tested and meets the requirements of the inch-pound ranges. This is to certify the above to be a true and accurate report as contained in the records of this company 5.2.5 END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr. qtc302 (v6.0) Page 1 of 1 Date Printed: 05/05/2016

Figure B-5. Rebar No. 4 Material Certificate, Test No. NJPCB-7

|  |  |  |  | CERTIFIED MA   | TERIAL TEST I            | REPORT          |                               |   |                                      | Page 1/1                                 |  |
|--|--|--|--|--|--------------------------|-----------------|-------------------------------|---|--------------------------------------|--|--|
| ତ୍ରେ ଜା  | ERDAU  | CUSTOMER SHI<br>TYE BAR LLC<br>1050 OHIO AV<br>GLASSPORT,F | Е  | CUSTOMER B<br>TYE BAR LL<br>1050 OHIO A<br>GLASSPORT | LC                       |                 | GRADE<br>60 (420)<br>LENGTH   |   | PE / SIZE<br>r / #5 (16MM)<br>WEIGHT | DOCUMENT II<br>00000000000<br>HEAT/BATCH |  |
| JS-ML-SAYREVILL  |  | USA  |  | USA  | USA                      |                 |                               |   | 8,636 LB                             | 61108687/02                              |  |
| NORTH CROSSMAN<br>SAYREVILLE, NJ 08<br>JSA                       |  | SALES ORDEI<br>4209659/00001                               |  | CUSTOM   | CUSTOMER MATERIAL Nº     |                 |                               | SPECIFICATION / DATE or REVISION<br>ASTM A615/A615M-15 E1 |                                      |  |  |
| CUSTOMER PURCHA<br>160122  | SE ORDER NUMBER  |  | BILL OF LADING<br>1331-0000048641          |  | DATE<br>09/15/2016       |                 |                               |   |                                      |  |  |
|  | DN<br>In P<br>% %<br>62 0.012  | %<br>0.061   | Si Q<br>%<br>0.19 0.                       | Cu N<br>% %<br>31 0.1                                | li Ç<br>17 0.1           |                 |                               | %<br>0.015  | CEqyA706<br>0.56                     |  |  |
| MECHANICAL PROPERT<br>YS<br>PSI<br>65742<br>64419                | TIES<br>MI<br>45<br>44   | 3  | UTS<br>PSI<br>97290<br>96645               |  | UTS<br>MPa<br>671<br>666 |                 | G/L<br>Inch<br>8.000<br>8.000 | 20  | i/L<br>im<br>0.0<br>0.0              |  |  |
| MECHANICAL PROPERT<br>Elong.<br>15.00<br>15.00                   | TES Bend<br>OF<br>OF   |  |  |  |                          | a.              |                               |   |                                      |  |  |
| GEOMETRIC CHARACTH<br>%Light Def<br>% In<br>4,50 0.0<br>4,60 0.0 | Hgi Def Gap<br>ch Inch<br>35 0.095                                     | DefSpace<br>Inch<br>0.400<br>0.400                         |  |  | 1                        |                 |                               |   |                                      |  |  |
| OMMENTS / NOTES  |  |  |  |  |                          |                 |                               |   |                                      |  |  |
|  |  |  |  |  |                          |                 |                               |   |                                      |  |  |
|  |  |  |  |  |                          |                 |                               |   |                                      |  |  |
|  |  |  |  |  |                          |                 |                               |   |                                      |  |  |
|  | The above figures are certil<br>specified requirements. This<br>Macked | is material, includ  | ing the billets, was me<br>AR YALAMANCHILI |  |                          | CMTR complies v |                               |   | і Т НОМІС                            |  |  |
|  |  | QUALI  | TY DIRECTOR                                |  |                          | 0               |                               | QUALF   | FY ASSURANCE MGR.                    |  |  |

Figure B-6. Rebar No. 4 Material Certificate, Test No. NJPCB-7

| ලො   | GERI   | DAU                               | CUSTOMER SH<br>TYE BAR LLC<br>1050 OHIO AV | 1                         | CI<br>T                    | FIED MATE<br>JSTOMER BILL<br>YE BAR LLC<br>50 OHIO AVE |   | RT            | GRAD<br>60 (420             |                                  |                 | APE / SIZE<br>par / #6 (19MM)     | Page 1/1<br>DOC UMENT<br>0000000000 |
|--|--|-----------------------------------|--|---------------------------|----------------------------|--|---|---------------|-----------------------------|----------------------------------|-----------------|-----------------------------------|-------------------------------------|
| US-ML-SAYRI<br>NORTH CROS                    |  |                                   | GLASSPORT,I<br>USA                         | PA 15045-1675             | GI                         | LASSPORT,P/<br>SA                                      |   |               | LENGTH<br>41'00"            |                                  |                 | WEIGHT<br>9,606 LB                | HEAT / BATCH<br>61110285/09         |
| SAYREVILLE.<br>JSA                           |  |                                   | SALES ORDE<br>4699099/00002                |                           |                            | CUSTOMER   | MATERIAL Nº                               |               |                             | FICATION / DA<br>A615/A615M-15 E |                 | SION                              |                                     |
| CUSTOMER PU<br>170014                        | JRCHASE ORDE                                       | R NUMBER                          |  | BILL OF LA<br>1331-000005 |                            |  | ATE<br>/13/2017                           |               |                             |                                  |                 |                                   |                                     |
| CHEMICAL COM<br>C<br>%<br>0.45               | 1POSITION<br>Mn<br>%<br>0.64                       | P<br>%<br>0.014                   | S<br>%<br>0.041                            | Si<br>%<br>0.20           | Cu<br>%<br>0.28            | Ni<br>%<br>0.14  | Çr<br>0.21                                | M<br>%<br>0.0 |                             | Տր<br>0.011                      | %<br>0.019      | CEqvA706<br>%<br>0.61             |                                     |
| MECHANICAL P<br>PS<br>686<br>685             | S<br>51<br>669                                     | Y<br>MI<br>47<br>47               | S.<br>3<br>2                               | U<br>F<br>10:<br>10:      | TTS<br>951<br>2440<br>2170 |  | UTS<br>MPa<br>706<br>704                  |               | G/L<br>Incl<br>8.00<br>8.00 | 0                                | 2               | G/L<br>mm<br>200.0<br>200.0       |                                     |
| MECHANICAL P<br>Elg<br>13.<br>13.            | ng.<br>00  | Bend<br>Ol<br>Ol                  | ĸ  |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
| GEOMETRIC CH.<br>%Light<br>%<br>4.00<br>4.10 | ARACTERISTICS<br>Def Hgt<br>Inch<br>0.051<br>0.051 | Def Gap<br>Inch<br>0.074<br>0.074 | DefSpace<br>Inch<br>0.453<br>0.453         |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
| OMMENTS / NO                                 | TES  |                                   | internation and and and an                 |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
|  |  |                                   |  |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
|  |  |                                   |  |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
|  |  |                                   |  |                           |                            |  |   |               |                             |                                  |                 |                                   |                                     |
|  |  |                                   |  |                           |                            |  | nanent records of con<br>in the USA. CMTR |               |                             |                                  | e correct and i | in compliance with                |                                     |
|  |  | hacke                             | BHASI                                      | KAR YALAMANCI             |                            |  |   |               |                             | 1 Khom                           | JOSEF<br>QUAL   | PH T HOMIC<br>.TTY ASSURANCE MGR. |                                     |
|  | Phone:   | (409) 769-1014 Er                 | nail: Bhaskar.Yalan                        | nanchili@gerdau.          | com                        |  |   |               | Phone                       | 2: 732 259 7660                  | Email: joe.hom  | ic@gerdau.com                     |                                     |

Figure B-7. Rebar No. 6 Material Certificate, Test No. NJPCB-7

|   |   |                                   |   |                          | CERT                      | IFIED MATERIAL                                   | TEST REPO       | RT             |  |                  |                                 | Page 1/1                  |
|---|---|-----------------------------------|---|--------------------------|---------------------------|--|-----------------|----------------|--|------------------|---------------------------------|---------------------------|
| GÐ  | GER   | DAU                               | CUSTOMER SHI<br>TYE BAR LLC<br>1050 OHIO AV | E                        | T<br>I                    | USTOMER BILL TO<br>YE BAR LLC<br>050 OHIO AVE    |                 |                | GRADE<br>60 (420)                      |                  | PE / SIZE<br>r / #5 (16MM)      | DOCUMENT ID<br>0000000000 |
| US-ML-SAYR<br>NORTH CROS                    |   |                                   | GLASSPORT,F<br>USA                          | PA 15045-1675            |                           | ELASSPORT,PA 1504<br>ISA                         | 5-1675          |                | LENGTH<br>41'00''                      |                  | WEIGHT<br>35,576 LB             | HEAT/BATCH<br>61110265/06 |
| SAYREVILLE<br>USA                           |   |                                   | SALES ORDER<br>4699099/000010               |                          |                           | CUSTOMER MAT                                     | ERIAL Nº        |                | SPECIFICATION / I<br>ASTM A615/A615M-1 | ON               |                                 |                           |
| CUSTOMER P<br>170014                        | URCHASE ORD   | ER NUMBER                         | 1   | BILL OF LA<br>1331-00000 |                           | DATE<br>02/13/20                                 | 17              |                |  |                  |                                 |                           |
| CHEMICAL CON<br>C<br>%<br>0.48              | MPOSITION<br>Mn<br>%<br>0.63                        | Р<br>%<br>0.010                   | %<br>0.030                                  | Si<br>%<br>0.18          | Cu<br>%<br>0.34           | Ni<br>%<br>0.13                                  | Cr<br>%<br>0.13 | M<br>%<br>0.0. | o Sn<br>32 0.012                       | V<br>%<br>0.012  | CEqvA706<br>0.60                | 4                         |
| MECHANICAL I<br>P<br>67<br>66               | 'S<br>SI<br>134                                     | MI<br>46<br>46                    | 3   | 10                       | TTS<br>SI<br>2850<br>1950 | UT:<br>MP<br>709<br>703                          | )               |                | G/L<br>Inch<br>8.000<br>8.000          | 20               | i/L<br>im<br>0.0<br>0.0         |                           |
| MECHANICAL I<br>Elç<br>13<br>13             | 2018.<br>.00  | Bend<br>Of<br>Of                  | <   |                          |                           |  |                 |                |  |                  |                                 |                           |
| GEOMETRIC CH<br>%Light<br>%<br>4.50<br>4.70 | IARACTERISTICS<br>Def Hgt<br>Inch<br>0.033<br>0.033 | Def Gap<br>Inch<br>0.130<br>0.130 | DefSpace<br>Inch<br>0.400<br>0.400          | -                        |                           |  |                 |                |  |                  |                                 |                           |
| COMMENTS / NO                               | DTES  |                                   |   |                          |                           |  |                 |                |  |                  |                                 |                           |
|   |   |                                   |   |                          |                           |  |                 |                |  |                  |                                 |                           |
|   |   |                                   |   |                          |                           |  |                 |                |  |                  |                                 |                           |
|   |   |                                   |   |                          |                           |  |                 |                |  |                  |                                 |                           |
|   |   |                                   |   |                          |                           |  |                 |                |  |                  |                                 |                           |
|   |   |                                   | is material, includ                         | ing the billets,         | was melted ar             | ained in the permanent<br>ad manufactured in the |                 | complies v     |  |                  |                                 |                           |
|   | 19  | hacke                             | Pres  | CAR YALAMANC             | HILI                      |  |                 | 0              | longa 1 Kom                            | QUALI            | I T HOMIC<br>I'Y ASSURANCE MGR. |                           |
|   | Phone   | e: (409) 769-1014 Er              | nail: Bhaskar.Yalan                         | nanchili@gerdau          | .com                      |  |                 |                | Phone: 732 259 7660                    | Email: joe.homic | @gerdau.com                     |                           |

Figure B-8. Rebar No. 6 Material Certificate, Test No. NJPCB-7



P.O. Box 13948 Roanoke, VA 24038-3934 Office: (540) 342-1831

Office: (540) 342-1831 (800) 753-3532 Fax: (540) 342-9437 www.roanokesteel.com PRODUCT CERTIFICATION

MFG LOT NBR HEAT NUMBER JL3511-479027 JL3511 BILL OF LADING SALES ORDER/LINE 00520094 129426 / 001 CERT ID / REV 00063374 / 01

SOLD TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA SHIP TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA

| CUSTOMER P.O.<br>9579  |   | CUSTOMER PART<br>N/A                          |  | QUANTITY<br>17,315                           |                      | DLE(S)<br>3                       |                               | PIECES<br>32 | GRADE<br>A615-60 | SHIPMENT DA<br>0 03/08/2017 |             |   |
|--|---|---|--|--|----------------------|-----------------------------------|-------------------------------|--------------|------------------|-----------------------------|-------------|---|
| PART NUMBE   | R: <b>R</b>                                     | B019776                                       | 5000CA   |  | DESCRIPTIO           | N :                               | Rebar                         | # 04 (1      | 3) 60'0'         | ' A615-60                   |             |   |
|  |   |   |  |  | C                    | hemica                            | al                            |              |                  |                             |             |   |
| C<br>0.41  | Mn<br>1.05                                      | S<br>0.024                                    | P<br>0.012                                       | Si<br>0.22                                   | Cr<br>0.16           | Ni<br>0.10                        | Mo<br>0.02                    | 0,2          | Cu<br>21 0.0     | V 0.0                       | ND<br>01    | CE<br>0.68  |
|  |   |   |  |  | Yield Ter            | sile Ele                          | ongatio                       | n            |                  |                             |             |   |
| Sample-1   | Yld-1   | (KSI)<br>68.9                                 | Yld-1  | (MPa)<br>475                                 | Ultimate-1           | (KSI)<br>107.6                    | Ultin                         | nate-1       | (MPa)<br>742     | Elong8"                     | (%)<br>15.6 |   |
| Sample-2   | Yld-2   | (KSI)<br>69.5                                 | Yld-2  | (MPa)<br>479                                 | Ultimate-2           | (KSI)<br>108.2                    | Ultir                         | nate-2       | (MPa)<br>746     | Elong8"                     | (%)<br>14   |   |
|  |   |   |  |  | Me                   | chanic                            | al                            |              |                  |                             |             |   |
| TEST<br>Bend Test  |   |   |  | Pass   |                      |                                   |                               |              |                  |                             |             |   |
| "ordered" Grade.<br>stated herein eith<br>ordered, this mate | Mercury, Rad<br>er Inch-pound<br>erial has been | ium or other<br>units or SI u<br>tested and m | Alpha source<br>hits are to be<br>leets the requ | materials in<br>regarded as<br>irements of t | any form have not be | een used in<br>In the ASTN<br>IS. | the producti<br>scope for the | on of this n | naterial. No     | Weld repair has             | been pe     | rnace process(ee) to meet<br>rformed. Any tensile value<br>rless a metric specification |
| END OF   | CERTIFIC  | CATION  |  | 7  | . 2                  | the fill                          | 1                             |              | Enginee          | r of Tests:                 | Lev         | wis E. Leftwich Jr.   |
| qtc302 (v6.0)  |   |   |  |  |                      | Page 1 c                          | of 1                          |              | a a Alfan ana    |                             | Di          | ate Printed: 03/08/2  |

Figure B-9. Rebar No. 6 Material Certificate, Test No. NJPCB-7



Metal Partners International

55 South Main Street

Naperville, IL 60540

SOLD TO

Suite 304

USA

P.O. Box 13948 Roanoke, VA 24038-3934

### PRODUCT CERTIFICATION

| fice:  | (540) 342-1831 |
|--------|----------------|
|        | (800) 753-3532 |
| x:     | (540) 342-9437 |
| ww.roa | anokesteel.com |

MFG LOT NBR HEAT NUMBER JL3506-479027 JL3506 BILL OF LADING SALES ORDER/LINE 00520481 130004 / 001 CERT ID / REV 00064145 / 01

SHIP TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA

CUSTOMER P.O. CUSTOMER PART BUNDLE(S) TOTAL PIECES GRADE SHIPMENT DATE QUANTITY 9726 N/A 15,390 384 A615-60 03/13/2017 2 PART NUMBER RB019776000CA DESCRIPTION : Rebar # 04 (13) 60'0" A615-60 Chemical Si Cr Cu Nb CE C Mn S P Ni Mo V 0.42 1.11 0.025 0.010 0.24 0.11 0.09 0.02 0.21 0.003 0.001 0.69 Yield Tensile Elongation Yld-1 (KSI) Yld-1 (MPa) Ultimate-1 (KSI) Ultimate-1 (MPa) Elong8" (%) 105.2 Sample-1 467 725 15.6 67.7 Yld-2 (KSI) Yld-2 (MPa) Ultimate-2 (KSI) Ultimate-2 (MPa) Elong8" (%) Sample-2 482 109.0 752 15.6 69.9 Mechanical TEST RESULT **Bend Test** Pass Approved ABS QA Mill. Certificate No. 12-MMPQA-676. This Material was melted and manufactured in our plant located in Roanoke, VA, USA, by basic Electric Furnace process(es) to meet the "ordered" Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weld repair has been performed. Any tensile values stated herein either inch-pound units or SI units are to be regarded as separate as defined in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is ordered, this material has been tested and meets the requirements of the inch-pound ranges. rtify the above to be a true and accurate report as contained in the records of this J. E. G. END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr. qtc302 (v6.0) Page 1 of 1 Date Printed: 03/13/2017

Figure B-10. Rebar No. 6 Material Certificate, Test No. NJPCB-7



SOLD TO

Suite 304

USA

Metal Partners International

55 South Main Street

Naperville, IL 60540

P.O. Box 13948 Roanoke, VA 24038-3934

Office: (540) 342-1831 (800) 753-3532 Fax: (540) 342-9437 www.roanokesteel.com

### PRODUCT CERTIFICATION

 MFG LOT NBR
 HEAT NUMBER

 JL3505-479027
 JL3505

 BILL OF LADING
 SALES ORDER/LINE

 00520481
 130004 / 001

 CERT ID / REV
 00064144 / 01

SHIP TO Metal Partners International 55 South Main Street Suite 304 Naperville, IL 60540 USA

| Y1d-2 (KST)       Y1d-2 (MPa)       Ultimate-2 (KST)       Ultimate-2 (MPa)       Elong#" (%)         mple-2       69.5       473       110.7       763       14.4         Mechanical         ESI       ESUT         Etend Test       Pass  | CUSTOMER P.O.<br>9726 |                  |              | CUSTOME<br>N/ |                |                     | NTITY<br><b>,540</b> | BUNDLE(S              | i) T      | OTAL PIEC       | ES         | GRADE<br>A615-60 |            | IPMENT DATE  |
|---|-----------------------|------------------|--------------|---------------|----------------|---------------------|----------------------|-----------------------|-----------|-----------------|------------|------------------|------------|--------------|
| C       Mn       S       P       Si       CC       Ni       Mo       Cu       V       Nb       CE         Vield Tensile Elongation         mple-1       70.5       466       110.0       759       12.5         vield Tensile Elongation       759       12.5         vield Tensile Elongation       763       14.4         mple-1       70.5       466       100.0       773       14.4         mple-2       69.5       479       100.7       763       14.4         Mechanical         ESI         ESI         ESI         ESI         ESI         Displant feature in explantionate in explantin explantin explantionate explantionate in explantion   | PART NUMBE            | R :              | RB019        | 7760000       | CA             | DES                 | CRIPTION             | N: Reb                | 15-60     |                 |            |                  |            |              |
| 0.42         1.04         0.03         0.01         0.24         0.03         0.001         0.68           Viold Tensile Elongation           mple-1         Yid-1         (MS3)         Ultimate-1         (MS3)         Ultimate-2         (MS3)         Elong8* (8)           mple-2         CS3         486         Ultimate-2         (MS3)         Ultimate-2         (MS3)         Ultimate-3         (MS3)           mple-2         CS3         479         Ultimate-2         (MS3)         Ultimate-3         (NS3)         Ultimate-3         (MS3)           Mechanical           ESI         RESULT           Besize         Pass  |                       |                  |              |               |                |                     |                      | Chemical              |           |                 |            |                  |            |              |
| TId-1 (KSI)       TId-1 (KSI)       Ultimate-1 (KSI)       Ultimate-1 (MPa)       Elong8* (%)         mple-1       70.5       486       110.0       759       12.5         TId-2 (KSI)       YId-2 (MPa)       Ultimate-2 (KSI)       Ultimate-2 (KSI)       Elong8* (%)         mple-2       69.5       479       Ultimate-2 (KSI)       Ultimate-2 (KSI)       Elong8* (%)         mple-2       69.5       479       Ultimate-2 (KSI)       Vitimate-2 (KSI)       Elong8* (%)         mple-2       69.5       479       Ultimate-2 (KSI)       Vitimate-2 (KSI)       Elong8* (%)         mple-2       69.5       479       Ultimate-2 (KSI)       Vitimate-2 (KSI)       Elong8* (%)         mple-2       69.5       479       Ultimate-7       763       14.4         Mechanical         Mechanical         Mechanical         Pass         Pass         Pass         State of the material, NA USA by basic Electric Furnace procees(se) to mest the order of of the material, NA USA, by basic Electric Furnace procees(se) to mest the order of of the material, NA USA, by basic Electric Furnace procees(se) to mest the order of of the material, AN USA, by basic Electric Furnace procees(se) to mest the order of the material, NA USA by basic Electric Fu   |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| mple-1       70.5       486       110.0       759       12.5         mple-2       69.5       479       Utimate-2 (KST)       Utimate-2 (KST)       Utimate-2 (KST)       Elong8" (%)         mple-2       69.5       479       110.7       763       14.4         Mechanical         ESI       RESULT         tend Test       Pass  |                       |                  |              |               |                |                     | Yield Te             | ensile Elonga         | tion      |                 |            |                  |            |              |
| mple-2       69.5       479       110.7       763       14.4         Mechanical         EST       RESULT         Pass       Pass  | ample-1               | Yld-1            |              | Yld-1         |                | Ultimate-1          |                      | Ultimate-1            |           | Elong8          |            |                  |            |              |
| EST RESULT<br>tend Test Pass  approved ABS QA.Mill. Certificate No. 12-MMPQA-076. This Material was melted and manufactured in our plant located in Reanoke, VA, USA, by basic Electric Furnace process(es) to meet the<br>provide ABS QA.Mill. Certificate No. 12-MMPQA-076. This Material was melted and manufactured in our plant located in Reanoke, VA, USA, by basic Electric Furnace process(es) to meet the<br>provide ABS QA.Mill. Certificate No. 12-MMPQA-076. This Material was melted and manufactured in our plant located in Reanoke, VA, USA, by basic Electric Furnace process(es) to meet the<br>provide ABS QA.Mill. Certificate No. 12-MMPQA-076. This Material was melted and manufactured in our plant located in Reanoke, VA, USA, by basic Electric Furnace process(es) to meet the<br>provide Constrained on the second and the second and the second and the ASTM scope for this material. All samples tested are full size. Unless a metric specification is<br>direct. Ubin material has been tested and metric the requirements of the inclusional ranges.<br>his is to certify the above to be a true and accurate report as contained in the records of this company.<br>END OF CERTIFICATION The Material Second | ample-2               | Yld-2            |              | Yld-2         |                | Ultimate-2          |                      | Ultimate-2            |           | Elong8          |            |                  |            |              |
| werd Test     Pass  |                       |                  |              |               |                |                     | 1                    | Mechanical            |           |                 |            |                  |            |              |
| eproved ABS QA MII. Certificate No. 12:MMPQA-676. This Material was melted and manufactured in our plant located in Roanoke, VA, USA, by basic Electric Furnace process(es) to meet the<br>ordered" Grade. Marcury, Radium or other Apina source materials in any form have not been used in the production of this material. No Waid repair has been performed. Any tensite values<br>tated havin attential has been tested and meets the requirements of the inch-pound mages.<br>This is to certify the above to be a true and accurate report as contained in the records of this company.<br>END OF CERTIFICATION DESCRIPTION DESCRIP    | TEST                  |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  | Bend Test             |                  |              |               |                | Pass                |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as adfended in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is determined the above to be a true and accurate report as contained in the records of this company.  END OF CERTIFICATION Engineer of Tests: Lewis E. Leftwich Jr.  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| ordered <sup>®</sup> Grade. Mercury, Radium or other Alpha source materials in any form have not been used in the production of this material. No Weid repair has been performed. Any tensile values tated herein either inch-pound units of 31 units are to be regarded as separate as a defined in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is deterred, this material has been tested and meets the requirements of the inch-pound ranges.<br>his is to certify the above to be a true and accurate report as contained in the records of this company.<br>END OF CERTIFICATION<br>Engineer of Tests: Lewis E, Leftwich Jr.   |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| tated herein either inch-pound units or SI units are to be regarded as separate as defined in the ASTM scope for this material. All samples tested are full size. Unless a metric specification is<br>rdered, this material has been tested and meets the requirements of the inch-pound ranges.<br>his is to certify the above to be a true and accurate report as contained in the records of this company.<br>END OF CERTIFICATION   |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| Inderect, this material has been tested and meets the requirements of the inch-pound ranges.         his is to certify the above to be a true and accurate report as contained in the records of this company.         END OF CERTIFICATION         Image: Company to the image: Company to the image of th   |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
| END OF CERTIFICATION  |                       |                  |              |               |                |                     |                      | scope for any materie | a. An sun | sies tested are | un size. c | incos a neuro sp | comoudonna |              |
| END OF CERTIFICATION  |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |
|   | this is to certify t  | ne above to t    | e a true and | accurate rep  | on as containe | eu mitte records of | uns compan           | y.                    |           |                 |            |                  |            |              |
|   | END O                 | F CERT           | FICATI       | ON            |                | 1.0                 | 1                    | the fill              |           | E               | nginee     | r of Tests:      | Lewis E. L | .eftwich Jr. |
|   | tc302 (v6.0)          | e o e kapolitaka |              |               |                |                     |                      |                       |           |                 |            |                  | Date Prin  | ted: 03/13/2 |
|   |                       |                  |              |               |                |                     |                      |                       |           |                 |            |                  |            |              |

Figure B-11. Rebar No. 6 Material Certificate, Test No. NJPCB-7

| Independen  | ice Tube   |   | CI                                     | 6226 W. 74th St<br>hicago, IL 60638<br>708-496-0380<br>ax: 708-563-1950   |  | Certific                    | ·                       | endencetube.<br>itctube.<br>iber: DCR 493 |
|---|--|---|--|---|--|-----------------------------|-------------------------|---|
| Sold By:<br>INDEPENDENCE<br>6226 W. 74th St.<br>Chicago, IL 60638<br>Tel: 708-496-0380<br>Fax: 708-563-1950   |  | ION   | S<br>B                                 | urchase Order No<br>ales Order No: DC<br>ill of Lading No: D<br>tvoice No:  | CR 87576 - 3                                     |                             | hipped: 10<br>voiced:   | 0/28/2016                                 |
| Sold To:<br>1214 - LIVINGSTO<br>P.O. BOX 300<br>STAUNTON, IL 62   |  |   | 1<br>1                                 | hip To:<br>- LIVINGSTON P<br>612 ROUTE 4 NO<br>TAUNTON, IL 620  | RTH  |                             |                         |   |
| CERTIFICAT<br>Customer Part No  | E of ANALYSIS  | and TE  | STS                                    |   |  | Certificate<br>Test D       | No: DCF<br>Date: 10/2   |   |
| TUBING A500B N<br>4" SQ X 1/2" X 40<br>* DO NOT SWITC   | <b>,</b>   |   |  |   |  | Total I                     | Pieces<br>9             | Total Weight<br>7,787                     |
| Bundle Tag Mill<br>921690 40<br>40  | SF1425 YL  | ecs<br>.D=82600/TE<br>.D=83800/TE                                 |  | 00/ELG=26.5<br>00/ELG=24  | Y/T Ra<br>0.9483<br>0.9426                       | tio Piec                    | es \<br>9               | Weight<br>7,787                           |
|   | SF1424 Carbon Eq   |   | 50000000000000000000000000000000000000 |   |  |                             | HE USA                  |   |
| C Mn<br>0.0600 0.5700   | P S<br>0.0080 0.0020   | Si<br>0.2140 (  | Al<br>0.0220                           | Cu Cr<br>0.0900 0.0300  | Mo \<br>0.0100 0.0                               |                             | Nb<br>0 0.010           | Cb<br>0 0.0100                            |
| Sn N<br>0.0090 0.0066   | B Ti<br>0.0002 0.0010  | Ca<br>0.0013  |  |   |  |                             |                         |   |
|   |  | recent LEED   | ) informa                              | ation from the prod   | ucina mill)                                      |                             |                         |   |
| LEED Information  | A  |   |  |   | <b>U</b> ,                                       |                             |                         |   |
| Method  | Locatio  |   |  | cycled Content  | Post Consi                                       |                             | Post Ir                 |   |
| Method<br>EAF   | Location<br>Decatur, AL  | n   | Rec                                    | cycled Content<br>66.1%   | Post Const                                       | 54.8%                       |                         | 11.2%                                     |
| Method<br>EAF<br>Mill #: 40 Heat #:   | Location<br>Decatur, AL<br>SF1425 Carbon Eq  | n<br>: 0.1631 He  | Rec<br>eat Src C                       | cycled Content<br>66.1%<br>Drigin: MELTED Al  | Post Consi                                       | 54.8%                       | HE USA                  | 11.2%                                     |
| Method           EAF           Mill #: 40         Heat #:           C         Mn           0.0500         0.5800  | Location           Decatur, AL           SF1425         Carbon Eq           P         S           0.0080         0.0020  | n<br>: 0.1631 He<br>Si<br>0.2160 (                                | Rec                                    | cycled Content<br>66.1%   | Post Consu                                       | 54.8%<br>URED IN TH<br>/ Ni | HE USA                  | 11.2%                                     |
| Method<br>EAF<br>Mill #: 40 Heat #:   | Locatio           Decatur, AL           SF1425         Carbon Eq           P         S           0.0080         0.0020           B         Ti                                  | n<br>: 0.1631 He<br>  Si  | eat Src C                              | cycled Content<br>66.1%<br>Drigin: MELTED Al<br>Cu Cr   | Post Consu                                       | 54.8%<br>URED IN TH<br>/ Ni | HE USA                  | 11.2%                                     |
| Method           EAF           Mill #: 40         Heat #:           C         Mn           0.0500         0.5800           Sn         N           0.0080         0.0068 | Locatio           Decatur, AL           SF1425         Carbon Eq           P         S           0.0080         0.0020           B         Ti                                  | n<br>: 0.1631 He<br>Si<br>0.2160 (<br>Ca<br>0.0012                | Rec<br>eat Src C<br>Al<br>0.0230       | Culed Content           66.1%           Drigin: MELTED Al           Cu         Cr           0.0900         0.0300 | Post Const<br>ND MANUFACT<br>Mo \<br>0.0100 0.00 | 54.8%<br>URED IN TH<br>/ Ni | HE USA                  | 11.2%                                     |
| Method           EAF           Mill #: 40         Heat #:           C         Mn           0.0500         0.5800           Sn         N           0.0080         0.0068 | Location           Decatur, AL           SF1425         Carbon Eq           P         S           0.0080         0.0020           B         Ti           0.0002         0.0010 | n<br>: 0.1631 He<br>Si<br>0.2160 0<br>Ca<br>0.0012<br>recent LEEE | eat Src C<br>Al<br>0.0230              | Culed Content           66.1%           Drigin: MELTED Al           Cu         Cr           0.0900         0.0300 | Post Const<br>ND MANUFACT<br>Mo \<br>0.0100 0.00 | 54.8%                       | HE USA<br>Nb<br>0 0.010 | 11.2%                                     |

Page - 1

Figure B-12. Steel Tube Material Certificate, Test No. NJPCB-7

| Independence T  | ſube   | Cł           | 226 W. 74<br>hicago, IL (<br>708-496-0<br>x: 708-563 | 30638<br>380           |                                    | ł            | Certifica    |                     | ndencetube<br>itctube<br>per: DCR 49 | .com |
|---|--|--------------|--|------------------------|------------------------------------|--------------|--------------|---------------------|--------------------------------------|------|
| Sold By:<br>INDEPENDENCE TUBE<br>6226 W. 74th St.<br>Chicago, IL 60638<br>Tel: 708-496-0380<br>Fax: 708-563-1950      | CORPORATION  | S:<br>Bi     | ales Orde  | r No: DCl<br>ng No: DC | 01033424<br>R 87579 -<br>R 58409 - |              |              | oped: 10/<br>biced: | /28/2016                             |      |
| Sold To:<br>1214 - LIVINGSTON PIF<br>P.O. BOX 300<br>STAUNTON, IL 62088   | PE & TUBE  | 1            | hip To:<br>• LIVING<br>612 ROU<br>TAUNTO             | TE 4 NOF               |                                    | E            |              |                     |                                      |      |
| CERTIFICATE of  | ANALYSIS and TE  | STS          |  |                        |                                    | Cer          | tificate N   | lo: DCR             | 493505                               |      |
| Customer Part No:   |  |              |  |                        |                                    |              | Test Dat     | te: 10/27           | /2016                                |      |
| REJECT TUBING<br>4" SQ X 1/2" X 34'   |  |              |  |                        |                                    |              | Total Pi€    | eces<br>2           | Total Weight<br>1,471                |      |
|   | eat Specs<br>F4193 YLD=77600/1   | EN=8300      | 0/ELG=2  | 5.5                    |                                    | Ratio<br>349 | Pieces<br>2  |                     | /eight<br>1,471                      |      |
| Mill #: 40 Heat #: SF419  | 3 Carbon Eq: 0.1776  | leat Src C   | Drigin: ME   | LTED AN                | D MANUF                            | ACTURE       | D IN THE     | USA                 |                                      |      |
| C Mn F<br>0.0600 0.5900 0.00  |  | Al<br>0.0320 | Cu<br>0.1000   | Cr<br>0.0400           | Mo<br>0.0100                       | V<br>0.0030  | Ni<br>0.0300 | Nb<br>0.0100        | Cb<br>0.0100                         |      |
| Sn         N         E           0.0060         0.0057         0.00   | 3 Ti Ca<br>004 0.0020 0.0012   |              |  |                        |                                    |              |              |                     |                                      |      |
| LEED Information (based   | d on the most recent LEE   | D informa    | ition from   | the produ              | icing mill)                        |              |              |                     |                                      |      |
| Method  | Location   | Rec          | ycled Co   |                        | Post C                             | onsumer      |              | Post In             |                                      |      |
| EAF Deca  | itur, AL   |              |  | 66.1%                  |                                    | 54           | .8%          |                     | 11.2%                                |      |
| Corporation. Sworn this of WE PROUDLY MANUFA  | ACTURE ALL OUR PRO   |              | THE USA  |                        | and mainta                         | ined by l    | ndepende     | ence Tub            | e                                    |      |
| AND INSPECTED IN AC<br>MATERIAL IDENTIFIED  | PRODUCT IS MANUFA<br>CORDANCE WITH AST<br>AS A500 GRADE B(C) M<br>AND A500 GRADE C SPE | M STAND      | ARDS.  | ),                     |                                    | C            | his          | A                   | len                                  |      |
| CURRENT STANDARDS<br>A252-10<br>A500/A500M-13<br>A513-13<br>ASTM A53/A53M-12   AS<br>A847/A847M-14<br>A1085/A1085M-15 |  |              |  |                        |                                    | Quality M    |              |                     | SQ CMQ/OE<br>ms Manager              |      |

and a substanting of a second

Page - 1

Figure B-13. Steel Tube Material Certificate, Test No. NJPCB-7

|   | CERTIFICATE O                       | F CONFORMANCE |  |
|---|-------------------------------------|---------------|--|
| *PHOENIX STEEL SERVICE IN<br>4679 JOHNSTON PARKWAY<br>CLEVELAND, OHIO 44128<br>216-332-0600 | c.                                  | DATE:         | 9/07/16  |
| SOLD TO: SEIBEL MODERN MF<br>38 PALMER PLACE<br>LANCASTER, NY 1                             |                                     | 38 PALMER     | DERN MFG. & WELDING<br>PLACE<br>NEW YORK 14086 |
| Cust P/O# SBS-16  |                                     |               |  |
| SIZE: .250 X  | 49.00 X                             | 144.00        |  |
| GRADE: HR A709 GR50   |                                     |               |  |
| DATE SHPPD: 9/07/16   |                                     |               |  |
| Wt.Shipped 43300  |                                     |               |  |
|   | CHEMICAL ANALY                      |               |  |
| Heat Number <mark>269878</mark>   |                                     |               |  |
| C : .05<br>Si: .019   | Mn: 1.020                           | P:.007        | S : .001                                       |
| Cu: .129  | Ti: .003<br>Al: .027                | Cb: .001      | V : .080<br>N : .017                           |
| B : .001  | Sn: .007                            | Ni: .053      | N : .017<br>Mo: .019                           |
|   | PHYSICAL PROP                       | ERTIES        |  |
| ······································  |                                     |               |  |
| Yield: 63700  | Tensile: 77700                      | Elongat       | zion: 30.1%                                    |
| Misc Info TAG#: C401239<br>Misc Info *MELTED AND M  | 09-10-11-12-13<br>ANUFACTURED IN TH | E USA*        |  |
|   |                                     |               |  |
|   |                                     |               |  |

THE ABOVE IS IN ACCORDANCE WITH OUR RECORDS. CONFORMANCE FORM REV. 10/04/12 DJD

Figure B-14. 2-in.  $\times$  <sup>1</sup>/<sub>4</sub>-in. (51-mm  $\times$  6-mm) Bent Steel Plate, Test No. NJPCB-7

|   |   | CI                                | RTIFIED MATERIAL TEST REPORT                          | ×   |                                    | Page 1/1                    |
|---|---|-----------------------------------|---|---|------------------------------------|-----------------------------|
| GÐ GERDAU   | CUSTOMER SHI<br>TRIAD METAL<br>3507 GRAND A | S                                 | CUSTOMER BILL TO<br>TRIAD METALS INTERNATIONAL<br>MET | GRADE<br>GGMULTI  | SHAPE / SIZE<br>Flat Bar / 1/2 X 2 | DOCUMENT<br>0000000000      |
| S-ML-CHARLOTTE<br>501 LAKEVIEW ROAD   | PITTSBURGH,<br>USA                          |                                   | I VILLAGE RD<br>HORSHAM,PA 19044-3800<br>USA          | LENGTH<br>20'00"  | WEIGHT<br>16,728 LB                | HEAT / BATCH<br>54148807/02 |
| HARLOTTE, NC 28269<br>SA  | SALES ORDEF<br>3566020/00002                |                                   | CUSTOMER MATERIAL Nº                                  | SPECIFICATION / DATE<br>ASTM A529-14, A572-15<br>ASTM A6-14, A36-14, ASME |                                    |                             |
| USTOMER PURCHASE ORDER NUMBER<br>0844W  |   | BILL OF LADING<br>1321-0000039076 | DATE<br>05/10/2016                                    | ASTM A709-13A, AASHTO<br>CSA G40.20-13/G40.21-13                          | M270-12                            |                             |
| снемкал сомрозитом<br>С Мп Р<br>0.17 0.79 0.011   | \$<br>0.035                                 | \$j Çu<br>0.21 0.3                | Ni Cr<br>0.18 0.15                                    | Mo V<br>0.060 0.017   | Np Sn<br>0.001 0.015               |                             |
| AECHANICAL PROPERTIES<br>2 Elong. G<br>25.00 8.0  | (L<br>ch<br>00                              | UTS<br>PSI<br>78985               | UTS<br>MPa<br>545                                     | P\$1<br>56738   | YS<br>MPa<br>391                   |                             |
| SEOMETRIC CHARACTERISTICS<br>R R<br>25 60   | n   | *                                 | <b>1910 - 1904 - 1999 - 1999 - 1999 - 1999</b>        |   |                                    |                             |
| OMMENTS / NOTES<br>his grade meets the requirements for the following grade<br>STM Grades: A36; A529-50; A572-50; A709-36; A709-<br>SA Grades: 44W; 50W<br>ASHTO Grades: M270-36; M270-50<br>SME Grades: SA36 |   |                                   |   |   |                                    |                             |
|   |   | ······                            | 2.<br>  | na dalama yang sa                     |                                    |                             |
|   |   |                                   |   |   |                                    |                             |
|   |   |                                   |   |   |                                    |                             |
| The shove figures are cert  | ilied chemical and                          | nhysical test records as          | contained in the permanent records of comp            | any. We cortify that these does not                                       | errat and is constituted with      |                             |
| the above figures are cert  | his material includ                         | ling the billets, was melte       | d and manufactured in the USA. CMTR co                | any, we certify that these data are c<br>implies with EN 10204.3.1        | priect and in compliance with      |                             |

Figure B-15. <sup>1</sup>/<sub>2</sub>-in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7

|   |                                       | C  | ERTIFIED MA                        | TERIAL TEST RI                         | PORT                          |                              |  |             |                             |    | Page 1/1                  |
|---|---------------------------------------|--|------------------------------------|--|-------------------------------|------------------------------|--|-------------|-----------------------------|----|---------------------------|
| CEDDALL   | CUSTOMER SHIPT<br>TRIAD METALS        |  | CUSTOMER                           | BILL TO<br>FALS INTERNATIO             | NAI                           | GRADE<br>GGMULT              | ٦I   |             | E / SIZE<br>r / 1/2 X 2 1/4 |    | DOCUMENT II<br>0000000000 |
| US-ML-CHARLOTTE   | 3507 GRAND AV<br>PITTSBURGH,PA<br>USA | Έ  | MET<br>1 VILLAGE                   |  | NAL                           | LENGTH<br>20'00"             |  |             | WEIGHT<br>1,979 LB          |    | EAT / BATCH<br>148805/02  |
| CHARLOTTE, NC 28269<br>JSA  | SALES ORDER<br>3806947/000010         |  |                                    | IER MATERIAL N                         |                               | ASTM A53<br>ASTM A6-         | CATION / DATE or<br>29-14, A572-15<br>14,A36-14, ASME SA | -36         | N                           |    |                           |
| CUSTOMER PURCHASE ORDER NUMBER<br>93494W  |                                       | BILL OF LADING<br>1321-0000039836                                    |                                    | DATE<br>06/08/2016                     |                               |                              | 09-13A, AASHTO M27<br>10-13/G40.21-13                    | 70-12       |                             |    |                           |
| CHEMICAL COMPOSITION<br>C Mn P<br>0.18 0.77 0.013   | \$<br>0.033                           | \$j Çu<br>0.21 0.3   | 1 0.                               | li Çı<br>23 0.16                       | M<br>0.0                      | lo<br>950                    | 0.013 0  | Nb<br>%     | \$n<br>0.016                |    |                           |
| MECHANICAL PROPERTIES<br>Elong. G/<br>25.00 8.0   | L<br>5h<br>00                         | UTS<br>PSI<br>75435  |                                    | UTS<br>MPa<br>520                      |                               | PS1<br>53469                 |  | MP<br>369   | a<br>a                      |    |                           |
| DEOMETRIC CHARACTERISTICS<br>R:R<br>22.00   |                                       |  |                                    |  |                               |                              |  |             |                             |    |                           |
| This grade meets the requirements for the following grades<br>STM Grades: A36: A529-50; A572-50; A709-36; A709-5<br>SA Grades: 44W; 50W<br>AASHTO Grades: M270-36; M270-50<br>ASME Grades: SA36 |                                       |  |                                    |  |                               |                              |  |             |                             |    |                           |
| e<br>   |                                       |  |                                    |  |                               |                              |  |             |                             | r. |                           |
|   |                                       |  |                                    |  |                               |                              |  |             |                             |    |                           |
| The above figures are certi<br>specified requirements. Th   | is material, includin                 | hysical test records as<br>g the billets, was melt<br>R YALAMANCHILI | contained in the<br>ed and manufac | permanent records tured in the USA, Cl | f company. We<br>ATR complies | e certify that<br>with EN 10 | t these data are corre<br>204 3.1.                       | ct and in c |                             |    |                           |
| Marke   | QUALITY                               | / DIRECTOR   |                                    |  |                               | C                            | Jorden Jacker  |             | ASSURANCE MGR.              |    |                           |

Figure B-16. <sup>1</sup>/<sub>2</sub>-in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7

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- -

|        |                  |  |          | CERTIFIC  | ATE OF | CONF  | ORMANCE      |   |   |
|--------|------------------|--|----------|-----------|--------|-------|--------------|---|---|
| 4679 J | OHNSTO<br>AND, C | CEL SERVIC<br>ON PARKWAY<br>OHIO 44128 | E INC.   |           |        |       | DATE :       |   |   |
| SOLD I | 38               | BEL MODERI<br>PALMER PL<br>ICASTER, N  | ACE      |           | SHI    | IP TO | 38 PALMER B  | ERN MFG. & WELDING<br>PLACE<br>NEW YORK 14086 | 3 |
| Cust   | P/0#             | SBR-41                                 |          |           |        |       |              |   |   |
| SIZE:  | .500             |  | х        | 40.00     | Х      | 144.0 | 00           |   |   |
| GRADE: | HR A3            | 6 *MELTED                              | & MANUF  | ACTURED   | IN THE | USA*  |              |   |   |
| DATE S | SHPPD:           |  |          |           |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   | x |
|        |                  |  |          | CHEMICAL  |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |
| Heat N | umber            | SF2550                                 |          |           |        |       |              |   |   |
|        |                  | .216                                   |          | .548      |        |       |              | S : .002                                      |   |
|        |                  | .222                                   |          | .002      |        |       | .033<br>.007 | V : .002                                      |   |
|        | çu.              | .070                                   |          | .0051     |        |       | .0012        | N : .0054                                     |   |
|        | в:               | .0002                                  |          |           |        |       | .0232        | Mo: .0103                                     |   |
|        |                  |  |          | PHYSICAL  |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |
| Y      | ield:            | 38700                                  | Ten      | sile: 720 | 000    |       | Elongati     | ion: 33%                                      |   |
| Misc I | Info             | TAG#: PS1                              | 49410A-E | -C-D      |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |
|        |                  |  |          |           |        |       |              |   |   |

THE ABOVE IS IN ACCORDANCE WITH OUR RECORDS. CONFORMANCE FORM REV. 10/04/12 DJD

Figure B-17. <sup>1</sup>/<sub>2</sub>-in. (13-mm) Thick Steel Plate Material Certificate, Test No. NJPCB-7

### 1107 Advantage Grout

Cement Based Grout

**TECHNICAL DATA SHEET** 

### **DESCRIPTION**

The 1107 Advantage Grout is a non-shrink, nonmetallic, non-corrosive, cementitious grout that is designed to provide a controlled, positive expansion to ensure an excellent bearing area. The 1107 Advantage Grout can be mixed from a fluid to a dry pack consistency.

### USE

Exterior grouting of structural column base plates, pump and machinery bases, anchoring bolts, dowels, bearing pads and keyway joints. It finds applications in paper mills, oil refineries, food plants, chemical plants, sewage and water treatment plants etc.

#### **FEATURES**

- Controlled, net positive expansion
- Non shrink
- Non metallic/non corrosive
- Pourable, pumpable or dry pack consistency
- Interior/exterior applications

#### PROPERTIES

Corps of Engineers Specification for non-shrink grout: CRD-C 621 Grades A. B. C ASTM C-1107 Grades A, B, C ASTM C-827 - 1107 Advantage Grout yielded a controlled positive expansion

Expansion - ASTM C-1090:

1 day: 0-0.3 3 days: 0-0.3 14 days: 0-0.3 28 days: 0-0.3

#### **Test Results**

|          | @1   | Day  | @ 3  | Days | @7   | Days | @ 28  | Days |
|----------|------|------|------|------|------|------|-------|------|
| Fluidity | PSI  | MPa  | PSI  | MPa  | PSI  | MPa  | PSI   | MPa  |
| Dry-Pack | 5000 | 34.5 | 7000 | 48.2 | 9000 | 62.0 | 10000 | 68,9 |
| Flowable | 2500 | 17.2 | 5000 | 34.5 | 6000 | 41_4 | 8000  | 55.1 |
| Fluid    | 2000 | 13.8 | 4000 | 27.6 | 5000 | 34.5 | 7500  | 51.7 |

#### Note:

The data shown is typical for controlled laboratory conditions. Reasonable variation from these results can be expected due to interlaboratory precision and bias. When testing the field mixed material, other factors such as variations in mixing, water content, temperature and curing conditions should be considered.

#### **Estimating Guide**

Yield (Flowable Consistency): 0.43 cu. ft./50 lbs. (0.0122 cu. M/22.67 kg) bag 0.59 cu. ft./50 lbs. (0.017 cu. M/22.67 kg) bag extended with 25 lbs. (11.34 kg) of washed 3/8 in. (1cm) pea gravel

#### Packaging

| PRODUCT | DIOUTOS   | S     | IZE      |
|---------|-----------|-------|----------|
| CODE    | PACKAGE   | lbs   | kg       |
| 67435   | Bag       | 50    | 22.67    |
| 67437   | Supersack | 3,000 | 1,360.78 |

#### STORAGE

Store in a cool, dry area free from direct sunlight. Shelf life of unopened bags, when stored in a dry facility, is 12 months. Excessive temperature differential and /or high humidity can shorten the shelf life expectancy.

#### **APPLICATION**

#### **Surface Preparation:**

Thoroughly clean all contact surfaces. Existing concrete should be strong and sound. Surface should be roughened to insure bond. Metal base plates should be clean and free of oil and other contaminants. Maintain contact areas between 45°F (7°C) and 90°F (32°C) before grouting and during curing period.

Thoroughly wet concrete contact area 24 hours prior to grouting, keep wet and remove all surface water just prior to placement. If 24 hours is not possible, then saturate with water for at least 4 hours. Seal forms to prevent water or grout loss. On the placement side, provide an angle in the form high enough to assist in grouting and to maintain head pressure on the grout during the entire grouting process. Forms should be at least 1 in. (2.5 cm) higher than the bottom of the base plate.

Water Requirements: Desired Mix Water / 50 lbs. (22.67 kg) Bag Dry Pack: 5 pints (2.4 L) Flowable: 8 pints (3.8 L Fluid: 9 pints (4.2 L)

#### Mixing:

A mechanical mixer with rotating blades like a mortar mixer is best. Small quantities can be mixed with a drill and paddle. When mixing less than a full bag, always first agitate the bag thoroughly so that a representative sample is obtained.



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File Date: 3/27/2015

Figure B-18. Non-Shrink Grout Specifications, Test No. NJPCB-7

### 1107 Advantage Grout

Cement Based Grout

TECHNICAL DATA SHEET

Place approximately 3/4 of the anticipated mix water into the mixer and add the grout mix, adding the minimum additional water necessary to achieve desired consistency.

Mix for a total of five minutes ensuring uniform consistency. For placements greater in depth than 3 in. (7.6 cm), up to 25 lbs. (11.34 kg) of washed 3/8 in. (1 cm) pea gravel must be added to each 50 lbs. (22.67 kg) bag of grout. The approximate working time (pot life) is 30 minutes but will vary somewhat with ambient conditions.

For hot weather conditions, greater than 85°F (29°C), mix with cold water approximately 40°F (4°C). For cold weather conditions, less than 50°F (10°C), mix with warm water, approximately 90°F (29°C). For additional hot and cold weather applications, contact Dayton Superior.

#### **Placement:**

Grout should be placed preferably from one side using a grout box to avoid entrapping air. Grout should not be over-worked or over-watered causing segregation or bleeding. Vent holes should be provided where necessary.

When possible, grout bolt holes first. Placement and consolidation should be continuous for any one section of the grout. When nearby equipment causes vibration of the grout, such equipment should be shut down for a period of 24 hours. Forms may be removed when grout is completely self-supporting. For best results, grout should extend downward at a 45 degree angle from the lower edge of the steel base plates or similar structures.

#### CLEAN UP

DEC

16

Use clean water. Hardened material will require mechanical removal methods.

#### CURING

Exposed grout surfaces must be cured. Dayton Superior recommends using a Dayton Superior curing compound, cure & seal or a wet cure for 3 days. Maintain the temperature of the grout and contact area at 45°F (7°C) to 90°F (32°C) for a minimum of 24 hours.

#### LIMITATIONS

#### FOR PROFESSIONAL USE ONLY

Do not re-temper after initial mixing Do not add other cements or additives

Setting time for the 1107 Advantage Grout will slow during cooler weather, less than 50°F (10°C) and speed up during hot weather, greater than 80°F (27°C) Prepackaged material segregates while in the bag, thus when mixing less than a full bag it is recommended to first agitate the bag to assure it is blended prior to sampling.

#### PRECAUTIONS

#### **READ SDS PRIOR TO USING PRODUCT**

- Product contains Crystalline Silica and Portland Cement Avoid breathing dust Silica may cause serious lung problems
- Use with adequate ventilation n Wear protective clothing, gloves and eye protection (goggles, safety glasses and/or face shield)
- Keep out of the reach of children
- Do not take internally
- In case of ingestion, seek medical help immediately
- May cause skin irritation upon contact, especially prolonged or repeated. If skin contact occurs, wash immediately with soap and water and seek medical help as needed.
- If eye contact occurs, flush immediately with clean water and seek medical he/p as needed
- Dispose of waste material in accordanc

#### MANUFACTURER

Dayton Superior Corporation 1125 Byers Road Miamisburg, OH 45342 Customer Service: 888-977-9600 Technical Services: 877-266-7732 Website: www.daytonsuperior.com

#### WARRANTY

Dayton Superior Corporation ("Dayton") warrants for 12 months from the date of manufacture or for the duration of the published product shelf life, whichever is less, that at the time of shipment by Dayton, the product is free of manufacturing defects and conforms to Dayton's product properties in force on the date of acceptance by Dayton of the order. Dayton shall only be liable under this warranty if the product has been applied, used, and stored in accordance with Dayton's instructions, especially surface preparation and installation, in force on the date of acceptance by Dayton of the order. The purchaser must examine the product when received and promptly notify Dayton in writing of any non-conformity before the product is used and no later than 30 days after such non-conformity is first discovered. If Dayton, in its sole discretion, determines that the product breached the above warranty, it will, in its sole discretion, replace the non-conforming product, refund the purchase price or issue a credit in the amount of the purchase price. This is the sole and exclusive remedy for breach of this warranty. Only a Dayton officer is authorized to modify this warranty. The information in this data sheet supersedes all other sales information received by the customer during the sales process. THE FOREGOING WARRANTY SHALL BE EXCLUSIVE AND IN LIEU OF ANY OTHER WARRANTY SHALL BE EXCLUSIVE AND IN LIEU OF ANY OTHER WARRANTY SHALL BE EXCLUSIVE AND IN LIEU OF ANY OTHER WARRANTY SHALL BE EXCLUSIVE AND IN LIEU OF PREATION OF LAW, COURSE OF DEALING, OTHERWISE ARISING BY OPERATION OF LAW, COURSE OF DEALING, CUSTOM, TRADE OR OTHERWISE.

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File Date: 3/27/2015

Figure B-19. Non-Shrink Grout Specifications, Test No. NJPCB-7



LINCOLN OFFICE 825 "M" Street, Suite 100 Lincoln, NE 68508 Phone: (402) 479-2200 Fax: (402) 479-2276

### COMPRESSION TEST OF CYLINDRICAL CONCRETE SPECIMENS - 4x8

ASTM Designation: C 39

Date 28-Jun-17

Client Name: Midwest Roadside Safety Facility Project Name: NJPCB-7

Placement Location: None Given

| lix Designati                | on: N/A                 |           |               |             |                        |                             |                      | Require                       | ed Streng                       | gth: N/A                       |                         |                                  |                               |                        |  |
|------------------------------|-------------------------|-----------|---------------|-------------|------------------------|-----------------------------|----------------------|-------------------------------|---------------------------------|--------------------------------|-------------------------|----------------------------------|-------------------------------|------------------------|--|
|                              |                         |           |               |             |                        | 1                           | Laboratory           | Test Data                     | a                               |                                |                         |                                  |                               |                        |  |
| Laboratory<br>Identification | Field<br>Identification | Date Cast | Date Received | Date Tested | Days Cured in<br>Field | Days Cured in<br>Laboratory | Age of Test,<br>Days | Length of<br>Specimen,<br>in. | Diameter of<br>Specimen,<br>in. | Cross-Sectional<br>Area,sq.in. | Maximum<br>Load,<br>Ibf | Compressive<br>Strength,<br>psi. | Required<br>Strength,<br>psi. | Type<br>of<br>Fracture | ASTM Practice<br>for Capping<br>Specimen |
| NCB- 1                       | А                       | 6/27/2017 | 6/27/2017     | 6/28/2017   | 0                      | 1                           | 1                    | 8                             | 4.01                            | 12.63                          | 54,291                  | 4,300                            |                               | 6                      | C 1231                                   |
| NCB- 2                       | В                       | 6/27/2017 | 6/27/2017     | 6/28/2017   | 0                      | 1                           | 1                    | 8                             | 4.01                            | 12.63                          | 56,844                  | 4,500                            |                               | 6                      | C 1231                                   |

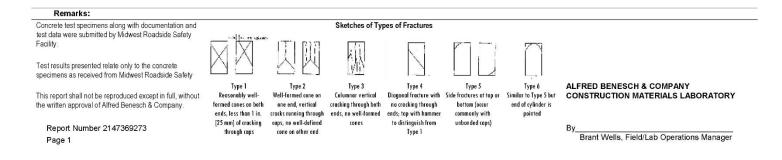


Figure B-20. Non-shrink Grout Compressive Test Certificate, Test No. NJPCB-7

## Appendix C. Concrete Tarmac Strength

|  | 1                   |            |                   |                              | D                  | 0040              |
|--|---------------------|------------|-------------------|------------------------------|--------------------|-------------------|
| Client:  | UNL<br>MwRSF        |            |                   | Date:                        | December 10,       | 2010              |
| Project:   |                     | 2          |                   |                              |                    |                   |
| Placement Location:  | WI - East 1, 2,     | 3          |                   | Mix No.:                     |                    |                   |
| Aix Type:  | Class:              |            | Cement Facto      |                              | 1                  | а                 |
| ype of Forms   |                     |            | Water-Cement      |                              |                    | 13                |
| desister Orentite  |                     | 12         | Siump inches      |                              | -                  | 12                |
| Admixture Quantity   |                     | 12         | Unit Wt, Ibs/cu   |                              |                    | 18                |
| Admixture Type   |                     | 18         | Air Content, %    |                              |                    | a                 |
| Admixture Quantity<br>Average Field Temperature  | _                   | 13         | Batch Volume      |                              |                    | 18                |
| femperature of Concrete F  |                     | 18         | Ticket No.        | 1 00. 100.                   |                    | 13                |
| dentification Laboratory   |                     | East 2     | East 3            | 1                            |                    |                   |
| Date Cast  | GAST                | 19151      |                   | Construction of the second   |                    |                   |
| Date Received in Laboratory  | 11/30/2010          | 11/30/2010 | 11/30/2010        |                              | 1.1.1.1.1.1        |                   |
| Date Tested  |                     |            |                   |                              |                    |                   |
| Days Cured in Field  | - 10 <sup>-10</sup> |            |                   |                              |                    |                   |
| Days Cured in Laboratory   | 1.000.01            |            |                   |                              |                    | Second and second |
| Age of Test, Days  |                     |            |                   |                              |                    |                   |
| ength, in.   | 7.78                | 7.81       | 7.75              |                              | Selection in the   |                   |
| Average Width (1), in.   | 3.72                | 3.72       | 3.72              |                              |                    |                   |
| Cross-Sectional Area, sq. in.  | 10.874              | 10.869     | 10.874            |                              |                    |                   |
| Aaximum Load, Ibf  | 71,030              | 76,470     | 73,310            |                              |                    |                   |
| Compressive Stength, psi   | 6,530               | 7,040      | 6,740             |                              |                    |                   |
| ength/Diameter Ratio   | 2.091               | 2.099      | 2.083             |                              |                    |                   |
| Correction   |                     |            |                   |                              |                    |                   |
| Corrected Compressive Strength,psi   | 0                   | 0          | 0                 |                              |                    |                   |
| Type of Fracture   | 4                   | 4          | 4                 |                              | and the set of the | Second Logar      |
| Required Strength,psi  |                     |            |                   |                              |                    |                   |
| Remarks:<br>All concrete break data in this report was pro<br>inless otherwise noted.<br>This report shall not be reproduced except in |                     |            | I of Alfred Benes | sch & Company<br>ESCH & COMP |                    | Ŷ                 |

Figure C-1. Concrete Tarmac Strength Test

benesch

LINCOLN OFFICE 825 J Street Lincoln, NE 68508 402/479-2200

### COMPRESSION TEST OF Cylindrical CONCRETE SPECIMENS ASTM Designation: C39-03

| Yd na<br>na<br>na<br>na<br>na<br>na | t Ratio                | Cement Facto  | əst 4 &5   | MwRSF         | Client:<br>Project:   |
|-------------------------------------|------------------------|---|------------|---------------|---|
| Yd na<br>na<br>na<br>na<br>na<br>na | or, Sks/Yd<br>it Ratio | and the second se | est 4 &5   |               | TOJECL.   |
| Yd na<br>na<br>na<br>na<br>na<br>na | or, Sks/Yd<br>it Ratio | and the second se |            | WI - Epoxy We | Placement Location:   |
| na<br>na<br>na<br>na                | t Ratio                | and the second se |            | Class:        | Mix Type:   |
| na<br>na<br>na                      |                        |   |            |               | Type of Forms   |
| na<br>na                            |                        | Water-Cemen   |            |               |   |
| na                                  | u Ft                   | Slump Inches  | а          | n             | Admixture Quantity  |
| 1.545                               |                        | Unit Wt, Ibs/c  | а          | n             | Admixture Type  |
|                                     | 6                      | Air Content, 9  | а          | n             | Admixture Quantity  |
| ds. na                              | e, Cu. Yds.            | Batch Volume  | а          | n             | Average Field Temperature   |
| na                                  |                        | Ticket No.  |            | n             | Temperature of Concrete F   |
|                                     |                        |   | 5          | 4             | dentification Laboratory  |
|                                     | ALC: NOT THE REAL      | a chairmanna  |            |               | Date Cast   |
|                                     |                        |   | 12/13/2010 | 12/13/2010    | Date Received in Laboratory   |
|                                     |                        |   |            |               | Date Tested   |
|                                     |                        |   |            | - P           | Days Cured in Field   |
|                                     |                        |   |            | 2             | Days Cured in Laboratory  |
|                                     |                        |   | na         | na            | Age of Test, Days   |
|                                     |                        |   | 8.06       | 8.05          | Length, in.   |
|                                     |                        | Construction and the second   | 3.90       | 3.91          | Average Width (1), in.  |
|                                     |                        |   | 11.952     | 11.977        | Cross-Sectional Area, sq. in.   |
|                                     |                        |   | 71,630     | 71,500        | Maximum Load, Ibf   |
|                                     |                        |   | 5,990      | 5,970         | Compressive Stength, psi  |
|                                     |                        |   | 2.065      | 2.061         | Length/Diameter Ratio   |
|                                     |                        |   |            |               |   |
|                                     |                        |   | 0          | 0             |   |
| Autor Marchine College              | a second da se         |   | 3          | 3             |   |
|                                     |                        |   |            | 198           |   |
|                                     | aneres folies (        |   |            |               | Correction<br>Corrected Compressive Strength,psi<br>Type of Fracture<br>Required Strength,psi |

Figure C-2. Concrete Tarmac Strength Test

## Appendix D. Vehicle Center of Gravity Determination

| Date   |  | · · · · · · · · · · · · · · · · · · ·  | CB-7 VIN:  |  | RB1GP7AS1  | 02101   |
|--|--|--|--|--|--|---|
| Yea  | r: <u>2010</u>   | Make: Doc  | ige Model:   |  | Ram 1500   |   |
|  |  |  |  |  |  |   |
| Vehicle CO   | Determination  | on .   | Moight   | Vortical CC  | Vortical M   |   |
|  | Faultament   |  |  |  | Vertical M   |   |
| VEHICLE  | Equipment  | Truck (Curb)   | (lb.)  | (in.)  | (lbin.)  | 1   |
| +  | Hub  |  | 5053   | 28 1/8   | 142115.63  |   |
| +  |  | tion outindar 9 fromo  | 19   | 15 1/4<br>24 1/2   | 289.75   |   |
| +<br>+   |  | ation cylinder & frame   | 27   | and the second s | 171.5  |   |
| +  | Strobe/Brak  | ank (Nitrogen)   | 5  | 28<br>26 1/4   | 756  |   |
| +  | Brake Recei  |  | 5  | 52 1/2   | 262.5  |   |
| +  | CG Plate inc   |  | 42   | 30 1/2   | 1281   |   |
|  |  | Juding DAS   | -44  | 42 1/4   | -1859  |   |
| -  | Battery  |  | -44  |  | Chall/Storaction   |   |
| р<br>р<br>да   | Oil  |  |  | 26 1/2   | -185.5   |   |
| -  | Interior<br>Fuel   |  | -96<br>-172  | 29 1/2<br>19 1/2   | -2832<br>-3354   |   |
| -  | LAN FRIDAY   |  | 516 - A  | 1 15231841 U27481 58   |  |   |
| 1 <b></b><br>6   | Coolant<br>Washer fluid  |  | -3   | 33 1/2<br>33   | -100.5<br>-33  |   |
| -  |  |  | 99   | 16 3/4   | 1658.25  |   |
| + +  |  | st (In Fuel Tank)  |  |  |  |   |
| +.   |  | pplemental Battery   | 12<br>33   | 26 1/2<br>33 1/4   | 318<br>1097.25   |   |
|  |  |  |  |  | 1 1097.20  |   |
| Note: (+) is add   |  | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio  | ipment from vehicle<br>ht (Ib.) 4979   | ]  | 139717.13  |   |
| Vehicle Din  | ded equipment to v   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations   | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613   | ]  | 139717.13  | ]   |
|  | ded equipment to v   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations   | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:                             | 68 3/8   | in.  | ]   |
| Vehicle Din  | ded equipment to v   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations   | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613   | 68 3/8   | 139717.13  |   |
| Vehicle Din<br>Wheel Bas   | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u>  | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations<br>in. Fr<br>R  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:         | 68 3/8<br>68 1/4   | in.<br>in.   | -   |
| Vehicle Din<br>Wheel Bas<br>Center of G  | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u><br>Gravity   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations<br>in. Fr<br>R<br>2270P MASH Targ   | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:         | 68 3/8<br>68 1/4<br>Test Inertia   | in.<br>in.   | Differenc   |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial   | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u><br>Gravity<br>Weight (lb.)   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatic<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:         | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000  | in.<br>in.   | Differenc   |
| Vehicle Din<br>Wheel Bas<br>Center of C<br>Test Inertial<br>Longitudina  | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u><br>Gravity<br>Weight (Ib.)<br>I CG (in.)   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>8<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4   | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:         | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027   | _in.<br>_in.<br>_in.   | Differenc   |
| Vehicle Din<br>Wheel Bas<br>Center of C<br>Test Inertial<br>Longitudina<br>Lateral CG  | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u><br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)  | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875  | _in.<br>_in.<br>_in.   | Differenc<br>0.<br>-0.8973<br>N   |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG   | ded equipment to v<br>nensions for C<br>e: <u>140 1/4</u><br>Weight (Ib.)<br>I CG (in.)<br>(in.)   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027   | _in.<br>_in.<br>_in.   | Differenc<br>0.<br>-0.8973<br>N<br>0.0612                                       |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C  | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>G is measured from   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06   | _in.<br>_in.<br>_in.   | Differenc<br>0<br>-0.8973<br>N  |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C  | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>G is measured from   | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06   | _in.<br>_in.<br>_in.   | Differenc<br>0.<br>-0.8973<br>N   |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C  | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from  | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle  | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side  | _in.<br>_in.<br>_in.   | Differenc<br>0<br>-0.8973<br>N<br>0.0612  |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G                               | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)  | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel                          | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side  | in.<br>in.<br>al   | Differenc<br>0.<br>-0.8973<br>N<br>0.0612                                       |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G<br>CURB WEI                   | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)<br>Left                         | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel<br>Right                 | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side  | in.<br>in.<br>in.<br>al<br>RTIAL WEIGH                             | Differenc<br>0.<br>-0.8973<br>N<br>0.0612<br>IT (Ib.)<br>Right                  |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G<br>CURB WEIG   | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)<br>Left<br>1439                 | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel<br>Right<br>1386         | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side<br><b>TEST INEF</b><br>Front   |  | Differenc<br>0.<br>-0.8973<br>N<br>0.0612<br>IT (Ib.)<br>Right<br>1414          |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G<br>CURB WEI                   | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)<br>Left                         | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel<br>Right                 | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side  | in.<br>in.<br>in.<br>al<br>RTIAL WEIGH                             | Differenc<br>0.<br>-0.8973<br>N<br>0.0612<br>IT (Ib.)<br>Right                  |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G<br>CURB WEIG<br>Front<br>Rear | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)<br>Left<br>1439<br>1116         | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel<br>Right<br>1386<br>1112 | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side<br><b>TEST INEF</b><br>Front<br>Rear   | in.<br>in.<br>in.<br>al<br><br>RTIAL WEIGH<br><br>Left<br><br>1093 | Difference<br>0.<br>-0.8973<br>N<br>0.0612<br>IT (Ib.)<br>Right<br>1414<br>1121 |
| Vehicle Din<br>Wheel Bas<br>Center of G<br>Test Inertial<br>Longitudina<br>Lateral CG<br>Vertical CG<br>Vertical CG<br>Note: Long. C<br>Note: Lateral G<br>CURB WEIG   | ded equipment to v<br>nensions for C<br>e: 140 1/4<br>Gravity<br>Weight (Ib.)<br>I CG (in.)<br>(in.)<br>(in.)<br>G is measured from<br>CG measured from<br>GHT (Ib.)<br>Left<br>1439<br>1116<br>2825 | vehicle, (-) is removed equi<br>Estimated Total Weig<br>Vertical CG Locatio<br>C.G. Calculations<br>in. Fr<br>2270P MASH Targ<br>5000 ± 110<br>63 ± 4<br>NA<br>28 or grea<br>m front axle of test vehicle<br>n centerline - positive to vel<br>Right<br>1386         | ipment from vehicle<br>ht (Ib.) 4979<br>on (in.) 28.0613<br>ont Track Width:<br>ear Track Width:<br>gets | 68 3/8<br>68 1/4<br><b>Test Inertia</b><br>5000<br>62.1027<br>0.4781875<br>28.06<br>r) side<br><b>TEST INEF</b><br>Front   |  | Differenc<br>0.<br>-0.8973<br>N<br>0.0612<br>IT (Ib.)<br>Right<br>1414          |

Figure D-1. Vehicle Mass Distribution, Test No. NJPCB-7

## Appendix E. Vehicle Deformation Records

| Year:         201           POINT         (in.           1         29.5           2         31.4           3         32.2           4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.72           23         7.04           24         6.87           25         -0.0           26         0.06           27         0.00           28         -0.04           Note:         Crush column | Y           (in.)           77         -34.638           09         -30.025           21         -26.016           48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           66         -30.710           7         -24.640           0         -19.022           24         -31.739  | Z<br>(in.)<br>2.449<br>0.658<br>-0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-4.354<br>-4.354<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.868<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.875<br>-6.875<br>-6.8909<br>-2.889 |   | PRE/POST<br>ORPAN - SI<br>Y'<br>(in.)<br>-33.618<br>-28.315<br>-24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-29.521<br>-24.334<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987<br>-23.902 | -<br>CRUSH  | ΔX<br>(in.)<br>-1.279<br>-2.621<br>-2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.557<br>0.519<br>0.421            | Ay           (in.)           1.020           1.710           1.674           1.263           0.974           1.273           1.065           1.004           1.083           1.113           0.872           1.018           0.982           0.878           0.914           0.871           0.872           0.827           0.719           0.724           0.724 | ΔZ<br>(in.)<br>1.001<br>1.940<br>2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250<br>-0.162     | Total Δ<br>(in.)<br>1.918<br>3.682<br>3.368<br>2.376<br>1.198<br>1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | Crush<br>(in.)<br>1.624<br>3.261<br>2.922<br>2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.099<br>-0.086<br>-0.209<br>-0.086<br>-0.123<br>-0.297<br>-0.299<br>-0.142<br>-0.204<br>-0.250 |
|---|---|---|---|--|---|--|--|--|---|---|
| POINT         (in.           1         29.5           2         31.4           3         32.2           4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.07           26         0.06           27         0.00           28         -0.04                                       | (in.)           (in.)           77         -34.638           09         -30.025           21         -26.016           48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           -8         -35.482           6         -30.710           7         -24.640           7         -24.640           7         -24.640           7         -24.640           0         -19.022           24         -31.739 | (in.)<br>2.449<br>0.658<br>-0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909   | FLO<br>X'<br>(in.)<br>28.298<br>28.788<br>30.140<br>30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469 | ORPAN - SI<br>Y'<br>(in.)<br>-33.618<br>-28.315<br>-24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | Z'           (in.)           3.449           2.598           1.723           1.164           -0.546           -1.056           -1.303           -2.348           -3.808           -4.089           -4.549           -6.888           -6.962           -7.174           -7.045           -6.962           -7.052           -7.066           -7.113 | (in.)<br>-1.279<br>-2.621<br>-2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519                  | (in.)<br>1.020<br>1.710<br>1.674<br>1.263<br>0.974<br>1.273<br>1.095<br>1.004<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.827<br>0.719<br>0.724  | (in.)<br>1.001<br>1.940<br>2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.096<br>-0.029<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250 | (in.)<br>1.918<br>3.682<br>3.368<br>2.376<br>1.198<br>1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | (in.)<br>1.624<br>3.261<br>2.922<br>2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.244<br>-0.204<br>-0.250          |
| POINT         (in.           1         29.5           2         31.4           3         32.2           4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.07           26         0.06           27         0.00           28         -0.04                                       | (in.)           (in.)           77         -34.638           09         -30.025           21         -26.016           48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           -8         -35.482           6         -30.710           7         -24.640           7         -24.640           7         -24.640           7         -24.640           0         -19.022           24         -31.739 | (in.)<br>2.449<br>0.658<br>-0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909   | (in.)<br>28.298<br>28.788<br>30.140<br>30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469              | (in.)<br>-33.618<br>-28.315<br>-24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | (in.)<br>3.449<br>2.598<br>1.723<br>1.164<br>-0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.113   | (in.)<br>-1.279<br>-2.621<br>-2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519                  | (in.)<br>1.020<br>1.710<br>1.674<br>1.263<br>0.974<br>1.273<br>1.095<br>1.004<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.827<br>0.719<br>0.724  | (in.)<br>1.001<br>1.940<br>2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.096<br>-0.029<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250 | (in.)<br>1.918<br>3.682<br>3.368<br>2.376<br>1.198<br>1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | (in.)<br>1.624<br>3.261<br>2.922<br>2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.244<br>-0.204<br>-0.250          |
| 1         29.5           2         31.4           3         32.2           4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.07           26         0.08           27         0.00           28         -0.04  | 77         -34.638           09         -30.025           21         -26.016           48         -22.114           72         -35.032           30         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.6467           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           .8         -35.482           66         -30.710           .7         -24.640           70         -19.022           24         -31.739  | 2.449<br>0.658<br>-0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 28.298<br>28.788<br>30.140<br>30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469                       | -33.618<br>-28.315<br>-24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>1-7.541<br>-34.763<br>-29.987   | 3.449<br>2.598<br>1.723<br>1.164<br>-0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | -1.279<br>-2.621<br>-2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.435<br>0.348<br>0.530<br>0.474<br>0.204<br>0.557<br>0.519                  | 1.020<br>1.710<br>1.674<br>1.263<br>0.974<br>1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.724  | 1.001<br>1.940<br>2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.020<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250          | 1.918           3.682           3.368           2.376           1.198           1.908           1.631           1.065           1.102           1.141           1.144           0.935           1.638           0.984           0.986           1.062           0.969           0.972           0.864           0.932 | 1.624<br>3.261<br>2.922<br>2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.089<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.140<br>-0.142<br>-0.250         |
| 2       31.4         3       32.2         4       32.0         5       27.2         6       28.7         7       28.5         8       28.0         9       24.6         10       24.6         11       24.6         12       24.6         13       19.0         14       18.9         15       18.6         16       18.4         17       13.5         18       13.1         20       13.0         21       6.74         22       6.96         23       7.04         24       6.87         25       -0.07         26       0.06         27       0.00         28       -0.04   | 09         -30.025           21         -26.016           48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           66         -30.710           7         -24.640           7         -24.640           0         -19.022           24         -31.739  | 0.658<br>-0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909   | 28.788<br>30.140<br>30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469                                 | -28.315<br>-24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | 2.598<br>1.723<br>1.164<br>-0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113   | -2.621<br>-2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.271<br>0.271<br>0.271<br>0.388<br>0.435<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519 | 1.710<br>1.674<br>1.263<br>0.974<br>1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.724   | 1.940<br>2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.069<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250         | 3.682<br>3.368<br>2.376<br>1.198<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | 3.261<br>2.922<br>2.012<br>0.698<br>1.4210<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.069<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.142<br>-0.244<br>-0.250                                     |
| 3         32.2           4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.08           27         0.00           28         -0.04  | 21         -26.016           48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           .8         -35.482           66         -30.710           .7         -24.640           .7         -24.640           .7         -24.640           .7         -24.640           .7         -24.640           .7         -24.640   | -0.329<br>-0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.354<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 30.140<br>30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -24.342<br>-20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | 1.723<br>1.164<br>-0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | -2.081<br>-1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519                                      | 1.674<br>1.263<br>0.974<br>1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.871<br>0.874<br>0.872<br>0.872<br>0.872   | 2.051<br>1.470<br>0.588<br>1.116<br>0.959<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.069<br>-0.086<br>-0.123<br>-0.229<br>-0.140<br>-0.142<br>-0.142<br>-0.204<br>-0.250                                     | 3.368<br>2.376<br>1.198<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | 2.922<br>2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.140<br>-0.244<br>-0.250   |
| 4         32.0           5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.07           26         0.08           27         0.00           28         -0.04   | 48         -22.114           72         -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           42         -22.666           45         -18.368           -8         -35.482           66         -30.710           77         -24.640           70         -19.022           24         -31.739  | -0.307<br>-1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.839<br>-6.878<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 30.674<br>26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -20.851<br>-34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | 1.164<br>-0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.113   | -1.374<br>-0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.271<br>0.553<br>0.348<br>0.435<br>0.348<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519                              | 1.263<br>0.974<br>1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.874<br>0.872<br>0.872<br>0.827<br>0.719<br>0.724   | 1.470<br>0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.086<br>-0.0297<br>-0.229<br>-0.123<br>-0.227<br>-0.229<br>-0.140<br>-0.142<br>-0.142<br>-0.204<br>-0.250                          | 2.376<br>1.198<br>1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932  | 2.012<br>0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.096<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.244<br>-0.250  |
| 5         27.2           6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04  | -35.032           80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           -8         -35.482           -6         -30.710           77         -24.640           0         -19.022           24         -31.739  | -1.133<br>-2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 26.895<br>27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -34.058<br>-29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -0.546<br>-1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.113  | -0.377<br>-0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 0.974<br>1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.827<br>0.719<br>0.724  | 0.588<br>1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.229<br>-0.229<br>-0.140<br>-0.142<br>-0.142<br>-0.204<br>-0.250  | 1.198<br>1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | 0.698<br>1.421<br>1.210<br>0.019<br>0.291<br>10.338<br>0.265<br>-0.200<br>-0.086<br>-0.089<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 6         28.7           7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.72           23         7.04           24         6.87           25         -0.0           26         0.06           27         0.00           28         -0.04  | 80         -30.467           55         -25.958           56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           -8         -35.482           66         -30.710           0         -19.022           24         -31.739   | -2.172<br>-2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 27.900<br>27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -29.194<br>-24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-21.7541<br>-34.763<br>-29.987   | -1.056<br>-1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | -0.880<br>-0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.530<br>0.474<br>0.204<br>0.557<br>0.519  | 1.273<br>1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.872<br>0.878<br>0.914<br>0.871<br>0.814<br>0.871<br>0.814<br>0.872<br>0.827<br>0.827<br>0.719<br>0.724   | 1.116<br>0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 1.908<br>1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932  | 1.421<br>1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 7         28.5           8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04  | -25.958           -25.958           -21.101           97           -35.352           38           -30.604           16           -25.446           92           92.20.070           13           -35.233           41           -29.912           45           -24.625           70           -19.070           -34.661           58           -29.611           42           -22.666           45           -18.368           .8           -35.482           66           -30.710           0           -19.022           24           -31.739   | -2.262<br>-2.366<br>-4.173<br>-4.146<br>-4.354<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 27.819<br>28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -24.864<br>-20.036<br>-34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -1.303<br>-2.348<br>-3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.888<br>-6.926<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.066<br>-7.113  | -0.737<br>0.004<br>0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 1.095<br>1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.871<br>0.814<br>0.827<br>0.827<br>0.719<br>0.724   | 0.959<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.224<br>-0.250  | 1.631<br>1.065<br>1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | 1.210<br>0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.244<br>-0.250   |
| 8         28.0           9         24.6           10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04   | 56         -21.101           97         -35.352           38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -34.661           58         -29.611           42         -22.666           45         -18.368           .8         -35.482           6         -30.710           .7         -24.640           0         -19.022           24         -31.739  | -4.173<br>-4.146<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 28.060<br>25.046<br>24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -34.348<br>-29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -3.882<br>-3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.348<br>0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 1.065<br>1.004<br>1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724   | 0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.142<br>-0.204<br>-0.250  | 1.102<br>1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | 0.019<br>0.291<br>0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 10         24.6           11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.05           27         0.00           28         -0.04   | 38         -30.604           16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           66         -30.712           77         -24.640           10         -19.022           24         -31.739  | -4.146<br>-4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 24.759<br>24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -29.521<br>-24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | -3.808<br>-4.089<br>-4.549<br>-6.962<br>-6.962<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.066<br>-7.113  | 0.121<br>-0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 1.083<br>1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.827<br>0.719<br>0.724   | 0.338<br>0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.142<br>-0.204<br>-0.250   | 1.141<br>1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | 0.338<br>0.265<br>-0.200<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 11         24.6           12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.05           27         0.00           28         -0.04   | 16         -25.446           92         -20.070           13         -35.233           41         -29.912           45         -24.621           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           6         -30.710           77         -24.640           0         -19.022           24         -31.739   | -4.354<br>-4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 24.615<br>24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -24.334<br>-19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -4.089<br>-4.549<br>-6.962<br>-6.888<br>-6.926<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.056<br>-7.113  | -0.001<br>0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 1.113<br>0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724  | 0.265<br>-0.200<br>-0.096<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  | 1.144<br>0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | 0.265<br>-0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   |
| 12         24.6           13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           23         7.04           24         6.87           25         -0.07           26         0.06           27         0.00           28         -0.04   | 92         -20.070           13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           66         -30.710           7         -24.640           0         -19.022           24         -31.739  | -4.349<br>-6.866<br>-6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 24.963<br>19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -19.198<br>-34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | -4.549<br>-6.962<br>-6.888<br>-6.926<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.271<br>0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 0.872<br>1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724  | -0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 0.935<br>1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | -0.200<br>-0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 13         19.0           14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04   | 13         -35.233           41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           .8         -35.482           66         -30.710           7         -24.640           0         -19.022           24         -31.739  | -6.866<br>-6.820<br>-6.839<br>-6.878<br>-6.878<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 19.567<br>19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -34.214<br>-28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -6.962<br>-6.888<br>-6.926<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.553<br>0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 1.018<br>0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724   | -0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 1.163<br>1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | -0.096<br>-0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 14         18.9           15         18.6           16         18.4           17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.08           27         0.00           28         -0.04   | 41         -29.912           45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           8         -35.482           66         -30.710           77         -24.640           00         -19.022           24         -31.739  | -6.820<br>-6.840<br>-6.839<br>-6.878<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 19.329<br>19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -28.930<br>-23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | -6.888<br>-6.926<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.388<br>0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 0.982<br>0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724  | -0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 1.058<br>0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | -0.069<br>-0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 15         18.6           16         18.4           17         13.5           18         13.1           19         13.0           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.01           26         0.02           27         0.00           28         -0.04   | 45         -24.625           70         -19.017           90         -34.661           58         -29.611           42         -22.666           45         -18.368           88         -35.482           66         -30.710           77         -24.640           10         -19.022           24         -31.739  | -6.840<br>-6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 19.080<br>18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -23.747<br>-18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -6.926<br>-6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.435<br>0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 0.878<br>0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724   | -0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 0.984<br>0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | -0.086<br>-0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 16         18.4           17         13.5           18         13.1           19         13.0           20         13.0           21         6.7           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04  | -19.017           -34.661           58         -29.611           42         -22.666           45         -18.368           -8         -35.482           66         -30.710           77         -24.640           10         -19.022           24         -31.739   | -6.839<br>-6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 18.818<br>14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -18.102<br>-33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | -6.962<br>-7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.348<br>0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 0.914<br>0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724  | -0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 0.986<br>1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925   | -0.123<br>-0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 17         13.5           18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04   | 90         -34.661           58         -29.611           42         -22.666           45         -18.368           88         -35.482           66         -30.710           77         -24.640           10         -19.022           24         -31.739  | -6.878<br>-6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 14.120<br>13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -33.790<br>-28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987   | -7.174<br>-7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.530<br>0.474<br>0.404<br>0.204<br>0.557<br>0.519   | 0.871<br>0.814<br>0.872<br>0.827<br>0.719<br>0.724   | -0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 1.062<br>0.969<br>0.972<br>0.864<br>0.932<br>0.925  | -0.297<br>-0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 18         13.1           19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.07           26         0.06           27         0.00           28         -0.04   | 558         -29.611           42         -22.666           45         -18.368           48         -35.482           46         -30.710           47         -24.640           10         -19.022           24         -31.739  | -6.816<br>-6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 13.632<br>13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -28.797<br>-21.794<br>-17.541<br>-34.763<br>-29.987  | -7.045<br>-6.962<br>-7.052<br>-7.066<br>-7.113  | 0.474<br>0.404<br>0.204<br>0.557<br>0.519  | 0.814<br>0.872<br>0.827<br>0.719<br>0.724  | -0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250   | 0.969<br>0.972<br>0.864<br>0.932<br>0.925   | -0.229<br>-0.140<br>-0.142<br>-0.204<br>-0.250  |
| 19         13.1           20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.06           27         0.00           28         -0.04   | 42         -22.666           45         -18.368           8         -35.482           6         -30.710           .7         -24.640           .0         -19.022           24         -31.739  | -6.822<br>-6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 13.546<br>13.249<br>7.305<br>7.485<br>7.469   | -21.794<br>-17.541<br>-34.763<br>-29.987   | -6.962<br>-7.052<br>-7.066<br>-7.113  | 0.404<br>0.204<br>0.557<br>0.519   | 0.872<br>0.827<br>0.719<br>0.724   | -0.140<br>-0.142<br>-0.204<br>-0.250   | 0.972<br>0.864<br>0.932<br>0.925  | -0.140<br>-0.142<br>-0.204<br>-0.250  |
| 20         13.0           21         6.74           22         6.96           23         7.04           24         6.87           25         -0.02           26         0.08           27         0.00           28         -0.04   | 45         -18.368           -8         -35.482           66         -30.710           .7         -24.640           .0         -19.022           24         -31.739   | -6.910<br>-6.863<br>-6.863<br>-6.875<br>-6.909  | 13.249<br>7.305<br>7.485<br>7.469   | -17.541<br>-34.763<br>-29.987  | -7.052<br>-7.066<br>-7.113  | 0.204<br>0.557<br>0.519  | 0.827<br>0.719<br>0.724  | -0.142<br>-0.204<br>-0.250   | 0.864<br>0.932<br>0.925   | -0.142<br>-0.204<br>-0.250  |
| 22         6.96           23         7.04           24         6.87           25         -0.02           26         0.02           27         0.002           28         -0.04  | 6 -30.710<br>7 -24.640<br>70 -19.022<br>24 -31.739  | -6.863<br>-6.875<br>-6.909  | 7.485<br>7.469  | -29.987  | -7.113  | 0.519  | 0.724  | -0.250   | 0.925   | -0.250  |
| 23         7.04           24         6.87           25         -0.02           26         0.08           27         0.00           28         -0.04   | 7 -24.640<br>70 -19.022<br>24 -31.739   | -6.875<br>-6.909  | 7.469   |  |   |  |  |  |   |   |
| 24 6.87<br>25 -0.00<br>26 0.08<br>27 0.00<br>28 -0.04   | 0 -19.022<br>24 -31.739   | -6.909  |   | -23.902  | -7.037  | 0.421  | 0.738  | -0.162   |   |   |
| 25 -0.02<br>26 0.08<br>27 0.00<br>28 -0.04  | -31.739   |   | 7115  |  |   |  |  |  | 0.865   | -0.162  |
| 26 0.08<br>27 0.00<br>28 -0.04  |   | -2 889  |   | -18.268  | -7.046  | 0.275  | 0.754  | -0.137   | 0.814   | -0.137  |
| 27 0.00<br>28 -0.04   |   |   | 0.621   | -31.108  | -3.031  | 0.645  | 0.630  | -0.142   | 0.913   | -0.142  |
| 28 -0.04  |   | -2.871  | 0.593   | -27.207  | -3.009  | 0.507  | 0.560  | -0.138   | 0.767   | -0.138  |
|   |   | -2.884  | 0.426   | -23.991<br>-19.008   | -3.019  | 0.424  | 0.578  | -0.135<br>-0.159   | 0.730   | -0.135<br>-0.159  |
| Note: Crush colun   | -13.011   | -2.500  | 0.000   | -19.000  | -0.000  | 0.000  | 0.000  | -0.155   | 0.717   | -0.108  |
| Note: Crush colun   |   |   |   |  |   |  |  |  |   |   |
| DOOR  | 22  | 23 24   | 6<br>20<br>4  | ASHBE  |   |  |  |  | DC  | JOR   |
|   | 25  | 26/27 28  |   | X  | Y   |  |  |  |   |   |

Figure E-1. Floor Pan Deformation Data – Set 1, Test No. NJPCB-7

| Date:         2/27/2018           Year:         2010           Year:         2010           1         56.526           2         58.261           3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767           1         1           14 | Y<br>(in.)<br>-34.264<br>-29.707<br>-25.465<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-29.314<br>-29.314<br>-28.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481<br>-24.226 | Z<br>(in.)<br>2.717<br>0.910<br>-0.048<br>-0.043<br>-0.787<br>-1.845<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.212<br>-6.212<br>-6.212<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.940<br>-5.940<br>-1.793                  | VEHICLE  | dge<br>PRE/POST<br>ORPAN - SI<br>Y'<br>(in.)<br>-33.926<br>-28.614<br>-24.617<br>-21.210<br>-34.347<br>-29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421<br>-31.323 | Model:  | ΔX<br>(in.)<br>-1.318<br>-2.578<br>-2.114<br>-1.151<br>-0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097<br>0.285 |   |   | Total Δ<br>(in.)           1.415           3.132           2.726           1.511           0.583           1.249           1.013           0.749           0.583           0.432           0.528           0.838           0.825           0.695           0.663           0.923           0.803           0.668           0.627           0.755           0.605 | Crush<br>(in.)<br>1.374<br>2.935<br>2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.543<br>-0.636<br>-0.556 |
|---|--|---|--|---|---|---|---|---|--|--|
| POINT         (in.)           1         56.526           2         58.261           3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | (in.)<br>-34.264<br>-29.707<br>-25.465<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.660<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481                            | (in.)<br>2.717<br>0.910<br>-0.043<br>-0.043<br>-0.787<br>-1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.785<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.163<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.940<br>-1.793   | FLO<br>X'<br>(in.)<br>55.208<br>55.684<br>57.024<br>57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.621<br>51.349<br>51.181<br>51.601<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597 | ORPAN - SI<br>Y'<br>(in.)<br>-33.926<br>-28.614<br>-24.617<br>-21.210<br>-34.347<br>-29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421                               | Z'<br>(in.)<br>3.108<br>2.313<br>1.449<br>0.763<br>-0.842<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.996<br>-6.965<br>-6.825<br>-6.796<br>-6.623<br>-6.623<br>-6.647<br>-6.623<br>-6.638<br>-6.636<br>-6.492<br>-6.425 | (in.)<br>-1.318<br>-2.578<br>-2.114<br>-1.151<br>-0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097                | (in.)<br>0.338<br>1.093<br>0.849<br>0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151 | (in.)<br>0.391<br>1.403<br>1.497<br>0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.543<br>-0.673<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.666<br>-0.566 | (in.)<br>1.415<br>3.132<br>2.726<br>1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.755<br>0.605   | (in.)<br>1.374<br>2.935<br>2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556                    |
| POINT         (in.)           1         56.526           2         58.261           3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | (in.)<br>-34.264<br>-29.707<br>-25.465<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.660<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481                            | (in.)<br>2.717<br>0.910<br>-0.043<br>-0.043<br>-0.787<br>-1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.785<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.163<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.940<br>-1.793   | (in.)<br>55.208<br>55.684<br>57.024<br>57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597                        | (in.)<br>-33.926<br>-28.614<br>-24.617<br>-21.210<br>-34.347<br>-29.449<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | (in.)<br>3.108<br>2.313<br>1.449<br>0.763<br>-0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.623<br>-6.623<br>-6.636<br>-6.636<br>-6.492<br>-6.425                           | (in.)<br>-1.318<br>-2.578<br>-2.114<br>-1.151<br>-0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097                | (in.)<br>0.338<br>1.093<br>0.849<br>0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151 | (in.)<br>0.391<br>1.403<br>1.497<br>0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.543<br>-0.673<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.663<br>-0.666<br>-0.566 | (in.)<br>1.415<br>3.132<br>2.726<br>1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.755<br>0.605   | (in.)<br>1.374<br>2.935<br>2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556                    |
| 1         56.526           2         58.261           3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -34.264<br>-29.707<br>-25.465<br>-21.765<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.660<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481               | 2.717<br>0.910<br>-0.048<br>-0.043<br>-0.787<br>-1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.940<br>-1.793  | 55.208<br>55.684<br>57.024<br>57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597                                 | -33.926<br>-28.614<br>-24.617<br>-21.210<br>-34.347<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | 3 108<br>2 313<br>1.449<br>0.763<br>-0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.765<br>-6.974<br>-6.623<br>-6.647<br>-6.636<br>-6.492<br>-6.425  | -1.318<br>-2.578<br>-2.114<br>-1.151<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.338<br>1.093<br>0.849<br>0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151          | 0.391<br>1.403<br>1.497<br>0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.663<br>-0.656  | 1.415<br>3.132<br>2.726<br>1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.635<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.6687<br>0.6627<br>0.795<br>0.755<br>0.605   | 1.374<br>2.935<br>2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.543<br>-0.673<br>-0.673<br>-0.673   |
| 2         58.261           3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -29.707<br>-25.465<br>-21.765<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481                          | 0.910<br>-0.048<br>-0.043<br>-0.787<br>-1.845<br>-1.845<br>-1.845<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.936<br>-5.930<br>-5.940<br>-1.793 | 55.684<br>57.024<br>57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -28.614<br>-24.617<br>-21.210<br>-34.347<br>-29.449<br>-20.258<br>-34.586<br>-29.863<br>-29.863<br>-29.863<br>-29.863<br>-29.863<br>-29.863<br>-29.194<br>-33.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421                                      | 2.313<br>1.449<br>0.763<br>-0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.765<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425   | -2.578<br>-2.114<br>-1.151<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.224<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 1.093<br>0.849<br>0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | 1.403<br>1.497<br>0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.685<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.663<br>-0.663<br>-0.666<br>-0.656   | 3.132<br>2.726<br>1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.635<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | 2.935<br>2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.685<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.686<br>-0.556  |
| 3         59.137           4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -25.465<br>-21.765<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481                                     | -0.048<br>-0.043<br>-0.787<br>-1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.605<br>-6.038<br>-6.104<br>-5.949<br>-5.940<br>-5.940<br>-1.793                    | 57.024<br>57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -24.617<br>-21.210<br>-34.347<br>-29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | 1.449<br>0.763<br>-0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.623<br>-6.647<br>-6.623<br>-6.638<br>-6.636<br>-6.492<br>-6.425                                  | -2.114<br>-1.151<br>-0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.849<br>0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | 1.497<br>0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.656  | 2.726<br>1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.638<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.755<br>0.605   | 2.590<br>1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.583<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 4         58.923           5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -21.765<br>-34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -0.043<br>-0.787<br>-1.845<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.225<br>-6.212<br>-6.212<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.940<br>-5.940<br>-1.793  | 57.772<br>53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -21.210<br>-34.347<br>-29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | 0.763<br>-0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425   | -1.151<br>-0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.555<br>0.310<br>0.608<br>0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | 0.806<br>-0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.6686<br>-0.556  | 1.511<br>0.583<br>1.249<br>1.013<br>0.749<br>0.528<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | 1.405<br>0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.6686<br>-0.556   |
| 5         54.142           6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.117           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -34.657<br>-30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -0.787<br>-1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.940<br>-1.793  | 53.651<br>54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -34.347<br>-29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -0.842<br>-1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | -0.491<br>-0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.310<br>0.608<br>0.438<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.056<br>0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.663<br>-0.663<br>-0.656  | 0.583<br>1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | 0.494<br>1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.743<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556   |
| 6         55.613           7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         3.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -30.057<br>-25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -1.845<br>-1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.940<br>-1.793  | 54.650<br>54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -29.449<br>-25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -1.332<br>-1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | -0.963<br>-0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.608<br>0.438<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | 0.513<br>0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.673<br>-0.666<br>-0.566  | 1.249<br>1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755   | 1.091<br>0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.510<br>-0.543<br>-0.543<br>-0.673<br>-0.668<br>-0.556  |
| 7         55.385           8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -25.532<br>-20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -1.898<br>-1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.940<br>-1.793  | 54.552<br>54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -25.094<br>-20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -1.524<br>-2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | -0.833<br>-0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.438<br>0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | 0.374<br>-0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.6686<br>-0.566  | 1.013<br>0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755   | 0.913<br>0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.578<br>-0.578<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556   |
| 8         54.868           9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -20.687<br>-35.010<br>-30.233<br>-25.074<br>-19.776<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -1.964<br>-3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 54.741<br>51.621<br>51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -20.258<br>-34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -2.566<br>-4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.638<br>-6.492<br>-6.425  | -0.126<br>0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.428<br>0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.602<br>-0.375<br>-0.216<br>-0.273<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.543<br>-0.673<br>-0.686<br>-0.566  | 0.749<br>0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | 0.615<br>-0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  |
| 9         51.484           10         51.407           11         51.385           12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -35.010<br>-30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -3.755<br>-3.716<br>-3.885<br>-3.862<br>-6.225<br>-6.212<br>-6.212<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.940<br>-5.936<br>-5.940<br>-1.793  | 51.621<br>51.349<br>51.181<br>51.601<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -34.586<br>-29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -4.130<br>-3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.137<br>-0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.425<br>0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | -0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.583<br>0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.375<br>-0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.578<br>-0.578<br>-0.578<br>-0.543<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 10         51.407           11         51.385           12         51.442           13         45.672           14         45.682           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -30.233<br>-25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -3.716<br>-3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 51.349<br>51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -29.863<br>-24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -3.932<br>-4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.765<br>-6.765<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | -0.058<br>-0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.370<br>0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.566  | 0.432<br>0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.216<br>-0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556   |
| 11         51.385           12         51.442           13         45.672           14         45.62           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767  | -25.074<br>-19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-35.106<br>-32.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -3.885<br>-3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 51.181<br>51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -24.672<br>-19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -4.158<br>-4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.623<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | -0.205<br>0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.402<br>0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | -0.273<br>-0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.566  | 0.528<br>0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.273<br>-0.737<br>-0.666<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.673<br>-0.686<br>-0.556   |
| 12         51.442           13         45.672           14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -19.776<br>-34.756<br>-29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -3.862<br>-6.299<br>-6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 51.601<br>46.060<br>45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.948<br>33.960<br>33.902<br>33.597   | -19.410<br>-34.461<br>-29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -4.599<br>-6.965<br>-6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.623<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.158<br>0.388<br>0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.366<br>0.295<br>0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.838<br>0.825<br>0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | -0.737<br>-0.666<br>-0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 14         45.582           15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -29.442<br>-24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -6.225<br>-6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 45.802<br>45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -29.169<br>-23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -6.825<br>-6.796<br>-6.765<br>-6.974<br>-6.623<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.636<br>-6.492<br>-6.425  | 0.220<br>0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.273<br>0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.695<br>0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | -0.601<br>-0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 15         45.317           16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -24.191<br>-18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -6.212<br>-6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 45.531<br>45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -23.900<br>-18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -6.796<br>-6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.214<br>0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.291<br>0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | -0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.687<br>0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.585<br>-0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 16         45.141           17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -18.574<br>-34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -6.187<br>-6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 45.266<br>40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -18.275<br>-33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -6.765<br>-6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.125<br>0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.299<br>0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.663<br>0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | -0.578<br>-0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 17         40.280           18         39.849           19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -34.310<br>-29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -6.163<br>-6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 40.582<br>40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -33.988<br>-29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -6.974<br>-6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.492<br>-6.425  | 0.302<br>0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.322<br>0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151   | -0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.923<br>0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.810<br>-0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 18         39.849           19         39.858           20         39.686           21         33.674           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -29.314<br>-22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -6.065<br>-6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 40.120<br>39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -29.056<br>-21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -6.776<br>-6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.492<br>-6.425  | 0.271<br>0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.258<br>0.299<br>0.304<br>0.197<br>0.131<br>0.151  | -0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.803<br>0.668<br>0.627<br>0.795<br>0.755<br>0.605   | -0.710<br>-0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 19         39.858           20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -22.281<br>-18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -6.038<br>-6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 39.977<br>39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -21.982<br>-17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421  | -6.623<br>-6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.119<br>0.075<br>0.374<br>0.286<br>0.182<br>0.097  | 0.299<br>0.304<br>0.197<br>0.131<br>0.151   | -0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556  | 0.668<br>0.627<br>0.795<br>0.755<br>0.605  | -0.585<br>-0.543<br>-0.673<br>-0.686<br>-0.556   |
| 20         39.686           21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -18.060<br>-35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -6.104<br>-5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 39.761<br>33.848<br>33.960<br>33.902<br>33.597   | -17.756<br>-34.909<br>-30.154<br>-24.079<br>-18.421   | -6.647<br>-6.638<br>-6.636<br>-6.492<br>-6.425  | 0.075<br>0.374<br>0.286<br>0.182<br>0.097   | 0.304<br>0.197<br>0.131<br>0.151  | -0.543<br>-0.673<br>-0.686<br>-0.556  | 0.627<br>0.795<br>0.755<br>0.605   | -0.543<br>-0.673<br>-0.686<br>-0.556   |
| 21         33.474           22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -35.106<br>-30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481   | -5.965<br>-5.949<br>-5.936<br>-5.940<br>-1.793  | 33.848<br>33.960<br>33.902<br>33.597   | -34.909<br>-30.154<br>-24.079<br>-18.421  | -6.638<br>-6.636<br>-6.492<br>-6.425  | 0.374<br>0.286<br>0.182<br>0.097  | 0.197<br>0.131<br>0.151   | -0.673<br>-0.686<br>-0.556  | 0.795<br>0.755<br>0.605  | -0.673<br>-0.686<br>-0.556   |
| 22         33.674           23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -30.285<br>-24.231<br>-18.619<br>-31.407<br>-27.481  | -5.949<br>-5.936<br>-5.940<br>-1.793  | 33.960<br>33.902<br>33.597   | -30.154<br>-24.079<br>-18.421   | -6.636<br>-6.492<br>-6.425  | 0.286<br>0.182<br>0.097   | 0.131<br>0.151  | -0.686<br>-0.556  | 0.755<br>0.605   | -0.686<br>-0.556   |
| 23         33.719           24         33.500           25         26.894           26         26.955           27         26.828           28         26.767   | -24.231<br>-18.619<br>-31.407<br>-27.481   | -5.936<br>-5.940<br>-1.793  | 33.902<br>33.597   | -24.079<br>-18.421  | -6.492<br>-6.425  | 0.182<br>0.097  | 0.151   | -0.556  | 0.605  | -0.556   |
| 24 33.500<br>25 26.894<br>26 26.955<br>27 26.828<br>28 26.767   | -18.619<br>-31.407<br>-27.481  | -1.793  |  |   | -6.425  | 0.097   | 0.198   | -0.485  |  | 0.405  |
| 26         26.955           27         26.828           28         26.767   | -27.481  |   | 27.178   | -31.323   | -2.329  | 0.285   |   | 0.400   | 0.533  | -0.485   |
| 27 26.828<br>28 26.767  |  |   |  |   |   | 0.200   | 0.083   | -0.536  | 0.613  | -0.536   |
| 28 26.767   | -24.226  | -1.759  | 27.212   | -27.369   | -2.263  | 0.257   | 0.112   | -0.504  | 0.577  | -0.504   |
|   |  | -1.756  | 27.091   | -24.199   | -2.231  | 0.263   | 0.027   | -0.475  | 0.543  | -0.475   |
| Note: Crush column is   | -19.307  | -1.752  | 26.909   | -19.240   | -2.218  | 0.142   | 0.067   | -0.466  | 0.492  | -0.466   |
| Note: Crush column is   |  |   |  |   |   |   |   |   |  | 2  |
|   | $ \begin{array}{c} 1 & 2 \\ 5 & 10 \\ 13 & 14 \\ 17 & 18 \\ 22 \\ 25 & 2 \end{array} $   | 19 2  | 6<br>20<br>4   | ASHBO   | ARD   |   |   |   | DC   | JOR  |

Figure E-2. Floor Pan Deformation Data – Set 2, Test No. NJPCB-7

|                     |          | x                | Y                 | z                | X                | Y                  | Z'               | ΔX             | ΔΥ             | ΔZ               | Total ∆        | Crush            |
|---------------------|----------|------------------|-------------------|------------------|------------------|--------------------|------------------|----------------|----------------|------------------|----------------|------------------|
|                     | POINT    | (in.)            | (in.)             | (in.)            | (in.)            | (in.)              | (in.)            | (in.)          | (in.)          | (in.)            | (in.)          | (in.)            |
|                     | 1        | 12.411           | -25.051           | 27.691           | 13.292           | -23.867            | 27.702           | 0.881          | 1.184          | 0.011            | 1.476          | 1.476            |
| Ŧ                   | 2        | 14.357           | -16.028           | 25.402           | 14.936           | -14.849            | 25.373           | 0.579          | 1.180          | -0.029           | 1.314          | 1.314            |
| DASH                | 3        | 11.151<br>9.984  | -6.412<br>-25.410 | 24.989<br>12.896 | 11.450<br>11.010 | -5.261             | 24.962           | 0.299          | 1.151<br>1.083 | -0.027           | 1.189<br>1.492 | 1.189            |
| Ď                   | 5        | 11.052           | -25.410           | 12.896           | 11.764           | -24.327<br>-15.523 | 12.888<br>12.226 | 1.026<br>0.712 | 1.118          | 0.008            | 1.326          | 1.492            |
|                     | 6        | 8.549            | -6.589            | 13.220           | 8.920            | -5.611             | 13.216           | 0.371          | 0.978          | -0.004           | 1.046          | 1.046            |
|                     | 7        | 21.988           | -38.766           | 5.024            | 23.545           | -36.878            | 5.232            | 1.557          | 1.888          | 0.208            | 2.456          | 1.888            |
| SIDE<br>PANEL       | 8        | 21.900           | -38.632           | 0.837            | 23.040           | -36.648            | 1.062            | 1.599          | 1.984          | 0.208            | 2.456          | 1.984            |
| PAI                 | 9        | 25.142           | -38.727           | 4.506            | 26.657           | -36.742            | 4.717            | 1.535          | 1.986          | 0.212            | 2.506          | 1.986            |
|                     | 10       | -13.495          | -40.512           | 21.402           | -11.633          | -41.736            | 21.164           | 1.862          | -1.223         | -0.238           | 2.240          | -1.223           |
| IMPACT SIDE<br>DOOR | 11       | -0.759           | -40.266           | 21.210           | 1.015            | -40.477            | 21.189           | 1.774          | -0.211         | -0.021           | 1.787          | -0.211           |
| S R                 | 12       | 12.503           | -40.136           | 21.004           | 14.303           | -39.251            | 21.066           | 1.800          | 0.885          | 0.062            | 2.007          | 0.885            |
| 5 Q                 | 13       | -8.632           | -41.873           | 2.699            | -6.523           | -41.535            | 2.513            | 2.109          | 0.339          | -0.186           | 2.144          | 0.339            |
| JP/                 | 14       | -0.394           | -41.987           | 2.314            | 1.723            | -41.187            | 2.217            | 2.117          | 0.801          | -0.097           | 2.266          | 0.801            |
| ≤                   | 15       | 7.151            | -41.820           | -0.018           | 9.147            | -40.444            | -0.006           | 1.996          | 1.376          | 0.013            | 2.424          | 1.376            |
|                     | 16       | 3.994            | -28.835           | 40.601           | 5.289            | -27.810            | 40.611           | 1.295          | 1.024          | 0.010            | 1.651          | 0.010            |
|                     | 17       | 5.843            | -21.619           | 40.820           | 6.837            | -20.482            | 40.845           | 0.995          | 1.137          | 0.025            | 1.511          | 0.025            |
|                     | 18       | 6.601            | -17.116           | 40.889           | 7.337            | -15.937            | 40.952           | 0.735          | 1.179          | 0.063            | 1.391          | 0.063            |
|                     | 19       | 7.170            | -10.433           | 41.010           | 7.741            | -9.227             | 41.014           | 0.571          | 1.206          | 0.005            | 1.334          | 0.005            |
|                     | 20       | 7.222            | -6.659            | 41.031           | 7.582            | -5.434             | 41.058           | 0.360          | 1.226          | 0.027            | 1.278          | 0.027            |
|                     | 21       | -3.518           | -29.028           | 43.553           | -2.184           | -28.224            | 43.504           | 1.334          | 0.805          | -0.049           | 1.559          | -0.049           |
| ROOF                | 22       | -2.604           | -21.671           | 44.037           | -1.603           | -20.825            | 43.992           | 1.001          | 0.846          | -0.045           | 1.312          | -0.045           |
| õ                   | 23<br>24 | -2.061           | -16.954           | 44.197           | -1.168<br>-0.920 | -16.123            | 44.122           | 0.893          | 0.831          | -0.076<br>-0.055 | 1.222          | -0.076           |
|                     | 24       | -1.624<br>-1.336 | -13.172<br>-7.360 | 44.253<br>44.285 | -0.920           | -12.274<br>-6.441  | 44.198<br>44.241 | 0.705<br>0.418 | 0.898<br>0.919 | -0.055           | 1.143          | -0.055<br>-0.044 |
|                     | 26       | -7.096           | -28.187           | 44.115           | -5.796           | -27.575            | 44.035           | 1.299          | 0.612          | -0.044           | 1.438          | -0.044           |
|                     | 27       | -6.350           | -21.357           | 44.538           | -5.286           | -20.723            | 44.460           | 1.064          | 0.635          | -0.078           | 1.241          | -0.078           |
|                     | 28       | -5.752           | -16.472           | 44.703           | -4.970           | -15.816            | 44.636           | 0.782          | 0.655          | -0.066           | 1.022          | -0.066           |
|                     | 29       | -5.267           | -12.626           | 44.763           | -4.636           | -11.942            | 44.693           | 0.630          | 0.684          | -0.070           | 0.933          | -0.070           |
|                     | 30       | -4.952           | -7.164            | 44.785           | -4.533           | -6.414             | 44.719           | 0.419          | 0.750          | -0.066           | 0.862          | -0.066           |
| ~                   | 31       | 4.154            | -34.017           | 38.358           | 5.571            | -32.917            | 38.391           | 1.417          | 1.101          | 0.033            | 1.795          | 1.101            |
| A<br>PILLAR         | 32       | 9.152            | -35.100           | 35.621           | 10.625           | -33.814            | 35.665           | 1.473          | 1.286          | 0.044            | 1.956          | 1.286            |
| יובו                | 33       | 15.181           | -36.383           | 31.468           | 16.795           | -34.890            | 31.541           | 1.614          | 1.494          | 0.073            | 2.201          | 1.494            |
| <u> </u>            | 34       | 19.063           | -37.176           | 28.404           | 20.741           | -35.540            | 28.542           | 1.677          | 1.636          | 0.137            | 2.347          | 1.636            |
|                     | 35       | -22.919          | -38.621           | 21.202           | -20.539          | -38.450            | 21.059           | 2.380          | 0.171          | -0.142           | 2.390          | 0.171            |
| с                   | 36       | -19.309          | -38.559           | 21.398           | -16.944          | -38.206            | 21.280           | 2.365          | 0.353          | -0.118           | 2.394          | 0.353            |
| B<br>PILLAR         | 37       | -23.146          | -37.942           | 27.538           | -20.876          | -37.800            | 27.463           | 2.270          | 0.143          | -0.076           | 2.276          | 0.143            |
| F                   | 38       | -20.098          | -37.972           | 27.066           | -17.810          | -37.703            | 26.948           | 2.289          | 0.269          | -0.118           | 2.307          | 0.269            |
| 830-534             | 39       | -23.927          | -34.091           | 39.069           | -21.929          | -34.104            | 38.860           | 1.998          | -0.013         | -0.209           | 2.009          | -0.013           |
|                     | 40       | -21.029          | -33.945           | 39.390           | -19.046          | -33.793            | 39.285           | 1.983          | 0.152          | -0.105           | 1.992          | 0.152            |

Figure E-3. Occupant Compartment Deformation Data – Set 1, Test No. NJPCB-7

|                     |             |                   |                    |                  |                  | RUSH - SET         | -                |                |                |                  | -                |                |
|---------------------|-------------|-------------------|--------------------|------------------|------------------|--------------------|------------------|----------------|----------------|------------------|------------------|----------------|
|                     | POINT       | <b>X</b><br>(in.) | Y<br>(in.)         | Z<br>(in.)       | X'<br>(in.)      | Y'<br>(in.)        | Z'<br>(in.)      | ΔX<br>(in.)    | ΔY<br>(in.)    | ΔΖ<br>(in.)      | Total ∆<br>(in.) | Crush<br>(in.) |
|                     | 1           | 40.050            | -24.777            | 28.462           | 40.842           | -24.635            | 28.051           | 0.791          | 0.142          | -0.411           | 0.903            | 0.903          |
| Т                   | 2           | 41.903<br>38.670  | -15.809<br>-6.148  | 26.156           | 42.527<br>39.082 | -15.661<br>-6.017  | 25.744<br>25.534 | 0.624          | 0.148          | -0.412<br>-0.339 | 0.762            | 0.762          |
| DASH                | 4           | 36.670            | -0.148             | 25.873<br>13.786 | 39.082           | -0.017             | 13.364           | 0.412          | 0.132          | -0.339           | 0.935            | 0.935          |
|                     | 5           | 38.242            | -16.346            | 13.129           | 38.900           | -16.116            | 12.641           | 0.657          | 0.234          | -0.422           | 0.850            | 0.850          |
|                     | 6           | 35.750            | -6.334             | 14.251           | 36.166           | -6.181             | 13.907           | 0.417          | 0.153          | -0.344           | 0.562            | 0.562          |
|                     | 7           | 49.104            | -38.396            | 5.472            | 50.118           | -37.482            | 5.072            | 1.014          | 0.914          | -0.400           | 1.422            | 0.914          |
| SIDE                | 8           | 49.310            | -38.243            | 1.325            | 50.349           | -37.213            | 0.896            | 1.038          | 1.029          | -0.428           | 1.524            | 1.029          |
| PA                  | 9           | 52.176            | -38.347            | 4.902            | 53.251           | -37.361            | 4.409            | 1.075          | 0.986          | -0.494           | 1.540            | 0.986          |
| ш                   | 10          | 14.004            | -40.315            | 22.800           | 15.142           | -42.245            | 22.340           | 1.138          | -1.930         | -0.460           | 2.287            | -1.930         |
| IMPACT SIDE<br>DOOR | 11          | 26.752            | -40.037            | 22.269           | 27.867           | -41.216            | 21.780           | 1.115          | -1.179         | -0.489           | 1.695            | -1.179         |
| ЕĞ                  | 12          | 40.032            | -39.891            | 21.698           | 41.084           | -40.217            | 21.207           | 1.052          | -0.325         | -0.491           | 1.206            | -0.325         |
| DO                  | 13          | 18.454            | -41.571            | 3.998            | 19.570           | -41.950            | 3.481            | 1.116          | -0.379         | -0.517           | 1.287            | -0.379         |
| MР                  | 14          | 26.659            | -41.669            | 3.342            | 27.720           | -41.741            | 2.801            | 1.061          | -0.072         | -0.541           | 1.193            | -0.072         |
| -                   | 15          | 34.040            | -41.475            | 0.915            | 35.202           | -41.096            | 0.312            | 1.162          | 0.379          | -0.603           | 1.363            | 0.379          |
|                     | 16          | 31.959            | -28.706            | 41.604           | 32.946           | -28.843            | 41.199           | 0.987          | -0.137         | -0.405           | 1.076            | -0.405         |
|                     | 17          | 33.808            | -21.526            | 41.796           | 34.634           | -21.556            | 41.446           | 0.826          | -0.031         | -0.350           | 0.898            | -0.350         |
|                     | 18<br>19    | 34.557<br>35.108  | -16.991<br>-10.278 | 41.869<br>42.013 | 35.601<br>35.997 | -16.648            | 41.560<br>41.709 | 1.044          | 0.343          | -0.309           | 1.142<br>0.974   | -0.309         |
|                     | 20          | 35.108            | -6.506             | 42.013           | 35.997           | -6.214             | 41.709           | 0.889          | 0.297          | -0.303           | 0.899            | -0.303         |
|                     | 20          | 24.565            | -28.843            | 44.746           | 26.045           | -28.971            | 44.341           | 1.480          | -0.128         | -0.405           | 1.540            | -0.200         |
| iu:                 | 22          | 25.433            | -21.484            | 45.248           | 26.684           | -21.549            | 44.890           | 1.251          | -0.065         | -0.358           | 1.303            | -0.358         |
| ROOF                | 23          | 25.971            | -16.836            | 45.413           | 27.162           | -16.898            | 45.050           | 1.191          | -0.062         | -0.363           | 1.247            | -0.363         |
| R                   | 24          | 26.454            | -13.079            | 45.463           | 27.432           | -13.078            | 45.157           | 0.978          | 0.001          | -0.306           | 1.025            | -0.306         |
|                     | 25          | 26.643            | -7.275             | 45.533           | 27.496           | -7.261             | 45.257           | 0.853          | 0.014          | -0.275           | 0.897            | -0.275         |
|                     | 26          | 21.073            | -28.169            | 45.379           | 22.507           | -28.326            | 44.996           | 1.434          | -0.157         | -0.383           | 1.492            | -0.383         |
|                     | 27          | 21.782            | -21.245            | 45.833           | 22.992           | -21.383            | 45.494           | 1.210          | -0.138         | -0.339           | 1.264            | -0.339         |
|                     | 28          | 22.312            | -16.343            | 46.013           | 23.367           | -16.620            | 45.702           | 1.055          | -0.277         | -0.311           | 1.134            | -0.311         |
|                     | 29          | 22.875            | -12.529            | 46.066           | 23.786           | -12.653            | 45.781           | 0.912          | -0.124         | -0.284           | 0.963            | -0.284         |
|                     | 30          | 23.109            | -7.024             | 46.118           | 23.837           | -7.135             | 45.871           | 0.728          | -0.111         | -0.247           | 0.777            | -0.247         |
| Ц                   | 31          | 32.076<br>37.040  | -33.838<br>-34.905 | 39.304           | 33.745<br>38.724 | -33.579<br>-34.467 | 38.829           | 1.669          | 0.259          | -0.474           | 1.754            | 0.259          |
| A<br>PILLAR         | 32<br>33    | 42.909            | -34.905            | 36.402<br>32.164 | 38.724<br>44.712 | -34.467<br>-35.510 | 35.942<br>31.574 | 1.684<br>1.803 | 0.438<br>0.641 | -0.460<br>-0.590 | 1.800 2.002      | 0.438<br>0.641 |
| Ы                   | 34          | 46.656            | -36.907            | 29.022           | 48.492           | -36.134            | 28.493           | 1.836          | 0.773          | -0.530           | 2.002            | 0.773          |
|                     | 35          | 4.549             | -38.446            | 22.862           | 6.434            | -38.869            | 22.425           | 1.885          | -0.423         | -0.437           | 1.980            | -0.423         |
|                     | 36          | 8.191             | -38.376            | 22.002           | 9.997            | -38.682            | 22.531           | 1.806          | -0.306         | -0.440           | 1.884            | -0.425         |
| AR                  | 37          | 4.515             | -37.781            | 29.302           | 6.419            | -38.306            | 28.812           | 1.905          | -0.525         | -0.490           | 2.036            | -0.525         |
| B<br>PILLAR         | 38          | 7.546             | -37.809            | 28.701           | 9.416            | -38.227            | 28.243           | 1.871          | -0.418         | -0.458           | 1.971            | -0.418         |
| с.                  | 39          | 4.052             | -34.006            | 40.765           | 5.817            | -34.694            | 40.379           | 1.765          | -0.688         | -0.385           | 1.933            | -0.688         |
|                     | 40          | 6.879             | -33.847            | 41.044           | 8.633            | -34.448            | 40.656           | 1.754          | -0.601         | -0.387           | 1.895            | -0.601         |
| ote: Cru            | sh column i | s deformatio      | n perpendic        | ular to the p    | plane area       | of interest        |                  |                |                |                  |                  |                |

Figure E-4. Occupant Compartment Deformation Data – Set 2, Test No. NJPCB-7

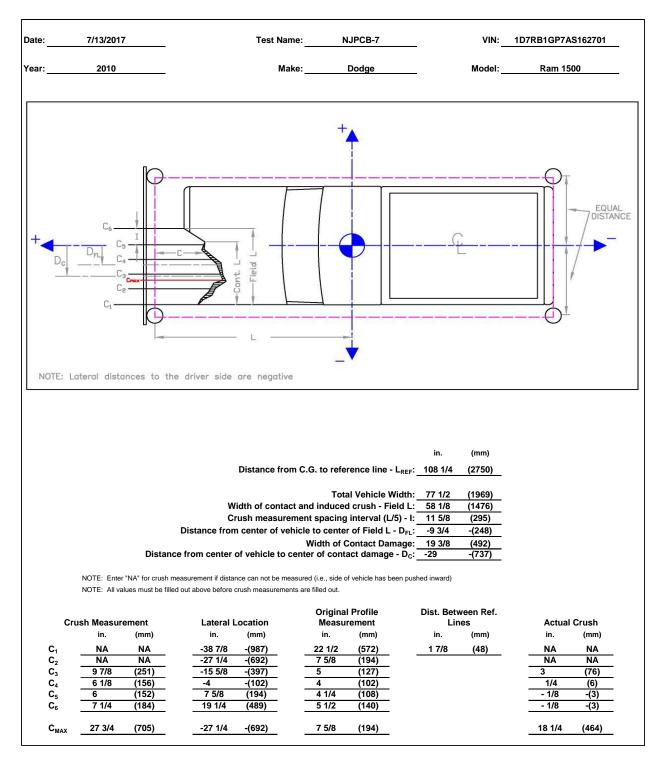


Figure E-5. Exterior Vehicle Crush (NASS) - Front, Test No. NJPCB-7

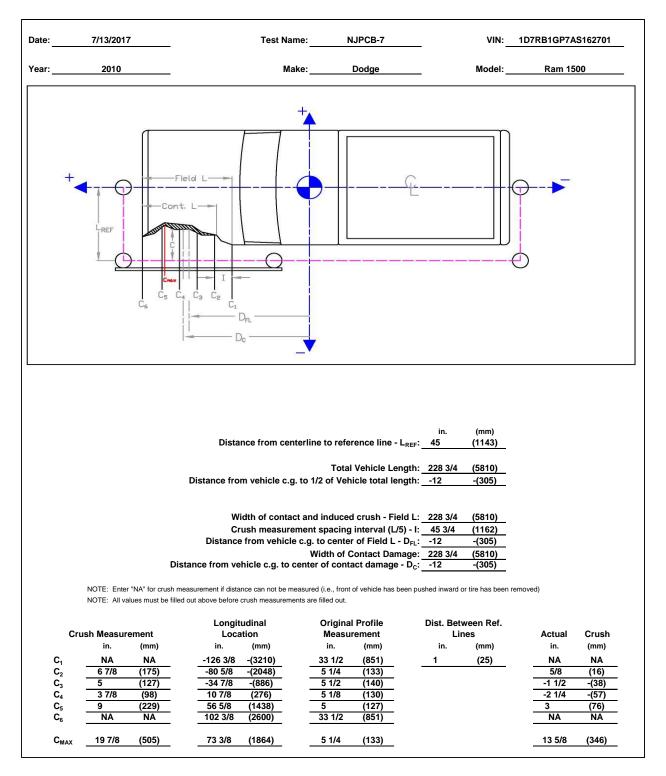


Figure E-6. Exterior Vehicle Crush (NASS) - Side, Test No. NJPCB-7

## Appendix F. Accelerometer and Rate Transducer Data Plots

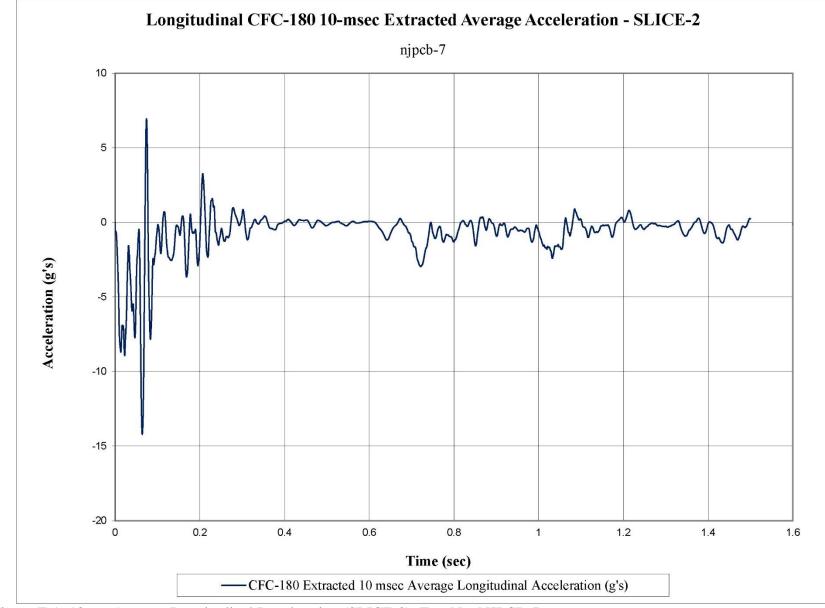


Figure F-1. 10-ms Average Longitudinal Deceleration (SLICE-2), Test No. NJPCB-7

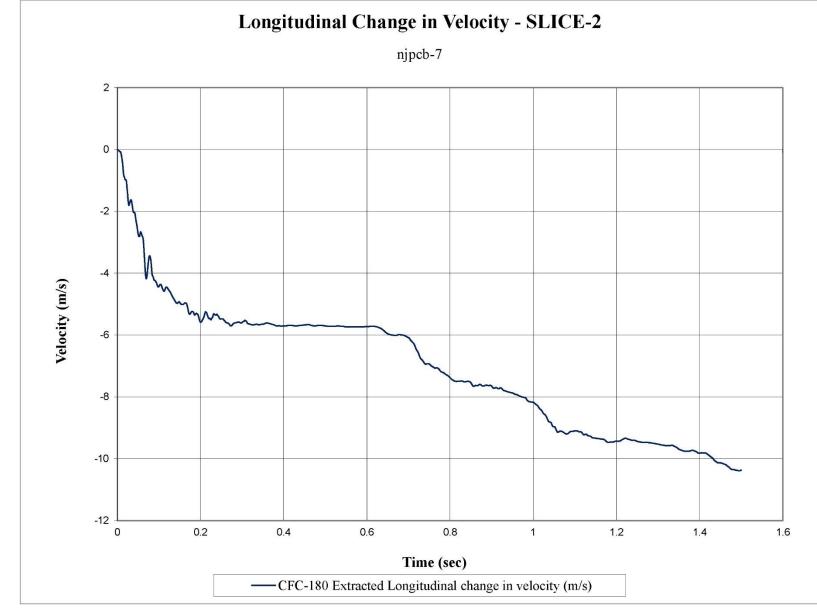


Figure F-2. Longitudinal Occupant Impact Velocity (SLICE-2), Test No. NJPCB-7

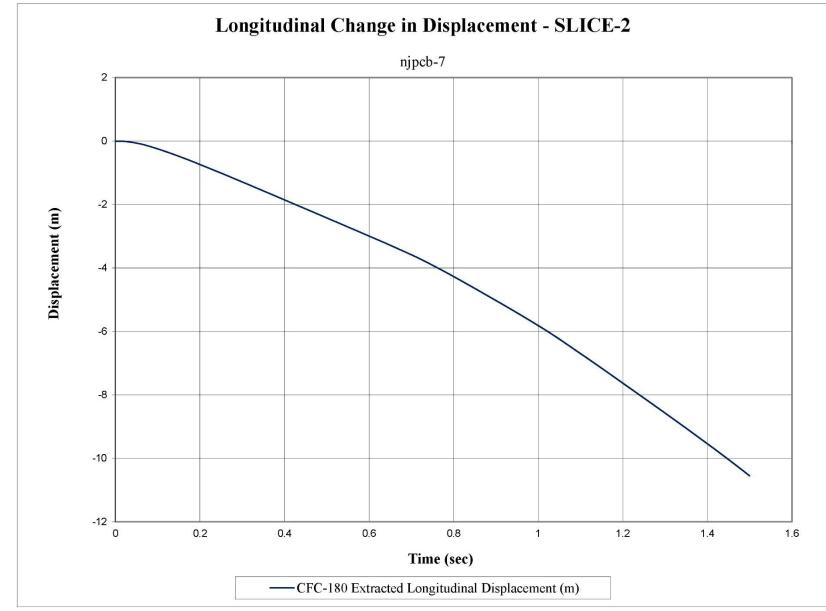


Figure F-3. Longitudinal Occupant Displacement (SLICE-2), Test No. NJPCB-7

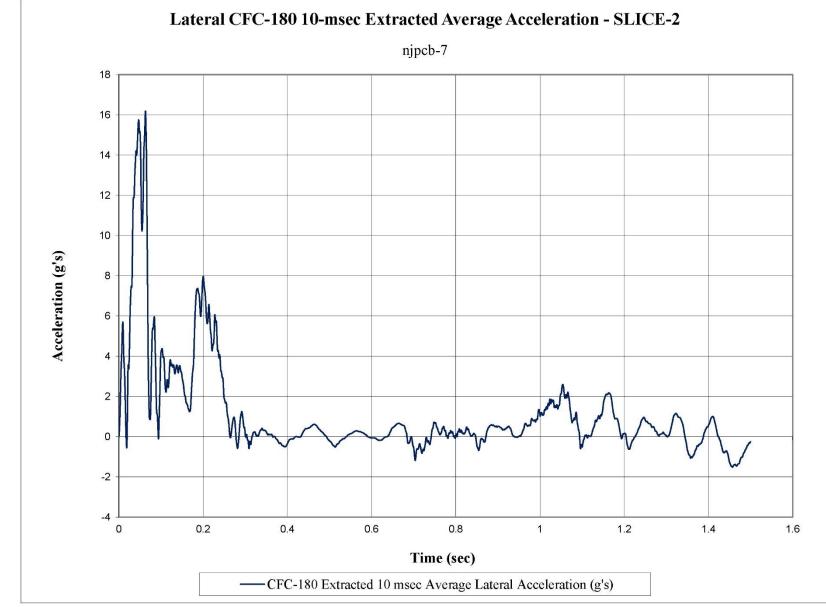


Figure F-4. 10-ms Average Lateral Deceleration (SLICE-2), Test No. NJPCB-7

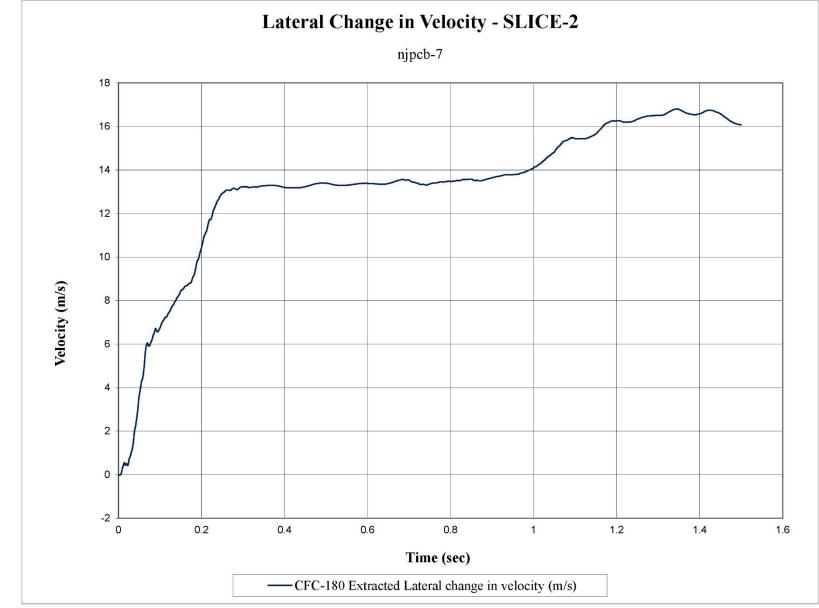


Figure F-5. Lateral Occupant Impact Velocity (SLICE-2), Test No. NJPCB-7

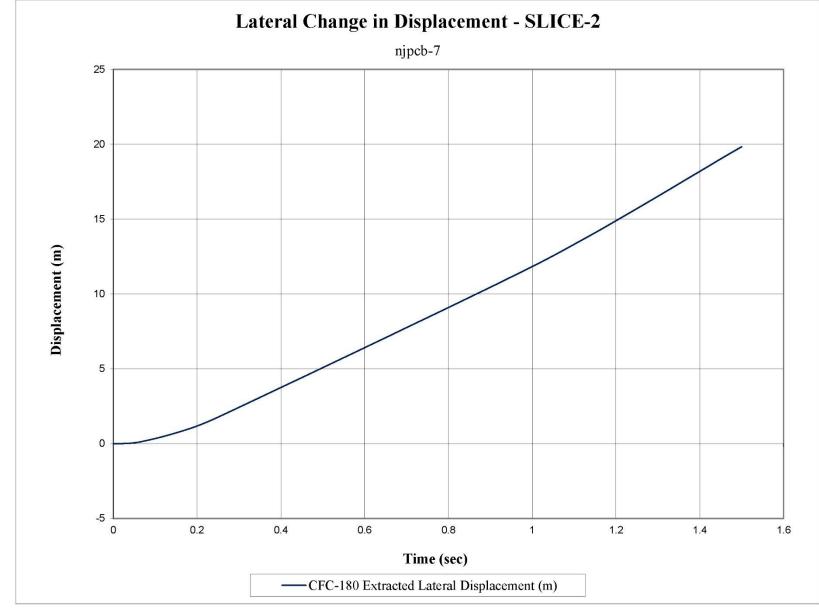


Figure F-6. Lateral Occupant Displacement (SLICE-2), Test No. NJPCB-7

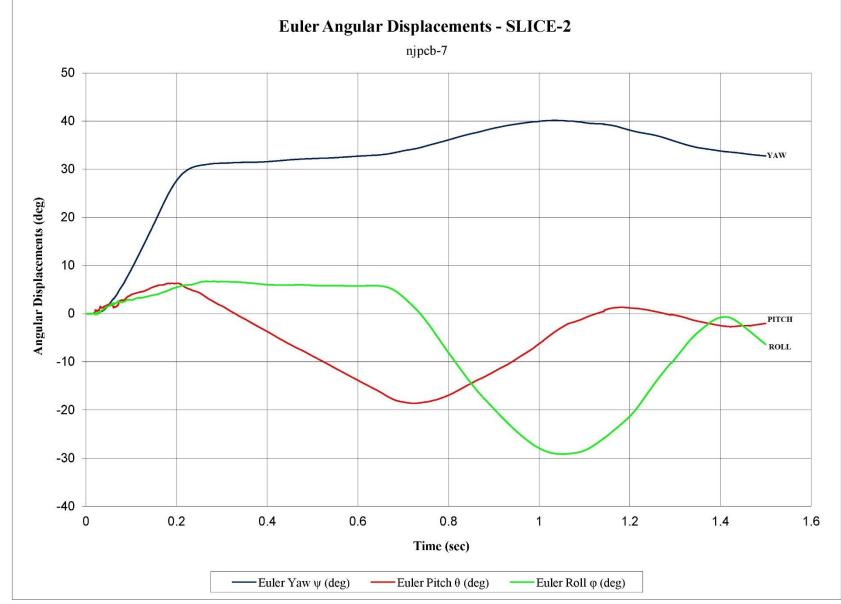


Figure F-7. Vehicle Angular Displacements (SLICE-2), Test No. NJPCB-7

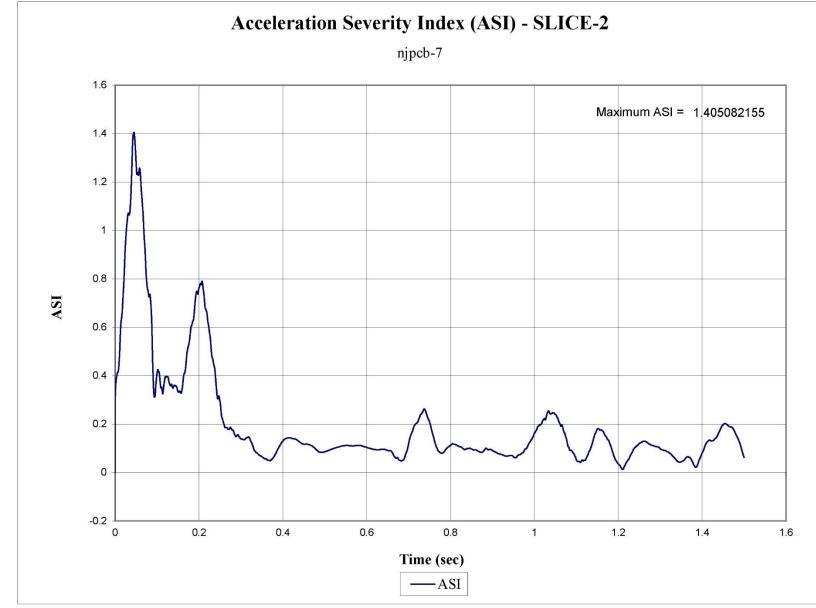


Figure F-8. Acceleration Severity Index (SLICE-2), Test No. NJPCB-7

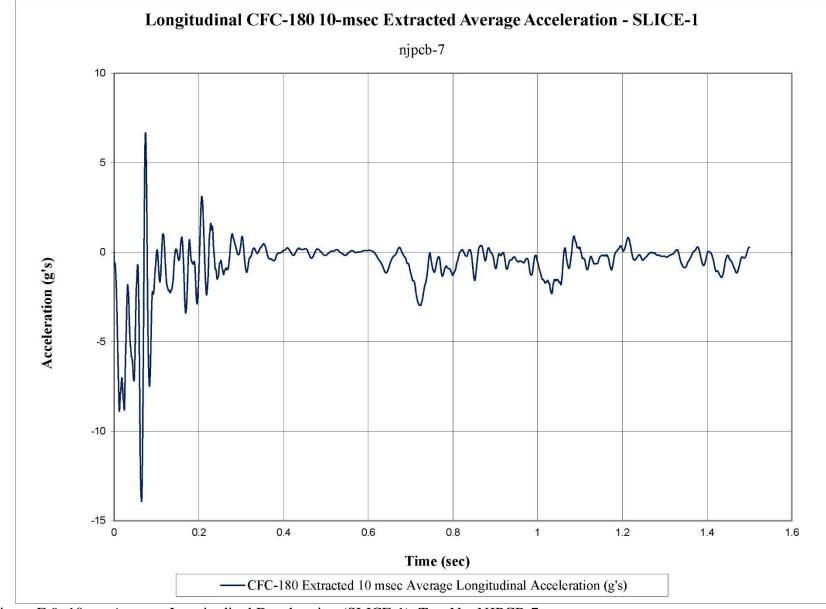


Figure F-9. 10-ms Average Longitudinal Deceleration (SLICE-1), Test No. NJPCB-7

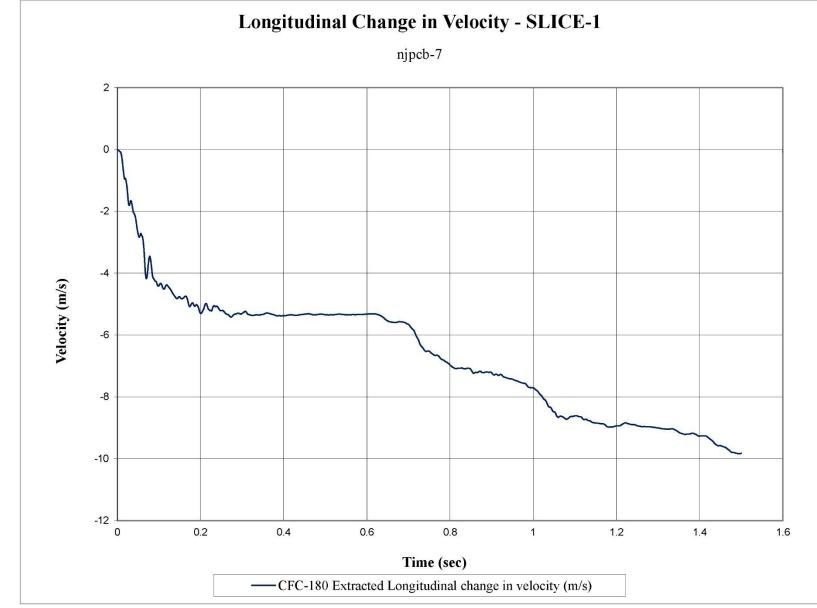


Figure F-10. Longitudinal Occupant Impact Velocity (SLICE-1), Test No. NJPCB-7

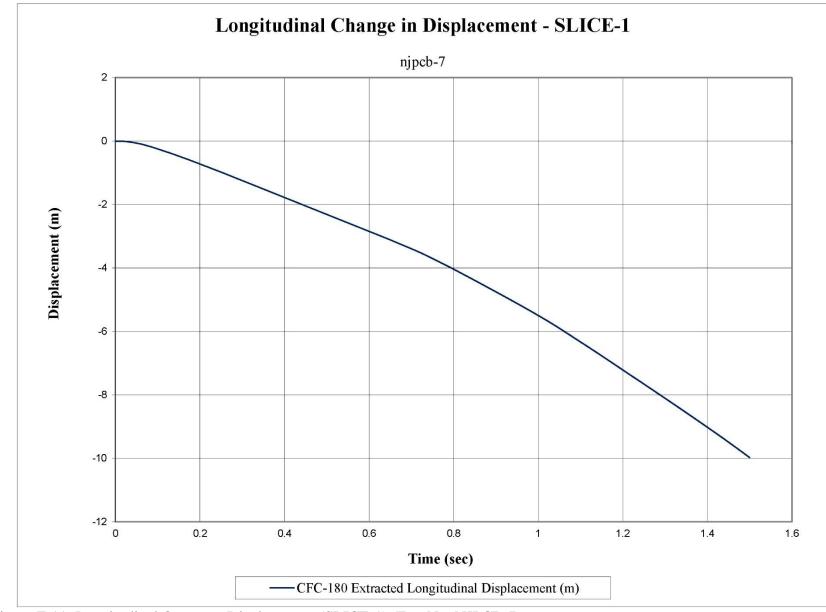


Figure F-11. Longitudinal Occupant Displacement (SLICE-1), Test No. NJPCB-7

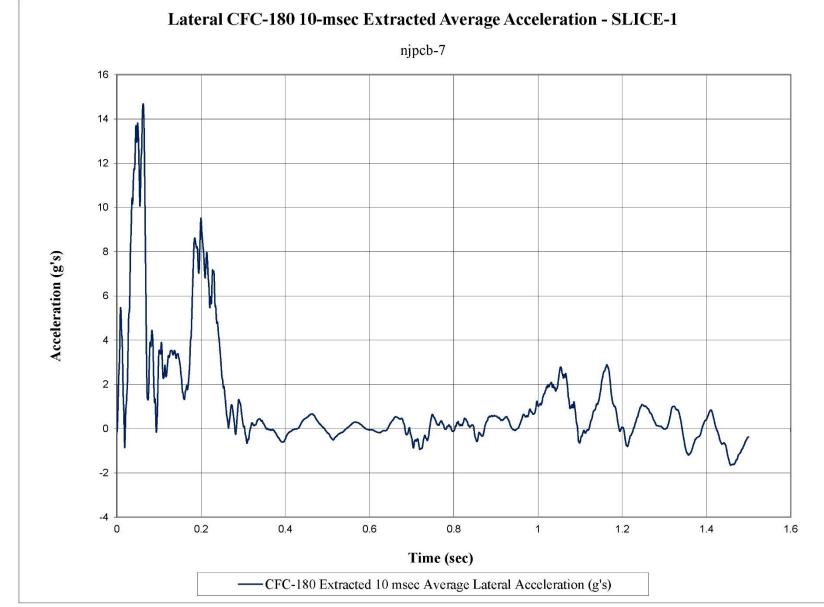


Figure F-12. 10-ms Average Lateral Deceleration (SLICE-1), Test No. NJPCB-7

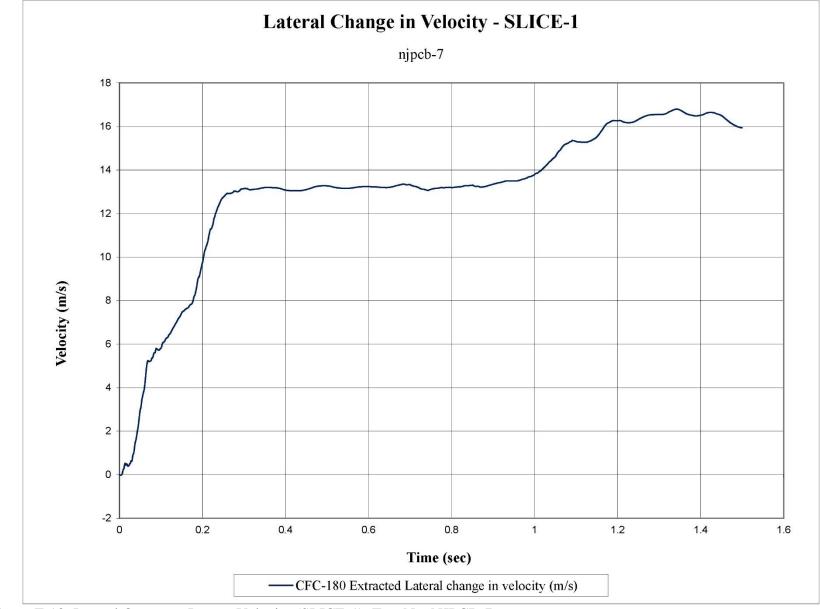


Figure F-13. Lateral Occupant Impact Velocity (SLICE-1), Test No. NJPCB-7



Figure F-14. Lateral Occupant Displacement (SLICE-1), Test No. NJPCB-7

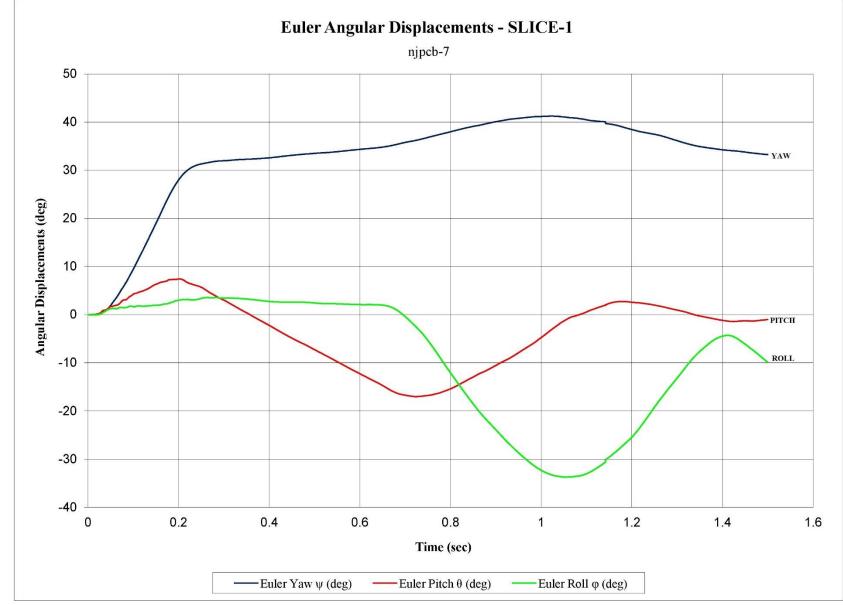


Figure F-15. Vehicle Angular Displacements (SLICE-1), Test No. NJPCB-7

122

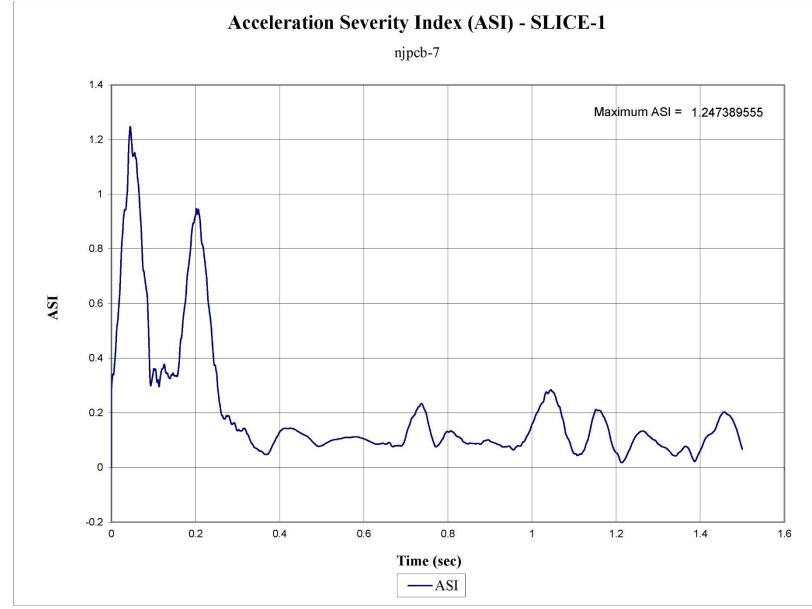


Figure F-16. Acceleration Severity Index (SLICE-1), Test No. NJPCB-7

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