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MASH TEST NOS. 3-11 AND 3-10 ON A NON-PROPRIETARY CABLE MEDIAN BARRIER

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16. Abstract <p>The Midwest States Pooled Fund has been developing a new non-proprietary cable median barrier. This system incorporates four evenly spaced cables, Midwest Weak Posts spaced at 8 to 16 ft (2.4 to 4.9 m) intervals, and a bolted, tabbed bracket to attach the cables to each post. Full-scale crash testing was needed to evaluate the barrier's safety performance. According to the <i>Manual for Assessing Safety Hardware</i> (MASH) updated/proposed testing matrix for cable barriers installed within a 6H:1V or median ditch, a series of eight full-scale tests are required to evaluate the safety performance of a system. A ninth test is required to establish the working width for systems with variable post spacing.</p> <p>Three full-scale crash tests were performed. Test no. MWP-4 was conducted according to MASH test no. 3-11 and utilized a 2270P pickup truck impacting the barrier on level terrain. The vehicle was contained by the barrier, and the test was deemed acceptable. Test no. MWP-6 was conducted according to MASH test no. 3-10 and utilized a 1100C passenger car impacting the barrier on level terrain. The vehicle was contained and redirected by the system. However, the system posts penetrated the occupant compartment through tearing and rupture of the vehicle floor board, and the test was deemed unacceptable. Test no. MWP-7 was also conducted with a 1100C vehicle according to MASH test no. 3-10. Alterations were made to the system posts. Although the vehicle was contained by the system, occupant compartment penetration by line posts was again observed. Test no. MWP-7 was deemed unacceptable.</p>			
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This report was completed with funding from the Federal Highway Administration, U.S. Department of Transportation. The contents of this report reflect the views and opinions of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the state highway departments participating in the Midwest States Pooled Fund Program nor the Federal Highway Administration, U.S. Department of Transportation. This report does not constitute a standard, specification, regulation, product endorsement, or an endorsement of manufacturers.

UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority (IAA) for the data contained herein was Dr. Cody Stolle, E.I.T.

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1 INTRODUCTION

1.1 Background

In recent years, the Midwest States Pooled Fund has been developing a non-proprietary, high-tension cable median barrier in conjunction with the Midwest Roadside Safety Facility (MwRSF) [1]. This cable barrier system was intended for use anywhere within a 6H:1V median V-ditch and consisted of four cables supported by Midwest Weak Posts (MWP) spaced at intervals ranging between 8 ft and 16 ft (2.4 m and 4.9 m). A bolted, tabbed bracket was utilized to attach the lower three cables to alternating sides of the MWPs, while a brass keeper rod was utilized to contain the top cable within a V-notch cut into the top of the posts.

Previously, this cable barrier system was subjected to three full-scale crash tests in accordance with the *Manual for Assessing Safety Hardware* (MASH) [2]. Test no. MWP-1, in accordance with MASH test designation no. 3-17, was conducted with a 1500A vehicle impacting the system placed on the slope break point of a 6H:1V median V-ditch. During the test, the sedan was successfully captured and redirected by cable no. 2, having overridden cable no. 1 and underridden cable nos. 3 and 4 [1].

For test no. MWP-2, the barrier was placed on level terrain, and the system cables were mirrored so that cable no. 2 was on the impact side of the posts and cable nos. 1 and 3 were on the non-impact side. A 16-ft (4.9-m) post spacing was utilized to evaluate the system's maximum deflection and working width. During the test, the front tires of the 2270P pickup overrode cable nos. 1 and 3. However, cable nos. 2 and 4 successfully captured and contained the vehicle.

For test no. MWP-3, the post spacing was changed to 8 ft (2.4 m) to evaluate system deflections and working width with the tighter post spacing. During the test, the 2270P pickup was initially captured by cable nos. 2 and 3 after overriding cable no. 1 and underriding cable no. 4. However, the capture cables were eventually pushed downward and overridden by the left-

front tire of the pickup. After containment of the vehicle was lost, the cables wrapped around the left-rear tire and yawed the pickup rapidly toward the barrier. The pickup ultimately rolled over as the right-side tires dug into the ground.

Following a review of test no. MWP-3, several factors may have contributed to the loss of vehicle capture. First, it was proposed that capture of the vehicle with additional cables were required for vehicle redirection. In order to evaluate the cable median barrier in a worst-case impact scenario, the researchers tested the barrier system in test nos. MWP-2 and MWP-3 with the primary capture cable for the 2270P vehicle, cable no. 3, or the third cable above the ground, on the non-impact side of the system, which limited its effectiveness in assisting in vehicle capture and redirection. This effect was shown in test no. MWP-2 when cable no. 3 was immediately knocked down as the vehicle bumper impacted the first post downstream from impact prior to cable engagement, which prevented the cable from interlocking with the vehicle.

In test no. MWP-3, the vehicle impacted the system slightly downstream from the target impact point, which allowed the vehicle to interlock with cable no. 3 prior to it being pushed down by a post. However, cable no. 3 eventually disengaged away from the vehicle, and vehicle capture was compromised. Thus, it was believed that cable no. 4, the top cable in the system, needs to contribute to interlock with the vehicle. In test no. MWP-2, cable no. 4 interlocked with the vehicle and aided in capture and redirection, but cable no. 4 overrode the vehicle in test no. MWP-3. Thus, it was believed that the height of cable no. 4 needed to be reduced to ensure vehicle interlock for level terrain test no. 3-11. Previous research at MwRSF regarding vehicle trajectories for 4:1 and 6:1 slopes [3] indicated that the top cable could be lowered to 38 in. (965 mm) and still be effective in capturing the 2270P vehicle at its maximum height above the slope in test designation no. 3-11. Thus, the top cable height was reduced from 40 in. (1016 mm) to 38 in. (965 mm) in order to improve vehicle capture.

Similarly, the cable spacing was reduced from 8¾ in. (222 mm) to 7½ in. (191 mm) in order to improve vehicle capture and interlock. More closely-spaced cables tend to improve the potential for multiple cables to interlock with the critical capture area of the vehicle and reduce the potential for penetration between the cables. A reduction of the cable spacing raised the height of the bottom cable to 15½ in. (394 mm). While the bottom cable height increased 2 in. (51 mm) over its original 13½ in. (343 mm) height, a review of simulated vehicle trajectories in 6:1 V-ditches indicated that the height of the bottom cable would still be sufficient for vehicle capture and preventing barrier underide.

Finally, the post spacing for the system was increased from 8 ft (2.4 m) to 10 ft (3.0 m). From a review of results from test no. MWP-3, it was believed that the reduced post spacing may have negatively affected cable motions after being interlocked with the vehicle, thus potentially contributing to the cables being pulled down and the loss of vehicle capture. Thus, it was decided to widen the post spacing slightly to 10 ft (3.0 m) in order to improve vehicle capture while continuing to manage barrier deflections.

After these modifications were made to improve system performance, full-scale crash testing was needed to evaluate the crashworthiness of the system. Therefore, the redesigned non-proprietary, four-cable, median barrier system required further testing according to the MASH Test Level 3 (TL-3) criteria [2].

1.2 Research Objectives

The primary objective of this project was to develop a high-tension, four-cable, median barrier that satisfies MASH TL-3 criteria when placed anywhere within a 6H:1V median V-ditch. Specific to this report, the cable system needed to be evaluated according to MASH test designation nos. 3-11 and 3-10.

1.3 Research Scope

The non-proprietary, four-cable, median barrier was subjected to three full-scale crash tests that are documented herein. The first test was a MASH test designation no. 3-11 test conducted with a 5,000-lb (2,268-kg) pickup truck impacting at a speed of 62 mph (100 km/h) and an angle of 25 degrees. The test was performed with a 10-ft (3.0-m) post spacing to establish the barrier's working width in a reduced post spacing configuration, as compared to the 16-ft (4.9-m) post spacing previously evaluated in test no. MWP-2. The second and third tests were MASH test designation no. 3-10 tests conducted with 2,425-lb (1,100-kg) passenger cars impacting at a speed of 62 mph (100 km/h) and an angle of 25 degrees. The tests were performed with 8-ft (2.4-m) post spacing. Minor alterations were made to posts in the impact region between the two small car tests to try to reduce the propensity for occupant compartment penetration. The results from all three tests were analyzed, evaluated, and documented. Conclusions and recommendations were then made pertaining to the safety performance of the cable barrier system.

2 TEST REQUIREMENTS AND EVALUATION CRITERIA

2.1 Test Requirements

Longitudinal barriers, such as cable median barriers, must satisfy impact safety standards in order to be declared eligible for federal reimbursement by the Federal Highway Administration (FHWA) for use on the National Highway System (NHS). For new hardware, these safety standards consist of the guidelines and procedures published in MASH [2]. According to the proposed MASH testing matrix for cable barriers placed anywhere within median V-ditches, the barrier system must be subjected to eight full-scale vehicle crash tests. However, for systems with variable post spacings, test designation no. 3-11 must be conducted with both the narrowest and widest post spacings to establish the working width bounds of the barrier system, increasing the required number of crash tests from eight to nine. Although the impact speed and angle are consistent for all nine tests, the critical location of the barrier system within the median ditch is dependent upon the specific crash test and the slope of the ditch. The MASH TL-3 testing matrix for a cable median barrier system designed for placement anywhere within a 6H:1V or flatter V-ditch is shown in Table 1. Note, MASH specifies that barrier systems designed for 6H:1V V-ditches are to be tested within a 30-ft (9.1-m) wide, 6H:1V V-ditch.

Many cable barrier systems have variable post spacings, which allow roadside designers to select the optimal configuration for a specific installation. When evaluating these variable post spacing systems, the critical post spacing should be utilized during crash testing. The proposed MASH update has identified the critical post spacing, either the narrowest or the widest spacing, for each individual test within the testing matrix. Proposed MASH test designation no. 3-11 must be conducted with both the narrowest and the widest post spacings to establish the working width bounds of the barrier system.

In accordance with MASH requirements, the critical impact point for the 2270P vehicle was 12 in. (305 mm) upstream of a post to maximize the risk that cables remain engaged with the post are pushed downward below the vehicle.. The critical impact point for the 1100C vehicle was determined to be located at the midspan between posts. This impact location was determined to maximize the potential for vehicle penetration by allowing the vehicle to penetrate between cables.

When non-symmetrical cable barriers are tested, it is important to test the orientation that produces the greatest risk of failure. To accomplish this critical evaluation, the orientation of the cables was selected such that primary capture cable would be located on the non-impact side of the post. The primary capture cable for the 2270P vehicle was determined to be the third cable above the ground. Selecting this orientation allowed for the greatest risk of failure due to the post pushing the backside cables down and preventing vehicle capture. This behavior would then potentially allow the vehicle to override the barrier. The primary capture cable for the 1100C vehicle was determined to be the second cable above the ground. Selecting this orientation allowed for the greatest risk of failure delaying vehicle interlock with the barrier and increasing the potential for the vehicle to penetrate through the system.

Table 1. MASH TL-3 Test Matrix for Barrier Placement Anywhere Within a 6V:1H V-Ditch

Test No.	Test Vehicle	Vehicle Weight, lb (kg)	Impact Conditions		System Configuration		Evaluation Criteria ²
			Speed, mph (km/h)	Angle, deg	System Location ¹	Post Spacing	
3-10	1100C	2,425 (1,100)	62 (100)	25	Level Terrain	Narrow	A,D,F,H,I
3-11	2270P	5,000 (2,270)	62 (100)	25	Level Terrain	Both	A,D,F,H,I
3-13	2270P	5,000 (2,270)	62 (100)	25	9 ft Down Front Slope	Narrow	A,D,F,H,I
3-14	1100C	2,425 (1,100)	62 (100)	25	9 ft Down Front Slope	Narrow	A,D,F,H,I
3-15	1100C	2,425 (1,100)	62 (100)	25	4 ft Up Back Slope	Wide	A,D,F,H,I
3-16	1100C	2,425 (1,100)	62 (100)	25	1 ft Down Back Slope	Narrow	A,D,F,H,I
3-17	1500A	3,300 (1,500)	62 (100)	25	See Note ³	Wide	A,D,F,H,I
3-18	2270P	5,000 (2,270)	62 (100)	25	At Back Slope Break Point	Wide	A,D,F,H,I

¹ Test nos. 3-13 through 3-18 shall be conducted within a 30 ft (9.1 m) wide, 6H:1V V-ditch

² Evaluation criteria explained in Table 2.

³ Testing laboratory to determine critical barrier position on front slope of ditch to maximize propensity for front end of 1500A vehicle to penetrate between vertically adjacent cables.

2.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the cable median barrier to contain and redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are

summarized in Table 2 and defined in greater detail in MASH. The full-scale vehicle crash tests were conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported on the test summary sheet. Additional discussion on PHD, THIV and ASI is provided in MASH.

Table 2. MASH Evaluation Criteria for Longitudinal Barrier

Structural Adequacy	A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.		
Occupant Risk	D. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.		
	F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.		
	H. Occupant Impact Velocity (OIV) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:		
	Occupant Impact Velocity Limits		
	Component	Preferred	Maximum
	Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)
I. The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:	Occupant Ridedown Acceleration Limits		
Component	Preferred	Maximum	
Longitudinal and Lateral	15.0 g's	20.49 g's	

2.3 Soil Strength Requirements

In accordance with Chapter 3 and Appendix B of MASH, foundation soil strength must be verified before any full-scale crash testing can occur. During the installation of a soil dependent system, additional W6x16 in. (W152x23.8 mm) posts are to be installed near the impact region utilizing the same installation procedures as the system itself. Prior to full-scale testing, a dynamic impact test must be conducted to verify a minimum dynamic soil resistance of 7.5 kips (33.4 kN) at post deflections between 5 and 20 in. (127 and 508 mm) measured at a height of 25 in. (635 mm). If dynamic testing near the system is not desired, MASH permits a static test to be conducted instead and compared against the results of a previously established baseline test. In this situation, the soil must provide a resistance of at least 90% of the static baseline test at deflections of 5, 10, and 15 in. (127, 254, and 381 mm). Further details can be found in Appendix B of MASH.

3 TEST CONDITIONS

3.1 Test Facility

The testing facility is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport, and is approximately 5 miles (8.0 km) northwest of the city campus of the University of Nebraska-Lincoln.

3.2 Vehicle Tow and Guide System

A reverse cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released away from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [4] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The $\frac{3}{8}$ -in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.5 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

3.3 Test Vehicles

For test no. MWP-4, a 2008 Dodge Ram was used as the test vehicle. This vehicle meets the requirements for a MASH 2270P pickup truck. The curb, test inertial and gross static vehicle weights were 5,140 lb (2,331 kg), 4,967 lb (2,253 kg), and 5,131 lb (2,327 kg), respectively. The test vehicle is shown in Figure 1, and vehicle dimensions are shown in Figure 2.

For test no. MWP-6, a 2009 Kia Rio was used as the test vehicle. This vehicle meets the requirements for a MASH 1100C passenger car. The curb, test inertial and gross static vehicle weights were 2,295 lb (1,041 kg), 2,405 lb (1,091), and 2,572 lb (1,167 kg), respectively. The test vehicle is shown in Figure 3, and the vehicle dimensions are shown in Figure 4.

For test no. MWP-7, a 2009 Kia Rio was used as the test vehicle. This vehicle meets the requirements for a MASH 1100C passenger car. The curb, test inertial and gross static vehicle weights were 2,384 lb (1,081 kg), 2,392 lb (1,085), and 2,557 lb (1,160 kg), respectively. The test vehicle is shown in Figure 5, and the vehicle dimensions are shown in Figure 6.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The vertical component of the c.g. for the 1100C vehicles was determined utilizing a procedure published by SAE [5]. The Suspension Method [6] was used to determine the vertical component of the c.g. for the 2270P vehicle. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The locations of the c.g. for test nos. MWP-4, MWP-6, and MWP-7 are shown in Figures 2, 4, and 6, respectively. Data used to calculate the location of the c.g. and ballast information are shown in Appendix B.

Square, black-and white-checked targets were placed on the vehicles for reference to be viewed from the high-speed digital video cameras and aid in video analysis, as shown in Figures 7 through 9. Round, checkered targets were placed on the center of gravity on the left-side door, the right-side door, and the roof of the vehicles.

The front wheels of the test vehicles were aligned to vehicle standards except the toe-in values were adjusted to zero so that the vehicles would track properly along the guide cable. A

5B flash bulb was mounted on the left side of the vehicles' dash and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed videos. A remote-controlled brake system was installed in the test vehicles so that the vehicles could be brought safely to a stop after the vehicle exited the system.



Figure 1. Test Vehicle, Test No. MWP-4

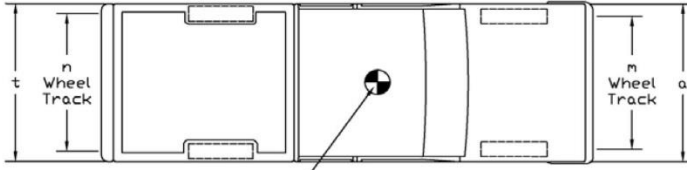
Date: <u>10/20/2014</u>		Test Number: <u>MWP-4</u>		Model: <u>Ram 1500 QC</u>																				
Make: <u>Dodge</u>		Vehicle I.D.#: <u>1D7HA18N18S590981</u>																						
Tire Size: <u>265/70 R17</u>		Year: <u>2008</u>		Odometer: <u>108323</u>																				
Tire Inflation Pressure: <u>35 psi.</u>																								
*(All Measurements Refer to Impacting Side)																								
			Vehicle Geometry -- in. (mm)																					
a	<u>78</u>	(1981)	b	<u>74 1/2</u>	(1892)																			
c	<u>227 3/8</u>	(5775)	d	<u>49</u>	(1245)																			
e	<u>140 1/2</u>	(3569)	f	<u>37 7/8</u>	(962)																			
g	<u>28</u>	(711)	h	<u>60 3/5</u>	(1539)																			
i	<u>10 1/4</u>	(260)	j	<u>26</u>	(660)																			
k	<u>21 1/2</u>	(546)	l	<u>30 1/4</u>	(768)																			
m	<u>67 1/2</u>	(1715)	n	<u>67 3/4</u>	(1721)																			
o	<u>50 1/2</u>	(1283)	p	<u>3 1/2</u>	(89)																			
q	<u>31 3/4</u>	(806)	r	<u>18 1/2</u>	(470)																			
s	<u>15 1/4</u>	(387)	t	<u>77</u>	(1956)																			
Wheel Center Height Front			<u>14 1/2</u> (368)																					
Wheel Center Height Rear			<u>14 7/8</u> (378)																					
Wheel Well Clearance (F)			<u>5</u> (127)																					
Wheel Well Clearance (R)			<u>8 1/2</u> (216)																					
Frame Height (F)			<u>17 3/4</u> (451)																					
Frame Height (R)			<u>26 1/4</u> (667)																					
Engine Type			<u>8cyl. Gas</u>																					
Engine Size			<u>4.7L</u>																					
Transmission Type:			<input type="radio"/> Automatic <input checked="" type="radio"/> Manual																					
			<input type="radio"/> FWD <input checked="" type="radio"/> RWD <input type="radio"/> 4WD																					
<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="4">Mass Distribution lb (kg)</th> </tr> <tr> <th></th> <th>LF</th> <th>RF</th> <th>LR</th> <th>RR</th> </tr> </thead> <tbody> <tr> <td>Gross Static</td> <td><u>1514</u> (687)</td> <td><u>1407</u> (638)</td> <td></td> <td></td> </tr> <tr> <td></td> <td><u>1079</u> (489)</td> <td><u>1131</u> (513)</td> <td></td> <td></td> </tr> </tbody> </table>						Mass Distribution lb (kg)					LF	RF	LR	RR	Gross Static	<u>1514</u> (687)	<u>1407</u> (638)				<u>1079</u> (489)	<u>1131</u> (513)		
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Rear	<u>3900</u>	Mass:	<u>164 lb</u>																					
Total	<u>6700</u>	Seat Position:	<u>Front Driver Seat</u>																					
Note any damage prior to test: <u>None</u>																								

Figure 2. Vehicle Dimensions, Test No. MWP-4



Figure 3. Test Vehicle, Test No. MWP-6

Date: <u>1/16/2015</u>	Test Number: <u>MWP-6</u>	Model: <u>Rio</u>
Make: <u>Kia</u>	Vehicle I.D.#: <u>knade223096452429</u>	
Tire Size: <u>186/65R14</u>	Year: <u>2009</u>	Odometer: <u>47322</u>
Tire Inflation Pressure: <u>32 psi</u>		

*(All Measurements Refer to Impacting Side)

Vehicle Geometry -- in. (mm)

a	<u>61 1/4 (1556)</u>	b	<u>57 3/4 (1467)</u>
c	<u>167 (4242)</u>	d	<u>36 (914)</u>
e	<u>98 1/2 (2502)</u>	f	<u>32 1/2 (826)</u>
g	<u>22 (559)</u>	h	<u>39 (989)</u>
i	<u>16 (406)</u>	j	<u>22 (559)</u>
k	<u>15 (381)</u>	l	<u>23 1/4 (591)</u>
m	<u>57 1/2 (1461)</u>	n	<u>56 1/2 (1435)</u>
o	<u>32 1/4 (819)</u>	p	<u>2 (51)</u>
q	<u>23 1/4 (591)</u>	r	<u>15 1/4 (387)</u>
s	<u>11 3/4 (298)</u>	t	<u>63 (1600)</u>

Wheel Center Height Front	<u>10 3/4 (273)</u>
Wheel Center Height Rear	<u>11 (279)</u>
Wheel Well Clearance (F)	<u>25 3/4 (654)</u>
Wheel Well Clearance (R)	<u>24 3/4 (629)</u>
Frame Height (F)	<u>8 1/2 (216)</u>
Frame Height (R)	<u>15 1/2 (394)</u>
Engine Type	<u>Gasoline</u>
Engine Size	<u>1.6L 4 Cyl</u>
Transmission Type:	<u>Automatic</u> <u>Manual</u>
	<u>FWD</u> <u>RWD</u> <u>4WD</u>

Mass Distribution lb (kg)			
Gross Static	LF <u>794 (360)</u>	RF <u>744 (337)</u>	
	LR <u>528 (239)</u>	RR <u>506 (230)</u>	

Weights lb (kg)	Curb	Test Inertial	Gross Static
W-front	<u>1469 (666)</u>	<u>1454 (660)</u>	<u>1538 (698)</u>
W-rear	<u>826 (375)</u>	<u>951 (431)</u>	<u>1034 (469)</u>
W-total	<u>2295 (1041)</u>	<u>2405 (1091)</u>	<u>2572 (1167)</u>

GVWR Ratings	Dummy Data
Front <u>1918</u>	Type: <u>Hybrid 1</u>
Rear <u>1874</u>	Mass: <u>167 lbs</u>
Total <u>3638</u>	Seat Position: <u>Driver</u>

Note any damage prior to test: Multiple Hail dents on multiple body panels, passenger side door trim missing.

Figure 4. Vehicle Dimensions, Test No. MWP-6



Figure 5. Test Vehicle, Test No. MWP-7

Date: 2/24/2015 Test Number: MWP-7 Model: Rio
Make: Kia Vehicle I.D.#: knade223596549481
Tire Size: 185/65/R14 Year: 2009 Odometer: 107161
Tire Inflation Pressure: 32 psi
*(All Measurements Refer to Impacting Side)

Vehicle Geometry -- in. (mm)

a	<u>62</u>	(1575)	b	<u>57 3/4</u>	(1467)
c	<u>166 3/4</u>	(4235)	d	<u>35 1/2</u>	(902)
e	<u>98 1/8</u>	(2492)	f	<u>33 1/8</u>	(841)
g	<u>23 1/9</u>	(587)	h	<u>37 1/2</u>	(952)
i	<u>15</u>	(381)	j	<u>21</u>	(533)
k	<u>15</u>	(381)	l	<u>23 1/2</u>	(597)
m	<u>57</u>	(1448)	n	<u>57</u>	(1448)
o	<u>27 3/4</u>	(705)	p	<u>4</u>	(102)
q	<u>23 1/4</u>	(591)	r	<u>15 1/4</u>	(387)
s	<u>11 1/4</u>	(286)	t	<u>61 1/2</u>	(1562)

Wheel Center Height Front 10 3/4 (273)
Wheel Center Height Rear 11 (279)
Wheel Well Clearance (F) 25 (635)
Wheel Well Clearance (R) 24 3/4 (629)
Frame Height (F) 6 (152)
Frame Height (R) 15 3/4 (400)
Engine Type Gasoline
Engine Size 4 Cyl 1.6L
Transmission Type: Automatic Manual
FWD RWD 4WD

Mass Distribution lb (kg)

Gross Static	LF	<u>794</u>	(360)	RF	<u>772</u>	(350)
	LR	<u>512</u>	(232)	RR	<u>479</u>	(217)

Weights lb (kg)

	Curb	Test Inertial	Gross Static
W-front	<u>1514</u>	<u>1478</u>	<u>1566</u>
W-rear	<u>870</u>	<u>914</u>	<u>991</u>
W-total	<u>2384</u>	<u>2392</u>	<u>2557</u>

GVWR Ratings

Front	<u>1918 lbs</u>
Rear	<u>1875 lbs</u>
Total	<u>3638 lbs</u>

Dummy Data

Type: Hybrid 1
Mass: 165 lbs.
Seat Position: Driver

Note any damage prior to test: 3 inch dent on leading edge of hood

Figure 6. Vehicle Dimensions, Test No. MWP-7

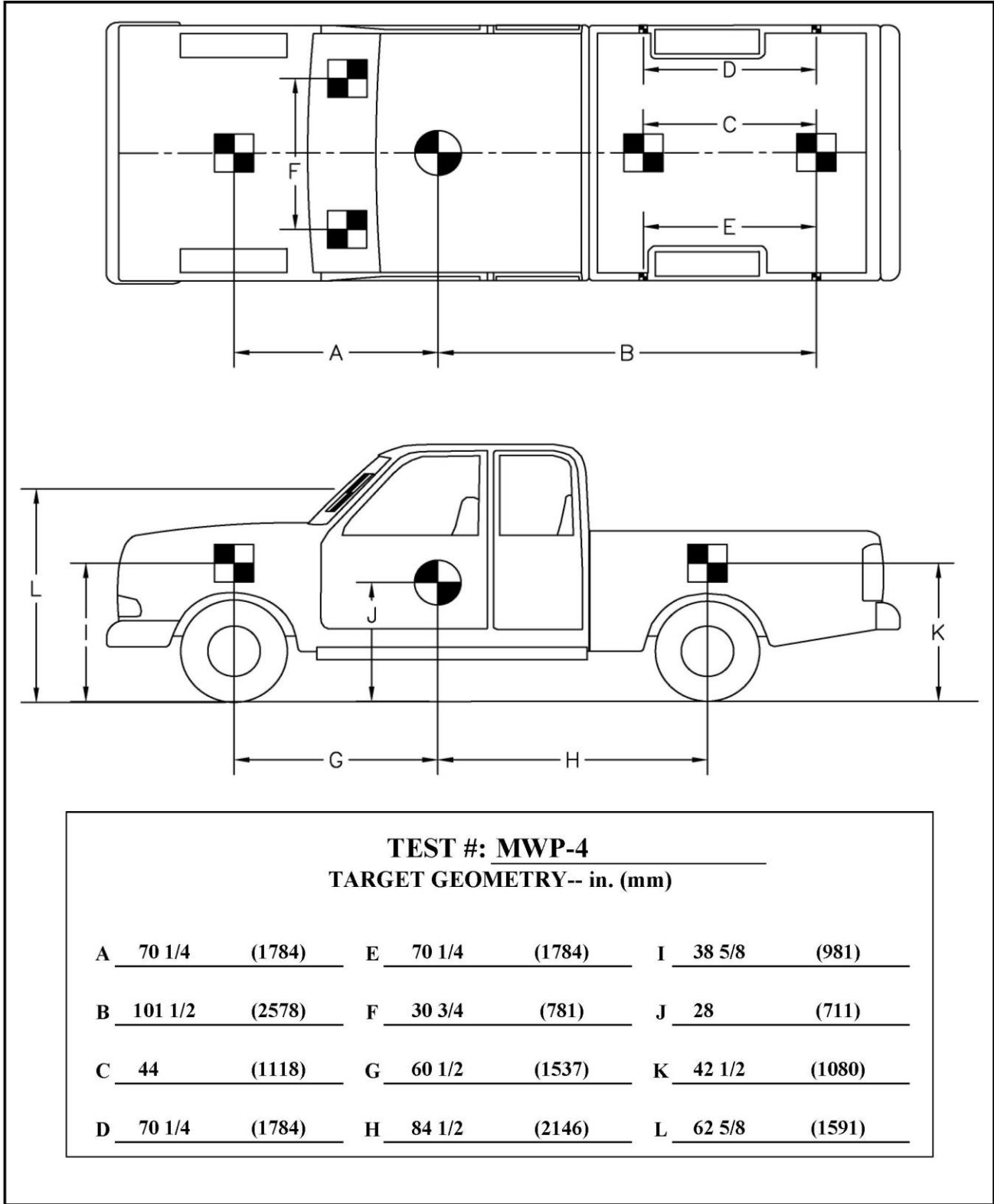


Figure 7. Target Geometry, Test No. MWP-4

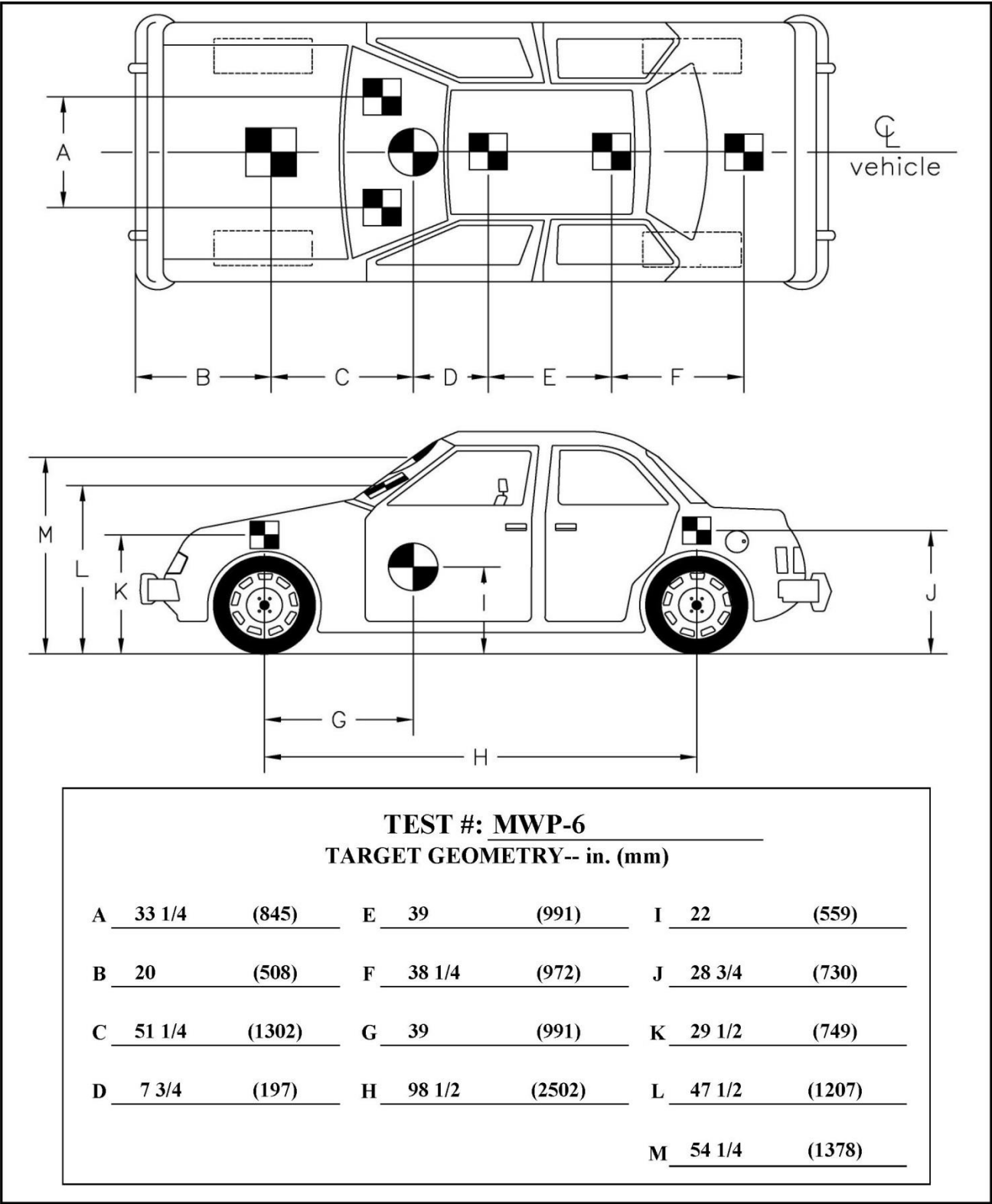


Figure 8. Target Geometry, Test No. MWP-6

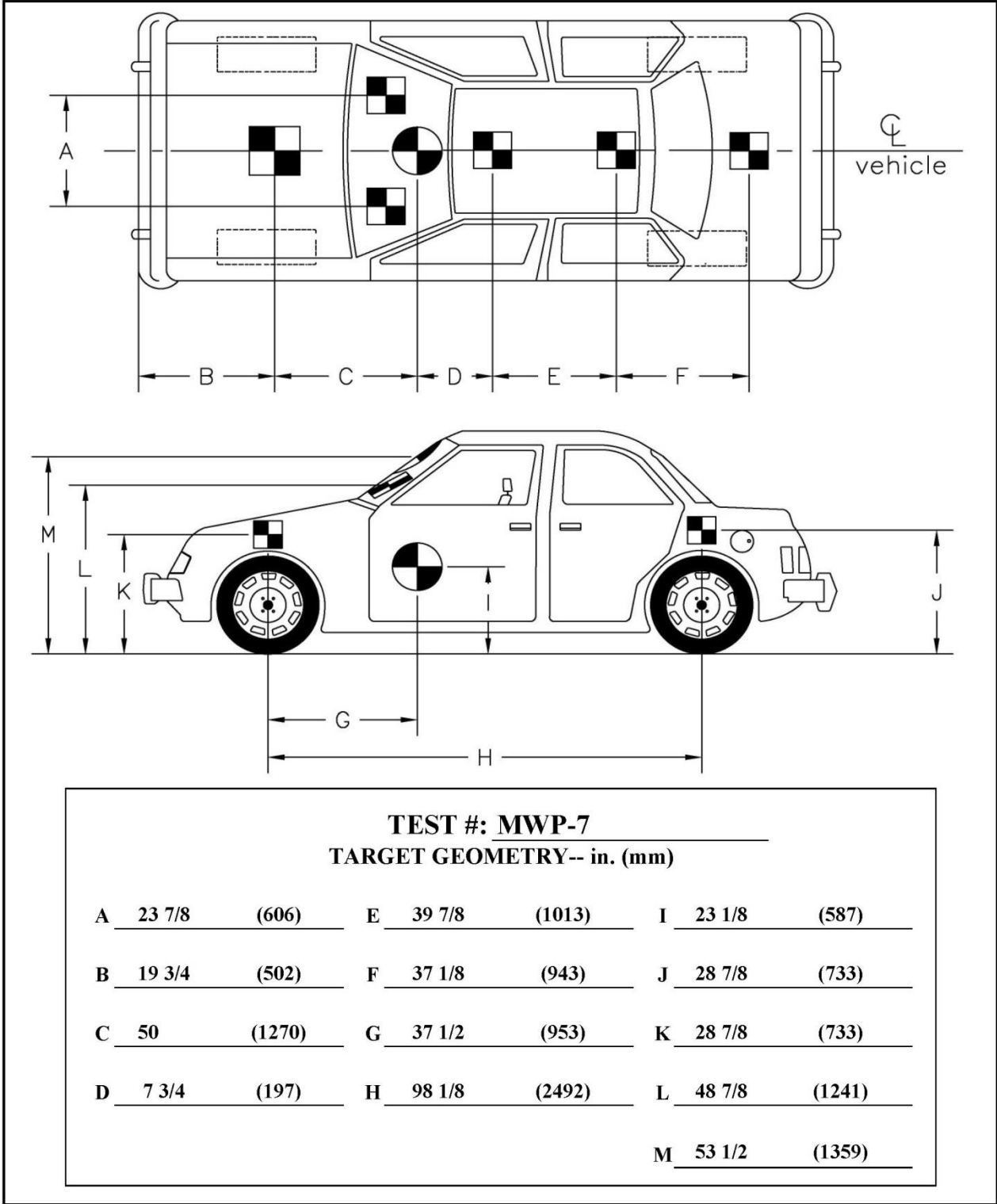


Figure 9. Target Geometry, Test No. MWP-7

3.4 Simulated Occupant

A Hybrid II 50th-Percentile, Adult Male Dummy, equipped with clothing and footwear, was placed in the left-front seat of all three test vehicles with the seat belt was fastened. The dummy, which had a final weight of 170 lb (77 kg), was model no. 572, serial no. 451, and was manufactured by Android Systems of Carson, California. As recommended by MASH, the dummy was not included in calculating the c.g location.

3.5 Data Acquisition Systems

3.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. Both accelerometers were mounted near the center of gravity of each test vehicle. The electronic accelerometer data obtained during dynamic testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filters conforming to the SAE J211/1 specifications [7].

The two accelerometer systems, the SLICE-1 and SLICE-2 units, were modular data acquisition systems manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. The acceleration sensors were mounted inside the bodies of the custom built SLICE 6DX event data recorders and recorded data at 10,000 Hz to the onboard microprocessor. Each SLICE 6DX was configured with 7 GB of non-volatile flash memory, a range of ± 500 g's, a sample rate of 10,000 Hz, and a 1,650 Hz (CFC 1000) anti-aliasing filter. The "SLICEWare" computer software programs and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

3.5.2 Rate Transducers

Two angle rate sensor systems were utilized to measure the rates of rotation of the vehicles during testing. Both were SLICE MICRO Triax ARS units, with a range of 1,500

degrees/sec in each of the three directions (roll, pitch, and yaw). The angular rate sensors were mounted inside the bodies of the two custom built SLICE 6DX event data recorders and recorded data at 10,000 Hz to the onboard microprocessor. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The SLICEWare computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

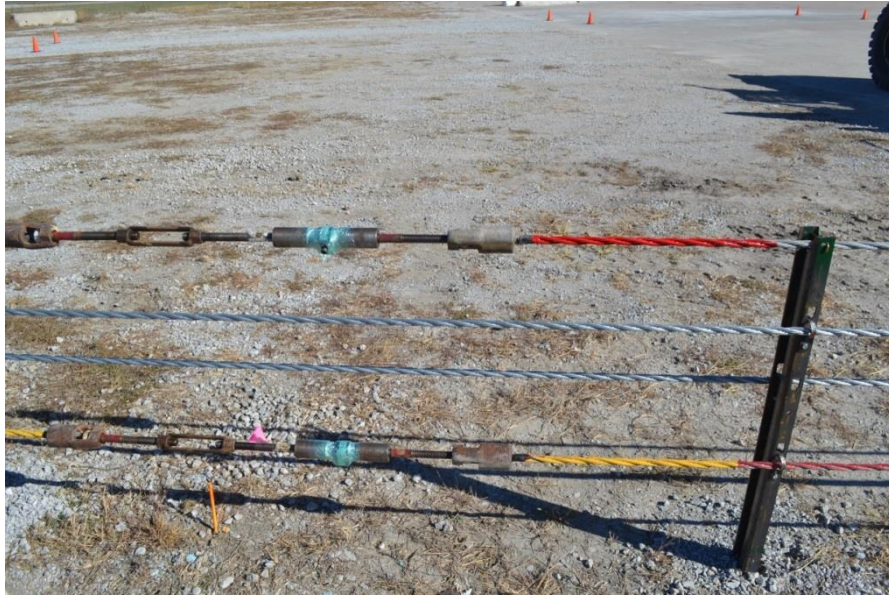
3.5.3 Retroreflective Optic Speed Trap

The retroreflective optical speed trap was used to determine the speed of the vehicle before impact. Five retroreflective targets, spaced at approximately 18-in. (457-mm) intervals, were applied to the sides of the vehicles. When the emitted beam of light was reflected by the targets and returned to the Emitter/Receiver, a signal was sent to the data acquisition computer, which recorded at 10,000 Hz, as well as activated the External LED box. The speed was then calculated using the spacing between the retroreflective targets and the time interval between the signals. LED lights and high-speed digital video analysis are only used as a backup in the event that vehicle speeds cannot be determined from the electronic data.

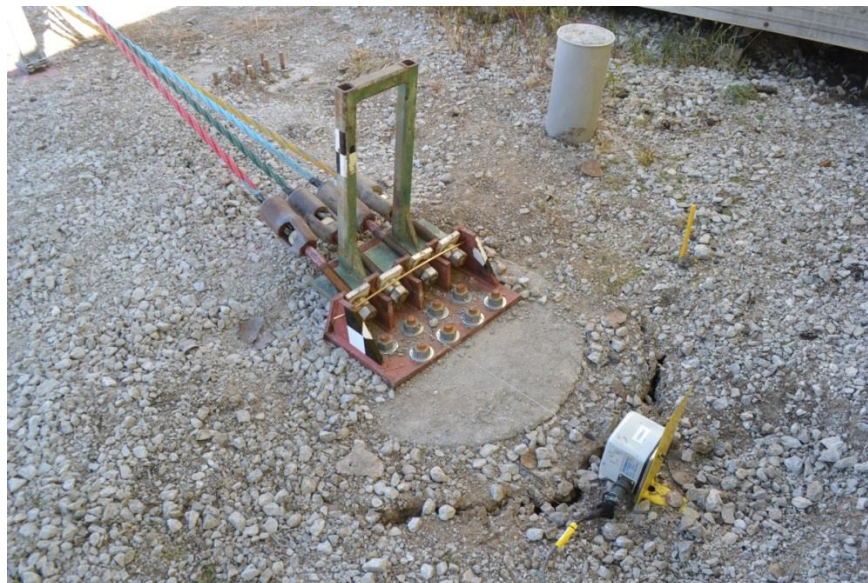
3.5.4 Load Cells and String Potentiometers

Load cells were spliced into each cable upstream from impact. The cables in each test were numbered 1 through 4 starting at the bottom cable. For test no. MWP-4 the load cells on cable nos. 2 and 4 were located between post nos. 5 and 6, and the load cells on cable nos. 1 and 3 were located between post nos. 6 and 7. For test nos. MWP-6 and MWP-7, the load cells on cable nos. 2 and 4 were located between post nos. 6 and 7, and the load cells on cable nos. 1 and 3 were located between post nos. 7 and 8. All four load cells were Transducer Techniques model no. TLL-50K with a load range up to 50 kips (222 kN). A string potentiometer was also attached to the upstream anchor foundation, labeled as post no. 1, for all three tests. The string

potentiometer was a Unimeasure model no. PA-50-70124 with a displacement range up to 50 in. (127 cm). During testing, output voltage signals were sent from the five transducers to a National Instruments PCI-6071E data acquisition board, acquired with LabView software, and stored on a personal computer at a sample rate of 10,000 Hz. The positioning and set up of the transducers are shown in Figure 10.



Load Cells, Test No. MWP-4



String Potentiometer Test Nos. MWP-4 through MWP-6

Figure 10. Location of Load Cells and String Potentiometer

3.5.5 Digital Photography

Two AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, one AOS S- VIT 1531 high-speed digital video camera, three JVC digital video cameras, four GoPro Hero 3+ digital video cameras and two GoPro Hero 3 digital video cameras were utilized to film test no. MWP-4. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 11.

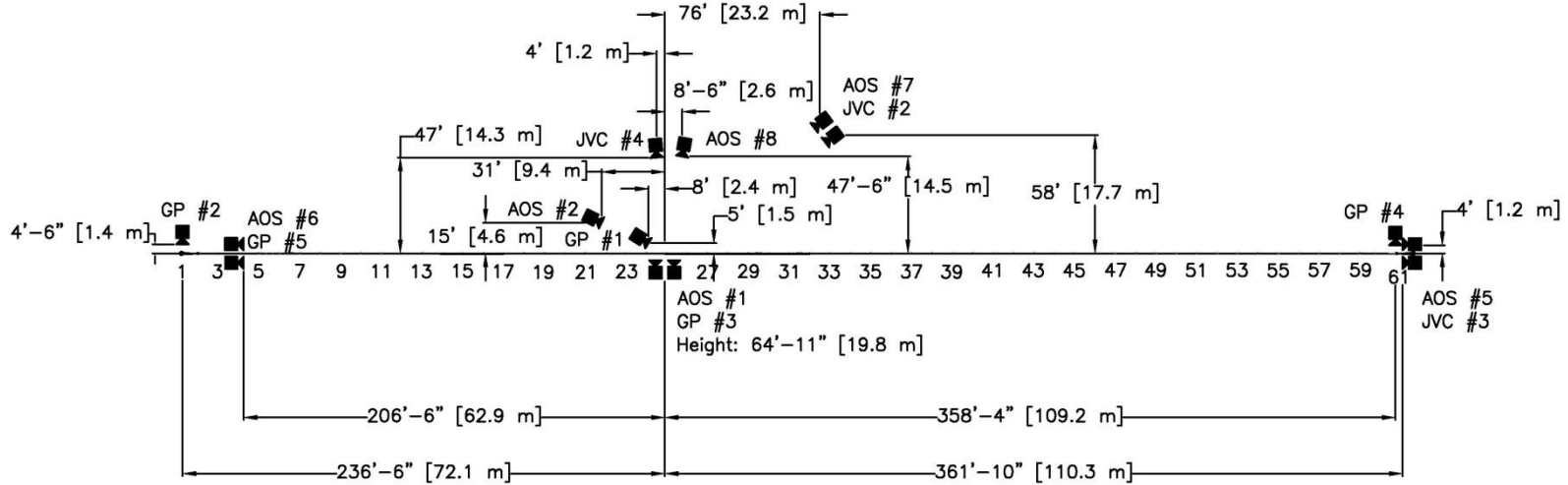
One AOS VITcam high-speed digital video camera, one AOS S-VIT 1531 high-speed digital video camera, one AOS TRI-VIT 2236 high speed digital camera, two AOS X-PRI high-speed digital video cameras, three JVC digital video cameras, four GoPro Hero 3+ digital video cameras, and two GoPro Hero 3 digital video cameras were utilized to film test no. MWP-6. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 12.

Two AOS Vitcam high-speed digital video cameras, one AOS S-VIT 1531 high-speed digital video camera, two AOS X-PRI high-speed digital video cameras, one AOS TRI-VIT 2236 high speed digital video camera, three JVC digital video cameras, four GoPro Hero 3+ digital video cameras, one GoPro Hero 4 digital video camera, and two GoPro Hero 3 digital video cameras were utilized to film test no. MWP-7. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 13.

In each of the three tests, one of the GoPro cameras was mounted inside the test vehicle, and therefore does not appear on the camera placement schematic.

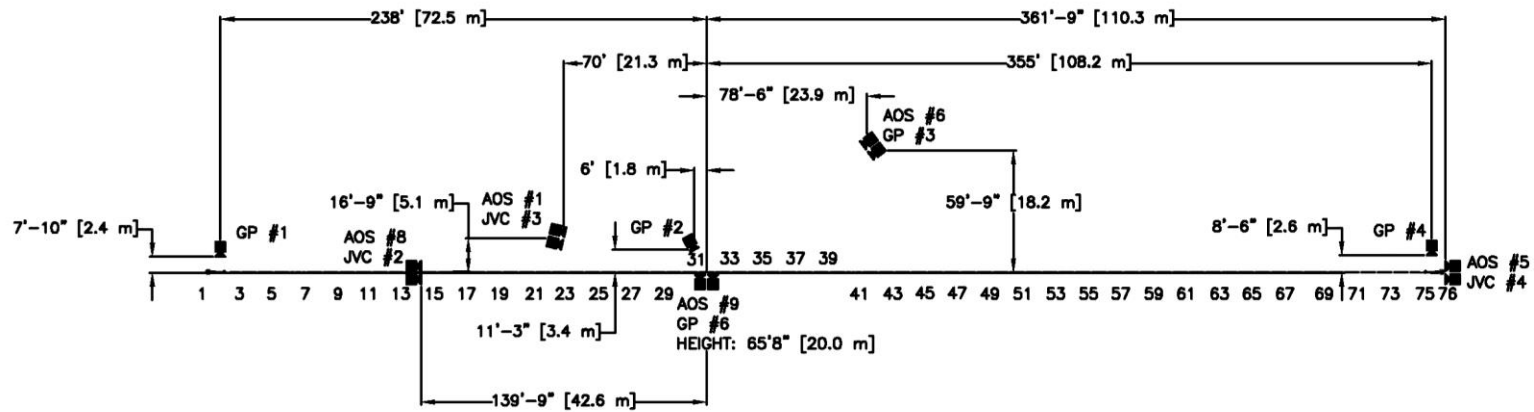
The high-speed videos were analyzed using ImageExpress MotionPlus and RedLake MotionScope software programs. Actual camera speed and camera divergence factors were

considered in the analysis of the high-speed videos. A Nikon D50 digital still camera was also used, to document pre- and post-test conditions for all tests.



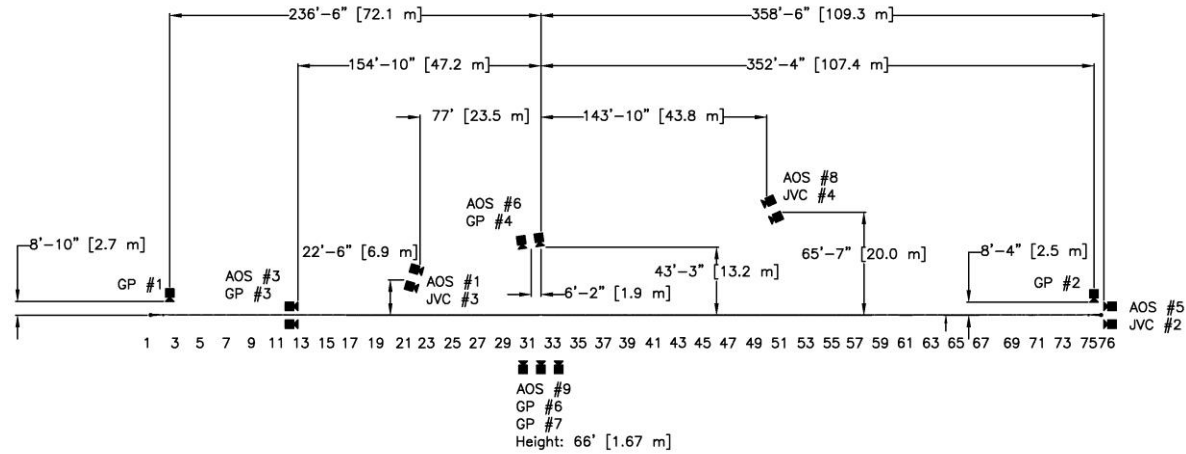
Camera No.	Type	Operating Speed (frames/sec)	Lens	Lens Setting
AOS-1	AOS Vitcam	500	Cosmicar 12.5mm fixed	12.5mm
AOS-2	AOS Vitcam	500	Sigma 28-70	28mm
AOS-5	AOS X-PRI	500	TV Zoom 17-102	102mm
AOS-6	AOS X-PRI	500	Fujinon 50mm fixed	50mm
AOS-7	AOS X-PRI	500	Nikon 28mm fixed	28mm
AOS-8	AOS S-VIT 1531	500	Nikon 28mm fixed	28mm
GP-1	GoPro Hero 3	120		
GP-2	GoPro Hero 3	120		
GP-3	GoPro Hero 3+	120		
GP-4	GoPro Hero 3+	120		
GP-5	GoPro Hero 3+	120		
GP-6	GoPro Hero 3+	120		
JVC-2	JVC – GZ-MG27u (Everio)	29.97		
JVC-3	JVC – GZ-MG27u (Everio)	29.97		
JVC-4	JVC – GZ-MG27u (Everio)	29.97		

Figure 11. Camera Locations, Speeds, and Lens Settings, Test No. MWP-4



Camera No.	Type	Operating Speed (frames/sec)	Lens	Lens Setting
AOS-1	AOS Vitcam	500	Sigma 24-70	35mm
AOS-5	AOS X-PRI	500	TV Zoom 17-102	102mm
AOS-6	AOS X-PRI	500	Nikon 28mm fixed	28mm
AOS-8	AOS S-VIT 1531	500	Sigma 24-135	85mm
AOS-9	AOS TRI-VIT 2236	500	Cosmicar 12.5mm fixed	12.5mm
GP-1	GoPro Hero 3	120		
GP-2	GoPro Hero 3	120		
GP-3	GoPro Hero 3+	120		
GP-4	GoPro Hero 3+	120		
GP-5	GoPro Hero 3+	120		
GP-6	GoPro Hero 3+	120		
JVC-2	JVC – GZ-MG27u (Everio)	29.97		
JVC-3	JVC – GZ-MG27u (Everio)	29.97		
JVC-4	JVC – GZ-MG27u (Everio)	29.97		

Figure 12. Camera Locations, Speeds, and Lens Settings, Test No. MWP-6



Camera No.	Type	Operating Speed (frames/sec)	Lens	Lens Setting
AOS-1	AOS Vitcam	500	Sigma 28-70	50mm
AOS-3	AOS Vitcam	500	Fujinon 50mm fixed	50mm
AOS-5	AOS X-PRI	500	Vivitar 135mm fixed	135mm
AOS-6	AOS X-PRI	500	Nikon Nikkor 20 mm fixed	20mm
AOS-8	AOS S-VIT 1531	500	Sigma 28-70	28mm
AOS-9	AOS TRI-VIT 2236	500	Kowa 12.5mm	12.5mm
GP-1	GoPro Hero 3	120		
GP-2	GoPro Hero 3	120		
GP-3	GoPro Hero 3+	120		
GP-4	GoPro Hero 3+	120		
GP-5	GoPro Hero 3+	120		
GP-6	GoPro Hero 3+	120		
GP-7	GoPro Hero 4	240		
JVC-2	JVC – GZ-MG27u (Everio)	29.97		
JVC-3	JVC – GZ-MG27u (Everio)	29.97		
JVC-4	JVC – GZ-MG27u (Everio)	29.97		

Figure 13. Camera Locations, Speeds, and Lens Settings, Test No. MWP-7

4 DESIGN DETAILS TEST NO. MWP-4

The non-proprietary, 4-cable median barrier system evaluated in test no. MWP-4 is shown in Figures 14 through 37. The test installation was constructed with a total length of 604 ft (184.1 m) on level terrain. The cable barrier system was comprised of several distinct components: (1) high-tension cables or wire ropes; (2) cable splices; (3) steel support posts; (4) cable-to-post attachment brackets; (5) breakaway end terminals; and (6) reinforced concrete foundations. Photographs of the test installation are shown in Figures 38 through 41. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix A.

Four $\frac{3}{4}$ -in. (19-mm) diameter, Class A galvanized 3x7 (pre-stretched) wire ropes were utilized for the longitudinal cables. The barrier utilized a consistent $7\frac{1}{2}$ -in. (190.5-mm) cable spacing as the cables were placed at heights of $15\frac{1}{2}$ in. (393.7 mm), 23 in. (584.2 mm), $30\frac{1}{2}$ in. (774.7 mm), and 38 in. (965.2 mm) above the ground surface. The cables were numbered 1 through 4, starting with the bottom cable and proceeding upward to the top cable.

Cable nos. 1 and 3 were attached to the non-impact side of each post, while cable no. 2 was attached to the impact side of each post, as shown in Figure 28. Cable no. 4 resided within the V-notch cut into the top of each post. MASH requires that cable barrier systems be tested with cable tensions set to the recommended tension at 100 degrees Fahrenheit. A cable tensioning chart was developed as a function of ambient air temperature for use when installing the barrier system, as shown in Table 3. Thus, the cables were tensioned to a pre-load of 2,500 lb (11.1 kN).

Each of the four wire ropes contained a splice in the impact region, between post nos. 29 and 33, as shown in Figure 15. Additionally, a load cell was spliced into each wire rope upstream

from impact, between post nos. 5 and 7, as shown in Figure 18. Details for the load cells, threaded rods, turnbuckles, end fittings, and rod couplers are provided in Figure 19.

Table 3. Pre-Stretched Cable Tension Chart

Ambient Air Temperature (Degrees Fahrenheit)	Cable Tension (lb)
110	2,240
100	2,500
90	2,760
80	3,021
70	3,281
60	3,541
50	3,801
40	4,062
30	4,322
20	4,582
10	4,842
0	5,102
-10	5,363
-20	5,623
-30	5,883
-40	6,143

The cables were supported by 58 line posts and anchored at the upstream and downstream ends with selected hardware from a prototype breakaway cable end terminal system. Post nos. 3 through 60 were Midwest Weak Posts (MWP) measuring 83 in. (2,108 mm) in length. The MWPs were fabricated from bent 7-gauge (4.6-mm) sheet steel to a 3-in. x 1¾-in. (76-mm x 44-mm) cross section, as shown in Figures 28 through 31. The post spacing between adjacent MWPs was 10 ft (3.05 m).

A prototype breakaway cable end terminal system was utilized at each end of the cable barrier system, as shown in Figures 16, 17 and 20 through 23. Post nos. 1 and 62 consisted of 4-cable anchor bracket assemblies that were anchored to reinforced concrete foundations at both ends of the system. Post nos. 2 and 61 were slip-base support posts with attached hanger

hardware, as shown in Figures 24 through 27. The spacing between the cable anchor brackets and the adjacent slip-base support posts was 8 ft (2.4 m).

Cable nos. 1 through 3 were attached to the MWP's using bolted, tabbed brackets. These brackets were fabricated from 12 gauge (2.7 mm) steel and bolted to the post utilizing a $\frac{5}{16}$ -in. (8-mm) diameter, 1-in. (25-mm) long bolt. Cable no. 4 was secured within the V-notch on top of each post with a $\frac{3}{16}$ -in. (5-mm) diameter brass keeper rod. Details for the cable-to-post attachment brackets and brass keeper rods can be found in Figures 28 through 34.

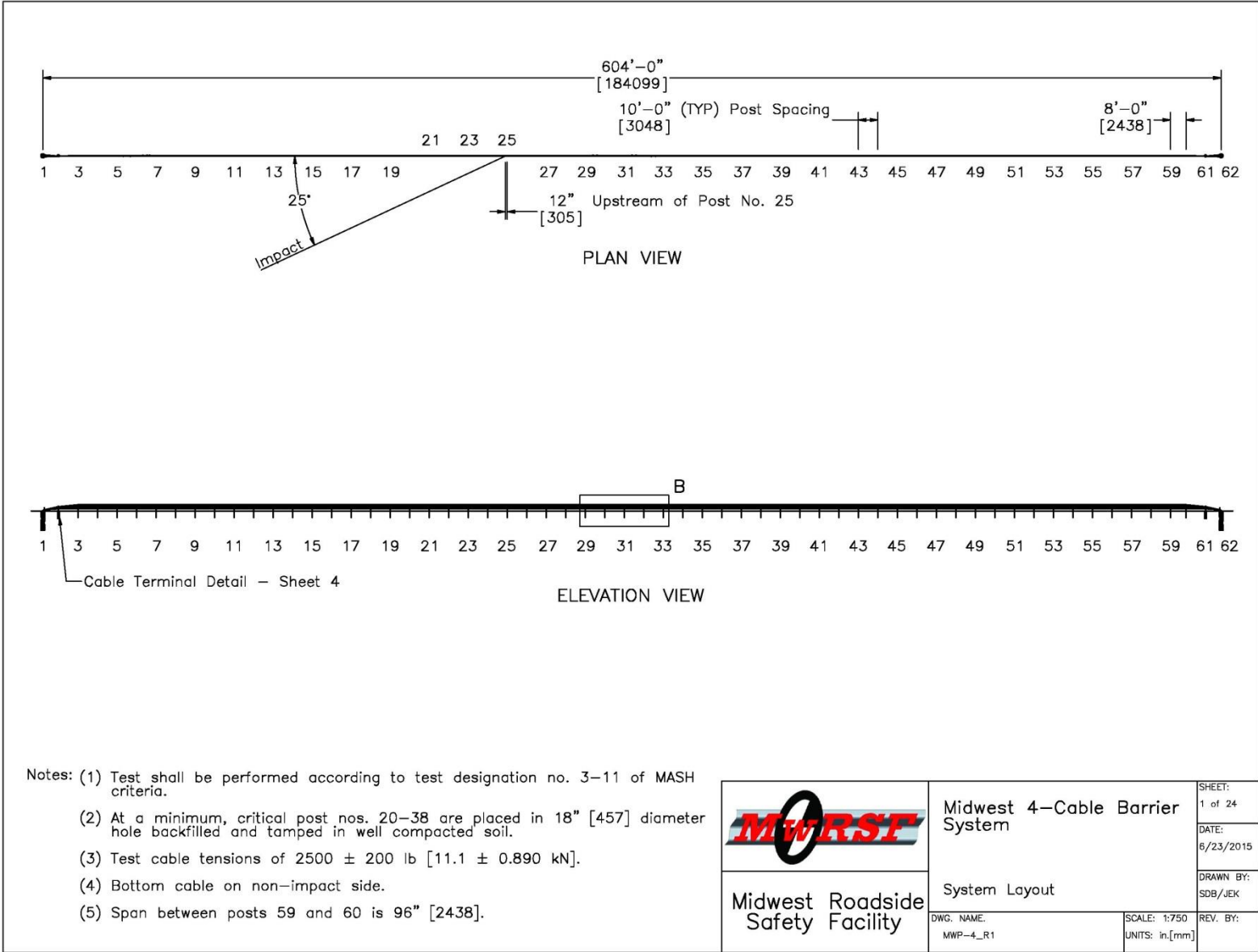


Figure 14. Test Installation Layout, Test No. MWP-4

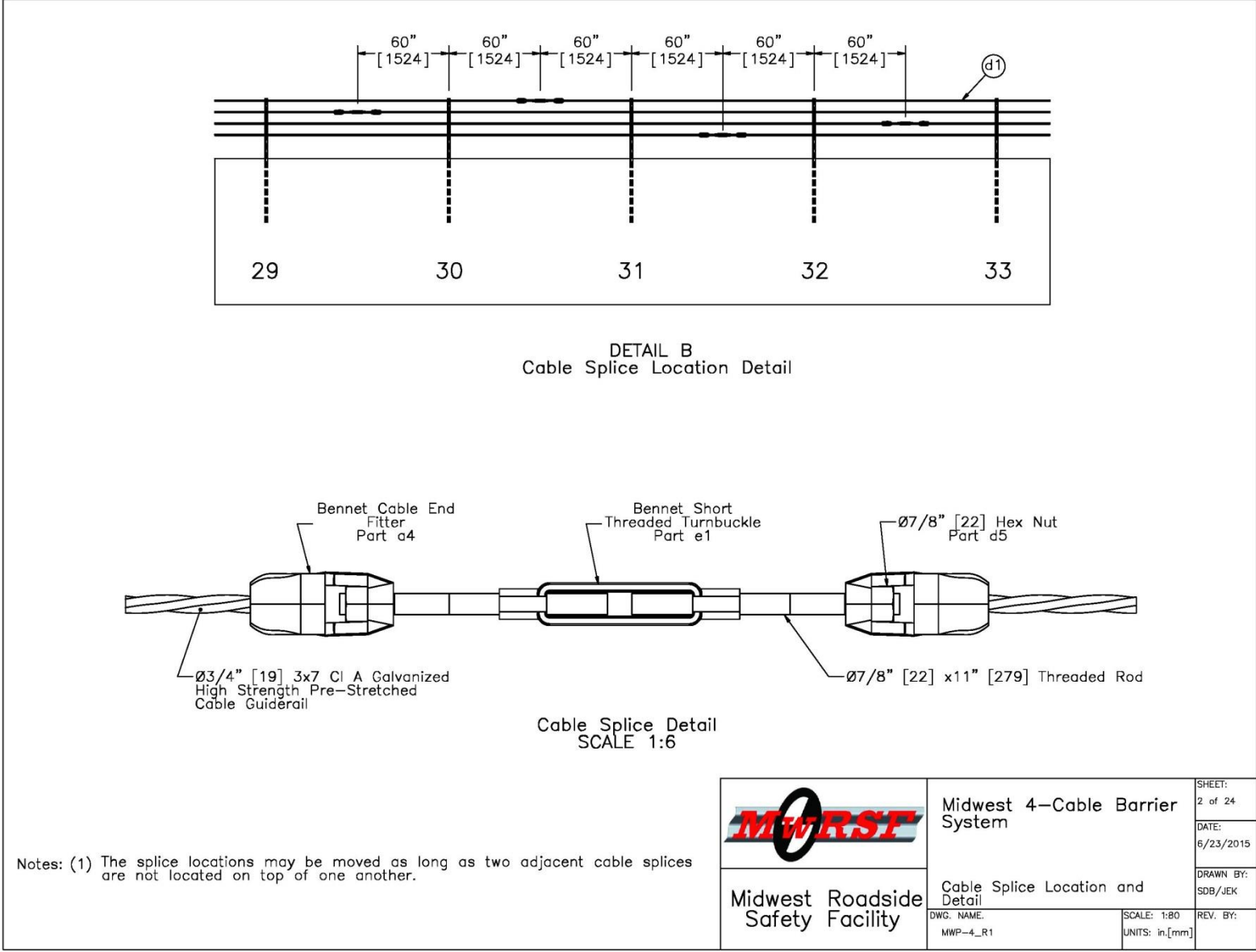


Figure 15. Cable Splice Location and Detail, Test No. MWP-4

35

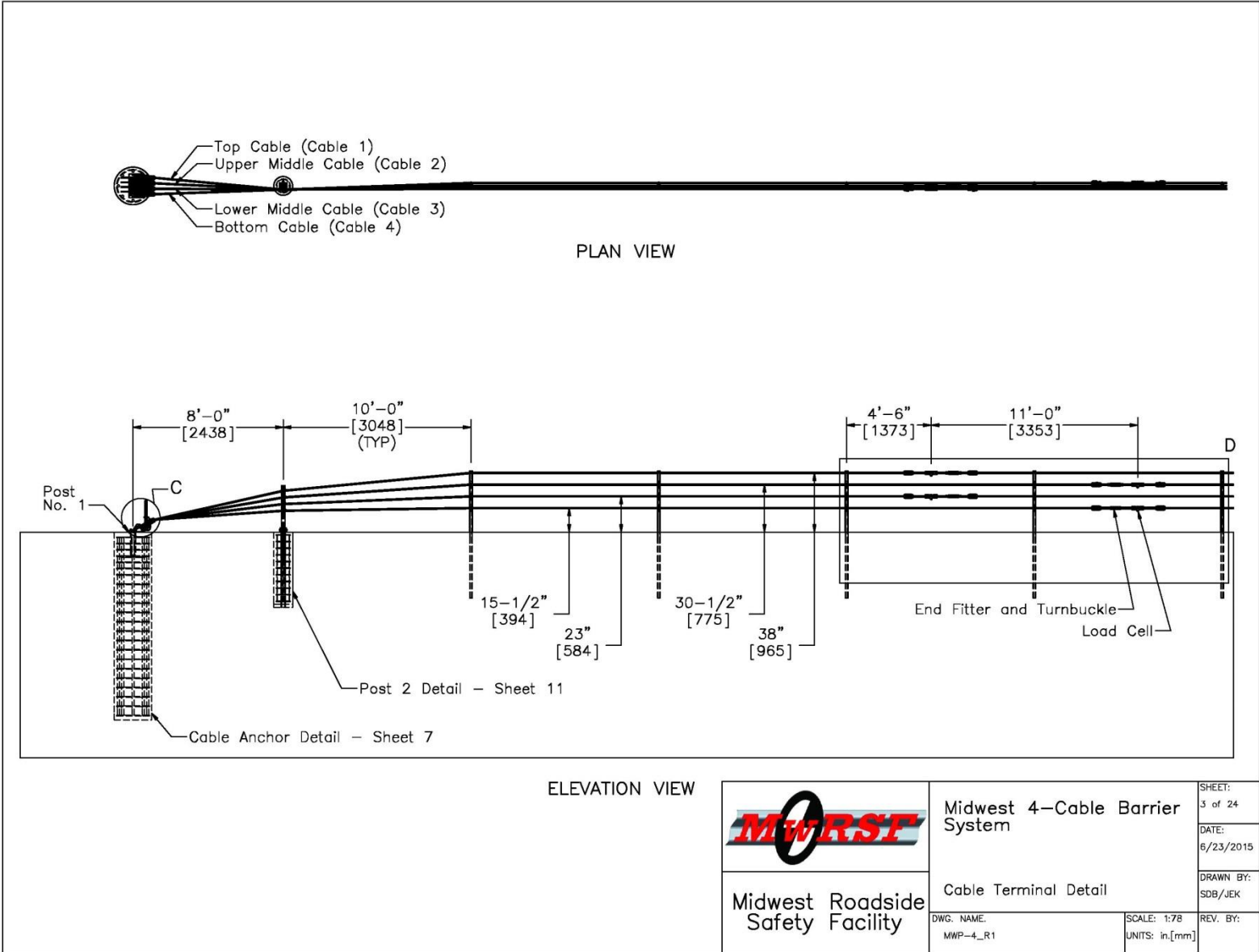


Figure 16. Cable Terminal Detail, Test No. MWP-4

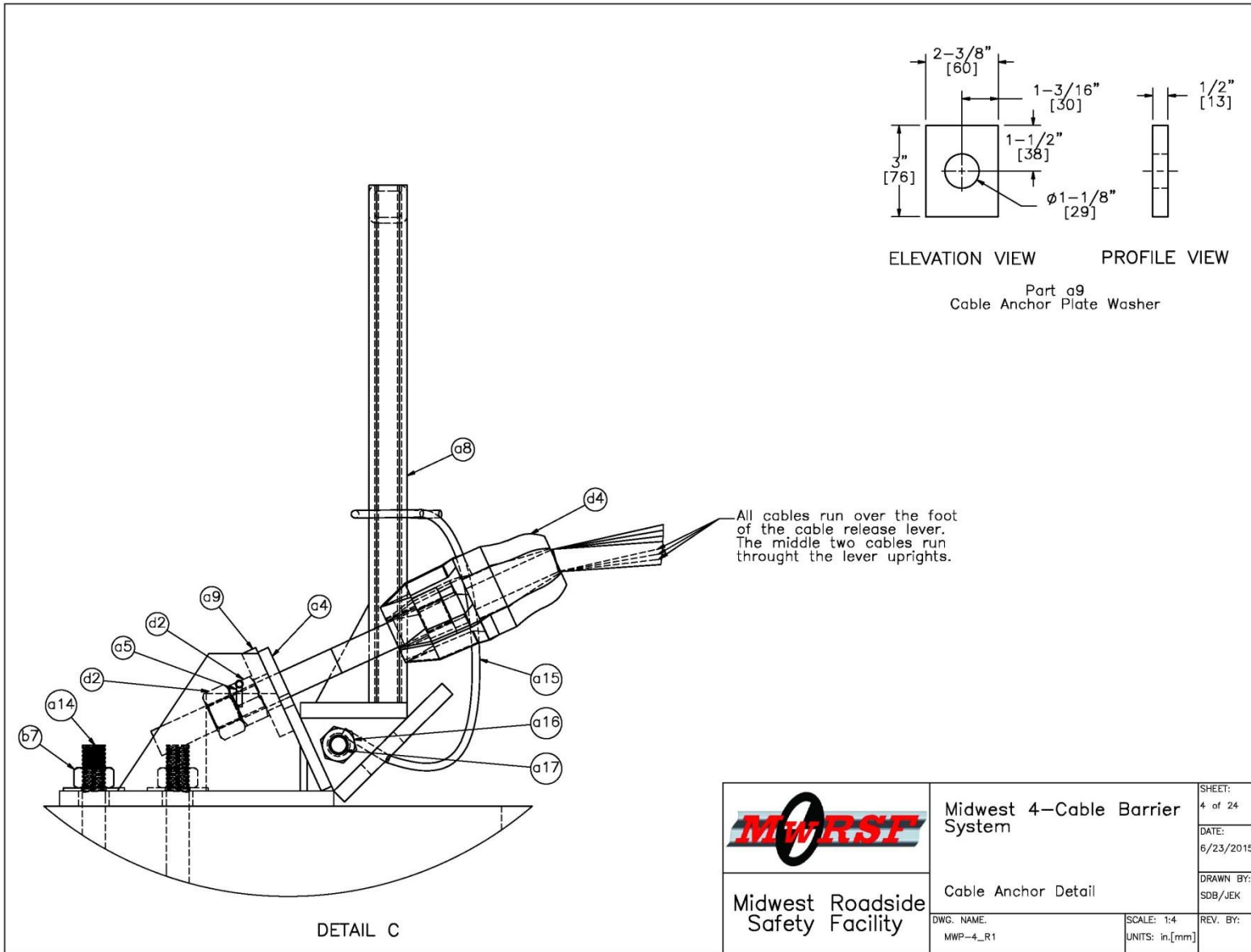


Figure 17. Cable Anchor Detail, Test No. MWP-4

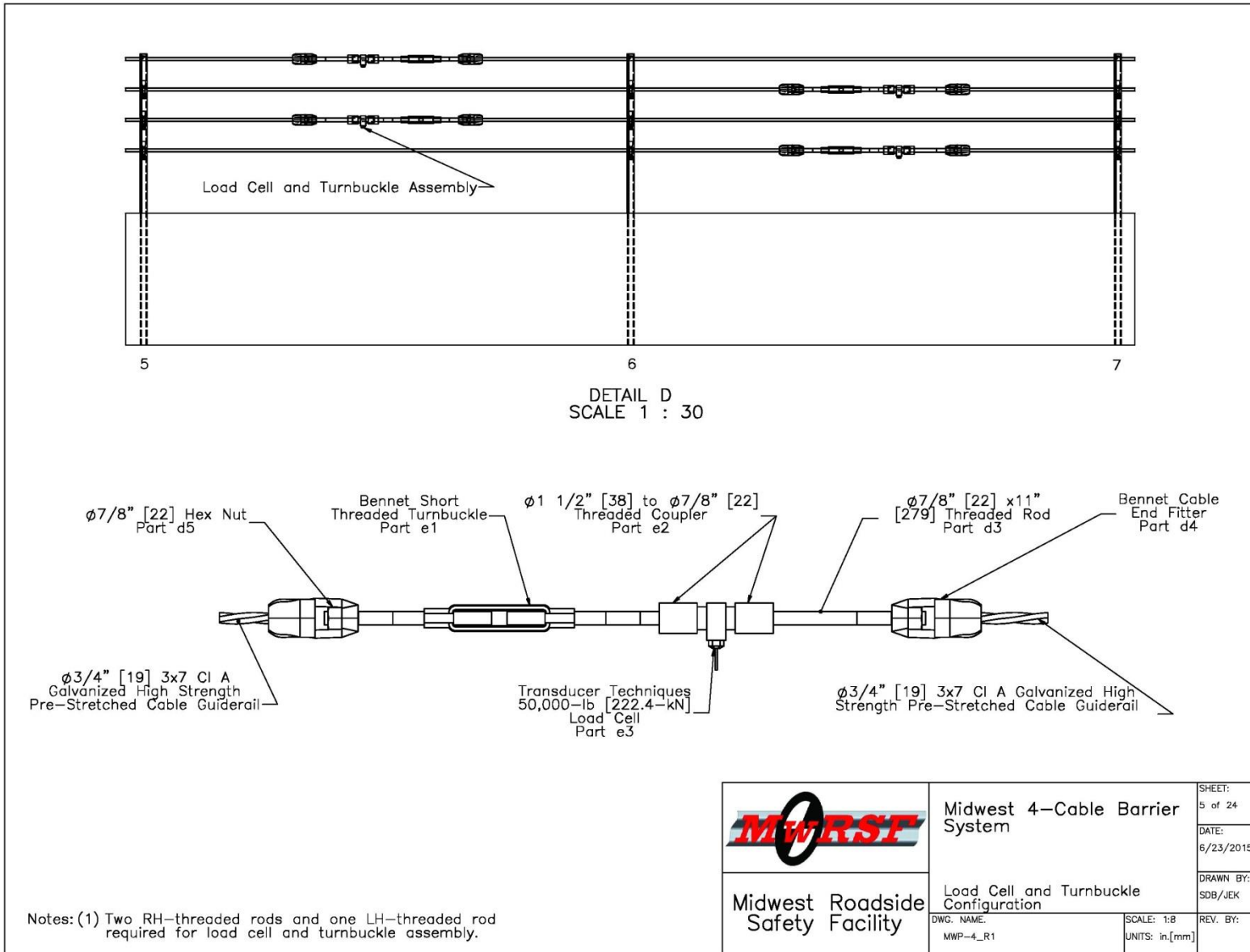


Figure 18. Load Cell and Turnbuckle Configuration, Test No. MWP-4

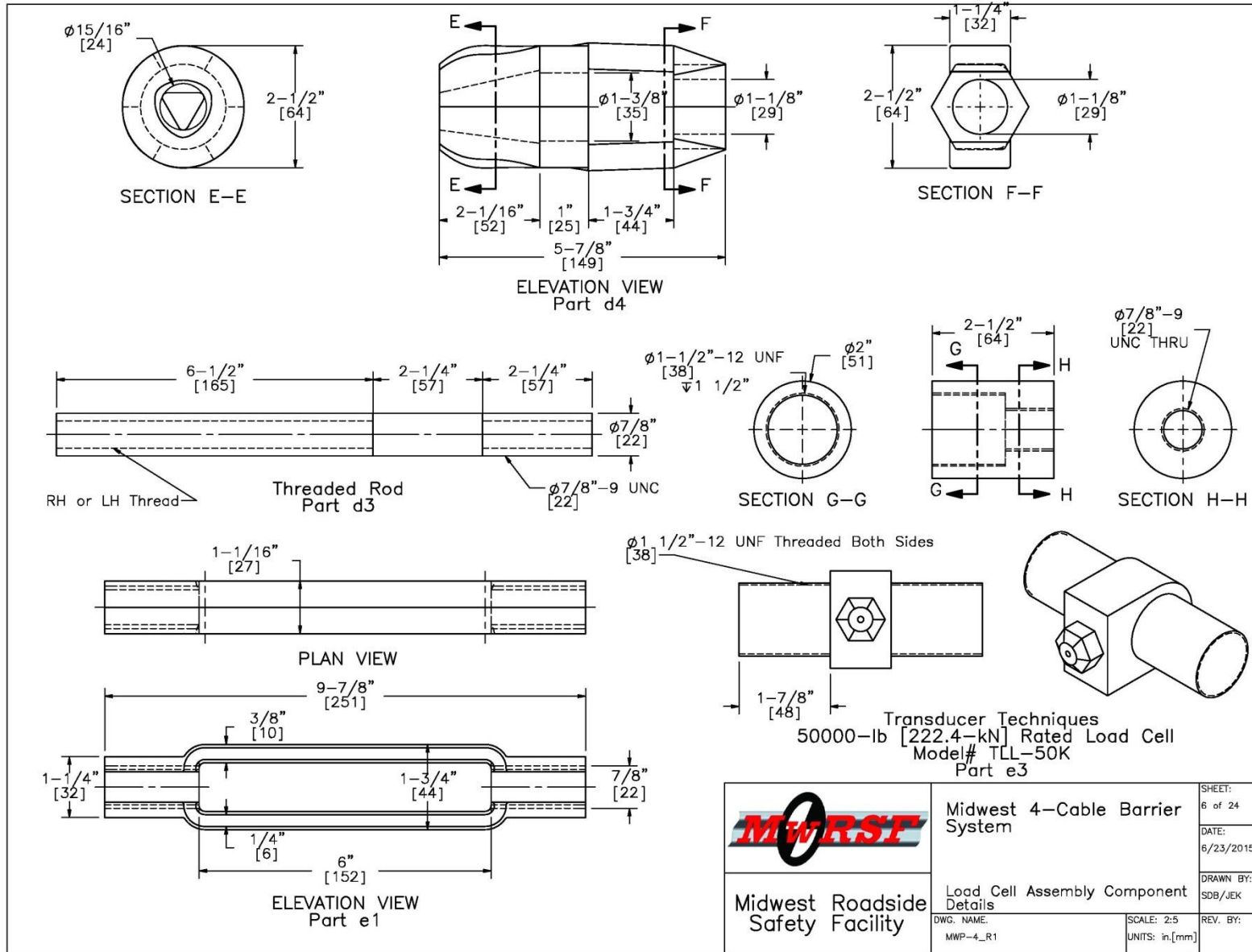



Figure 19. Load Cell Assembly Details, Test No. MWP-4

	Midwest 4-Cable Barrier System		SHEET: 6 of 24
	Load Cell Assembly Component Details		DATE: 6/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-4_R1	SCALE: 2:5 UNITS: in,[mm]	DRAWN BY: SDB/JEK REV. BY:

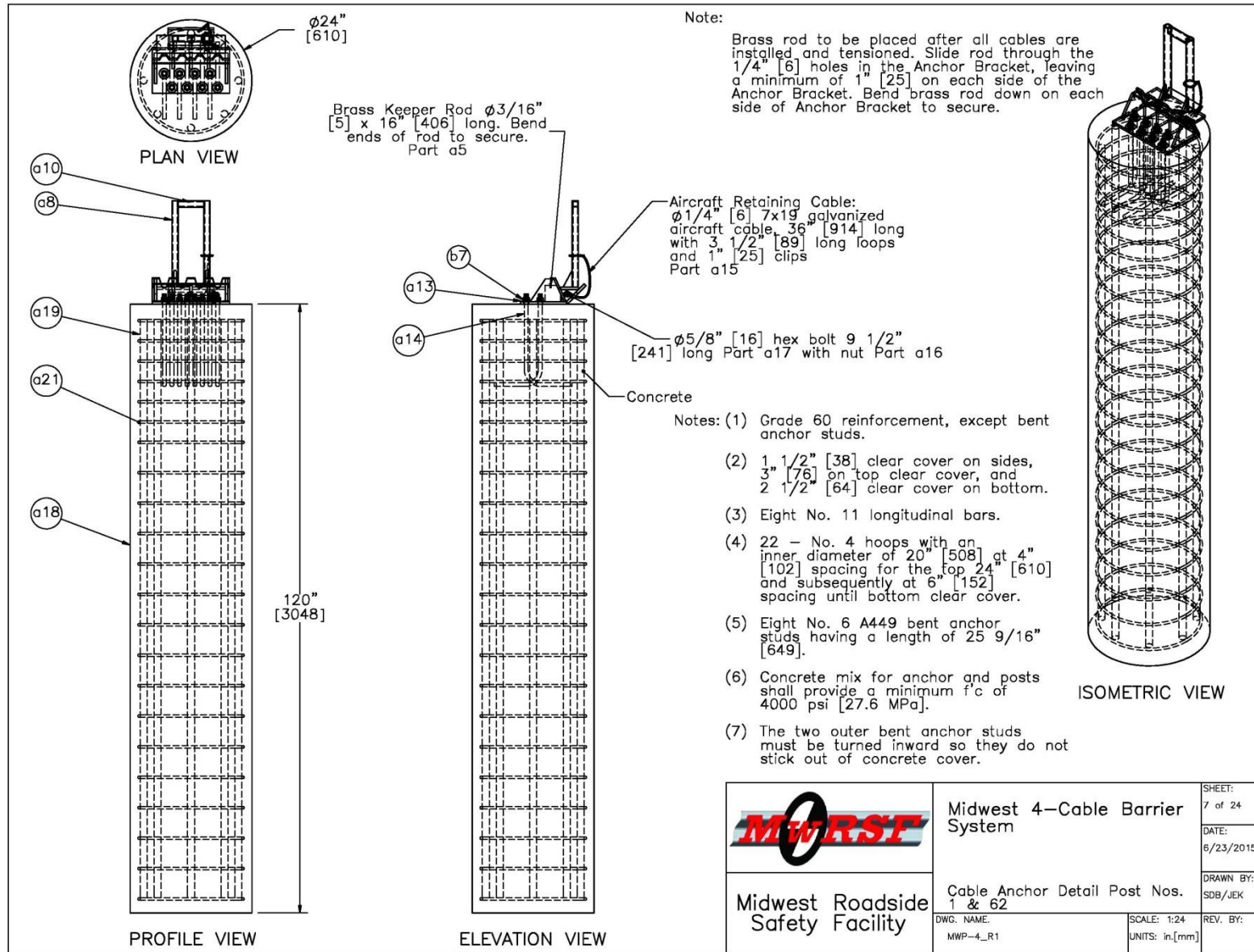


Figure 20. Cable Anchor Detail, Post Nos. 1 and 62, Test No. MWP-4

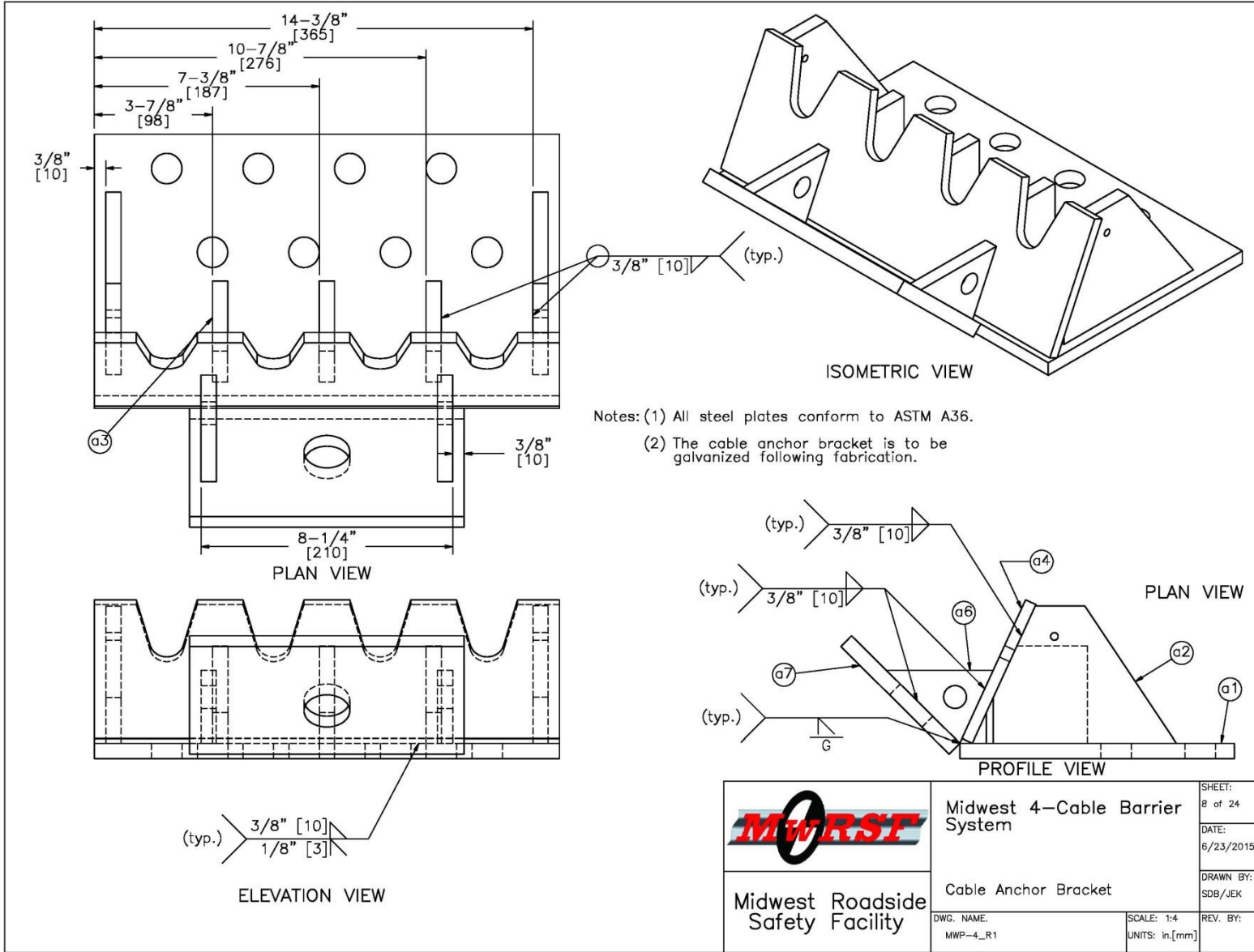


Figure 21. Cable Anchor Bracket, Test No. MWP-4

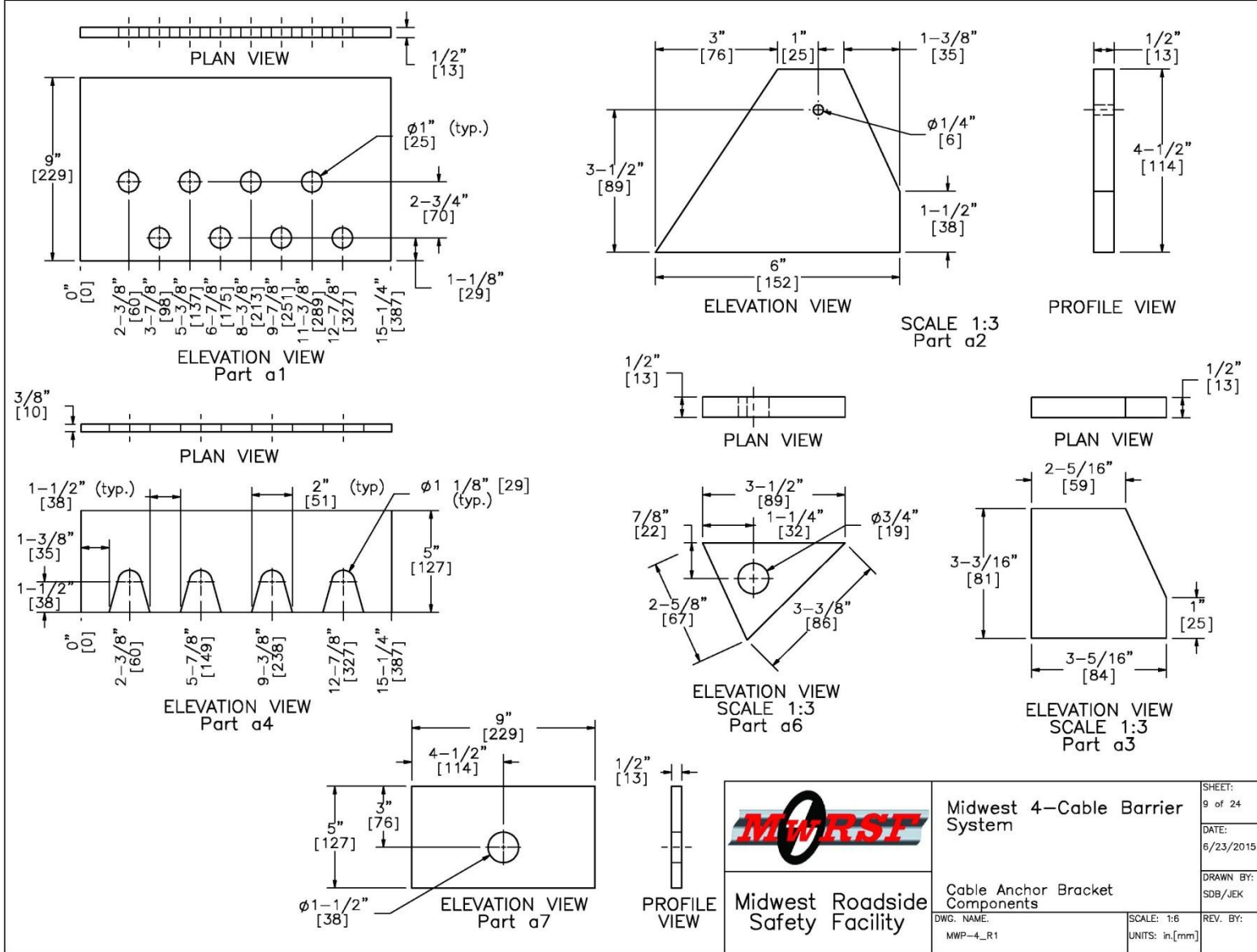


Figure 22. Cable Anchor Bracket Components, Test No. MWP-4

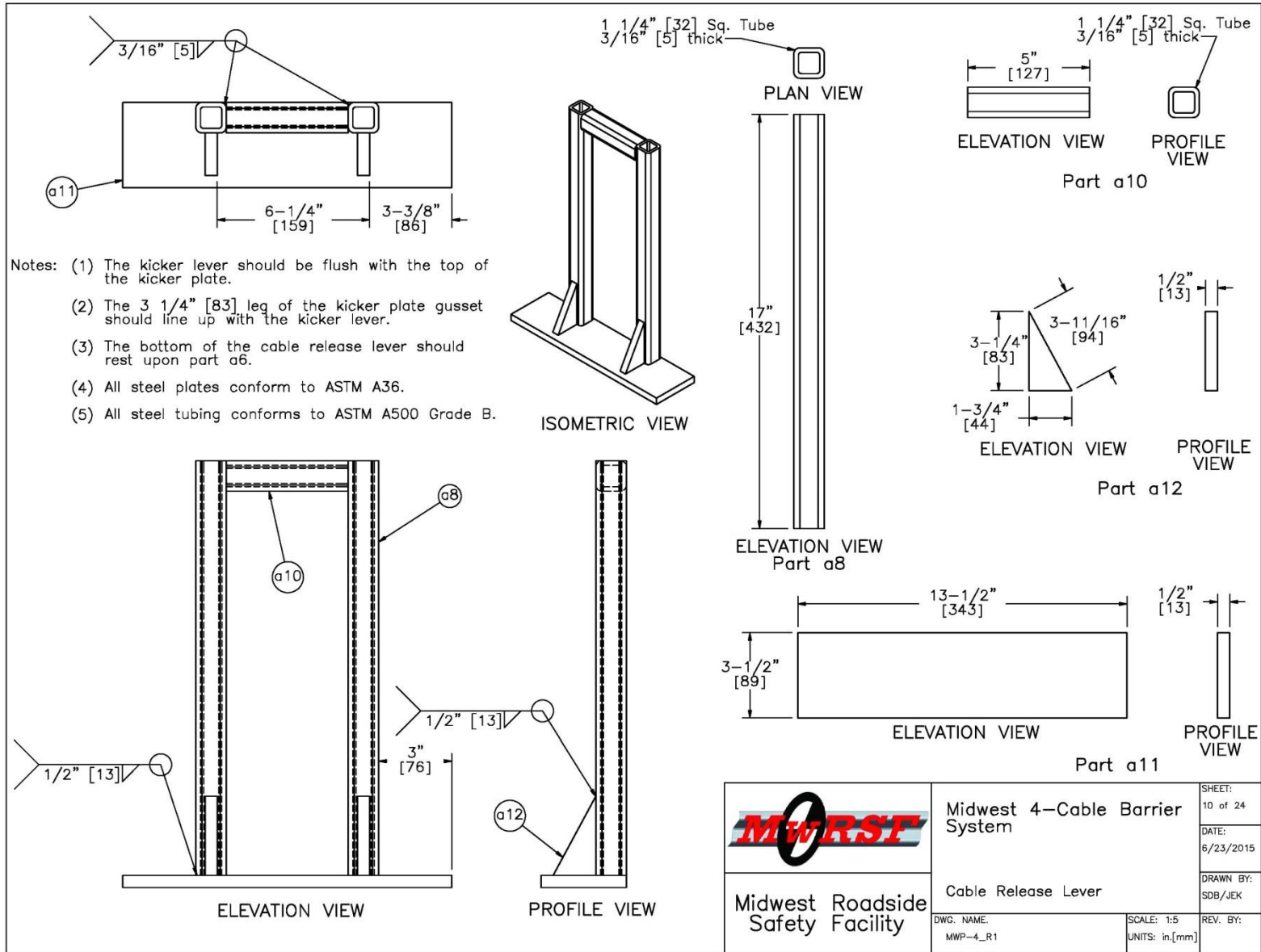


Figure 23. Cable Release Lever, Test No. MWP-4

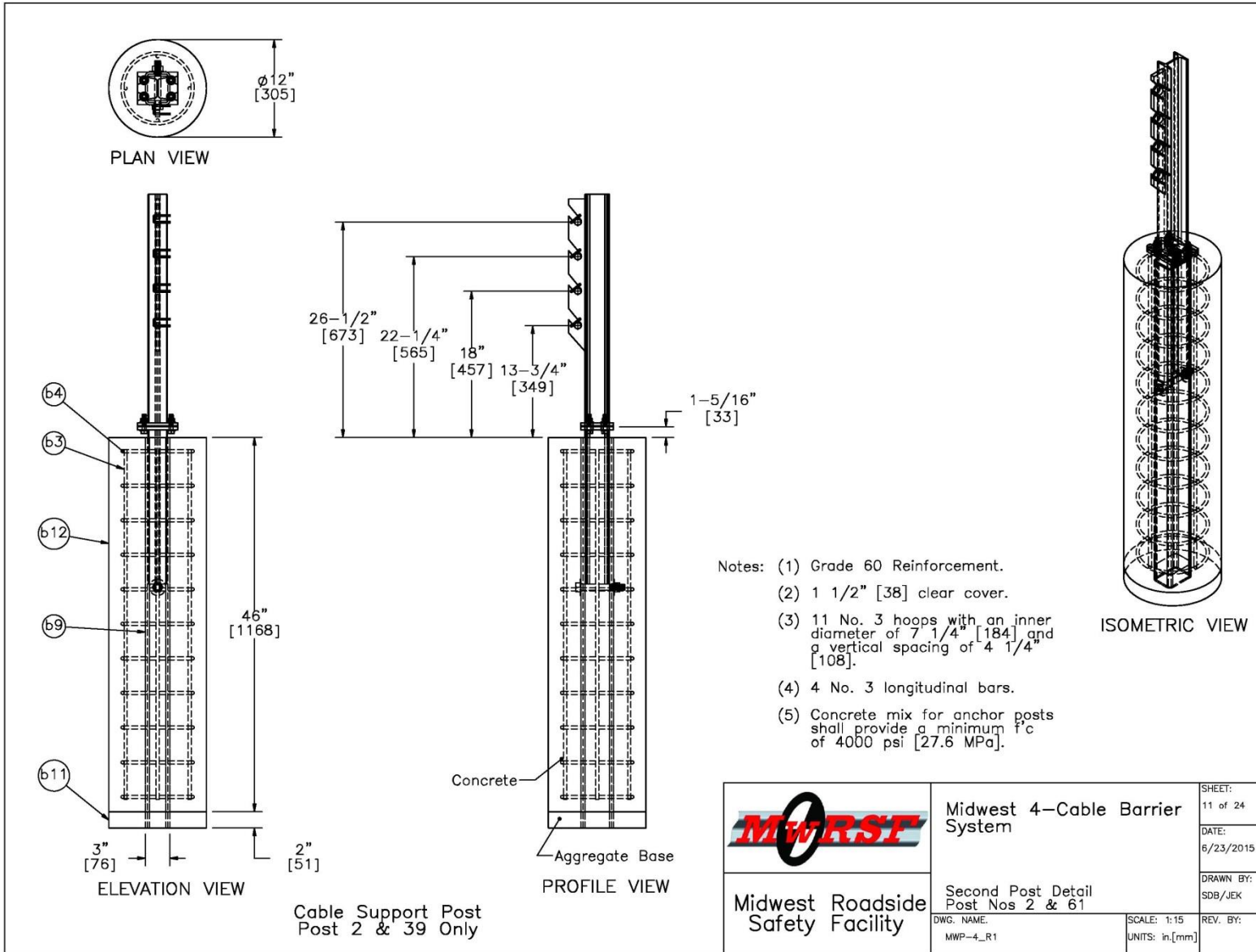


Figure 24. Second Post Details, Post Nos. 2 and 61, Test No. MWP-4

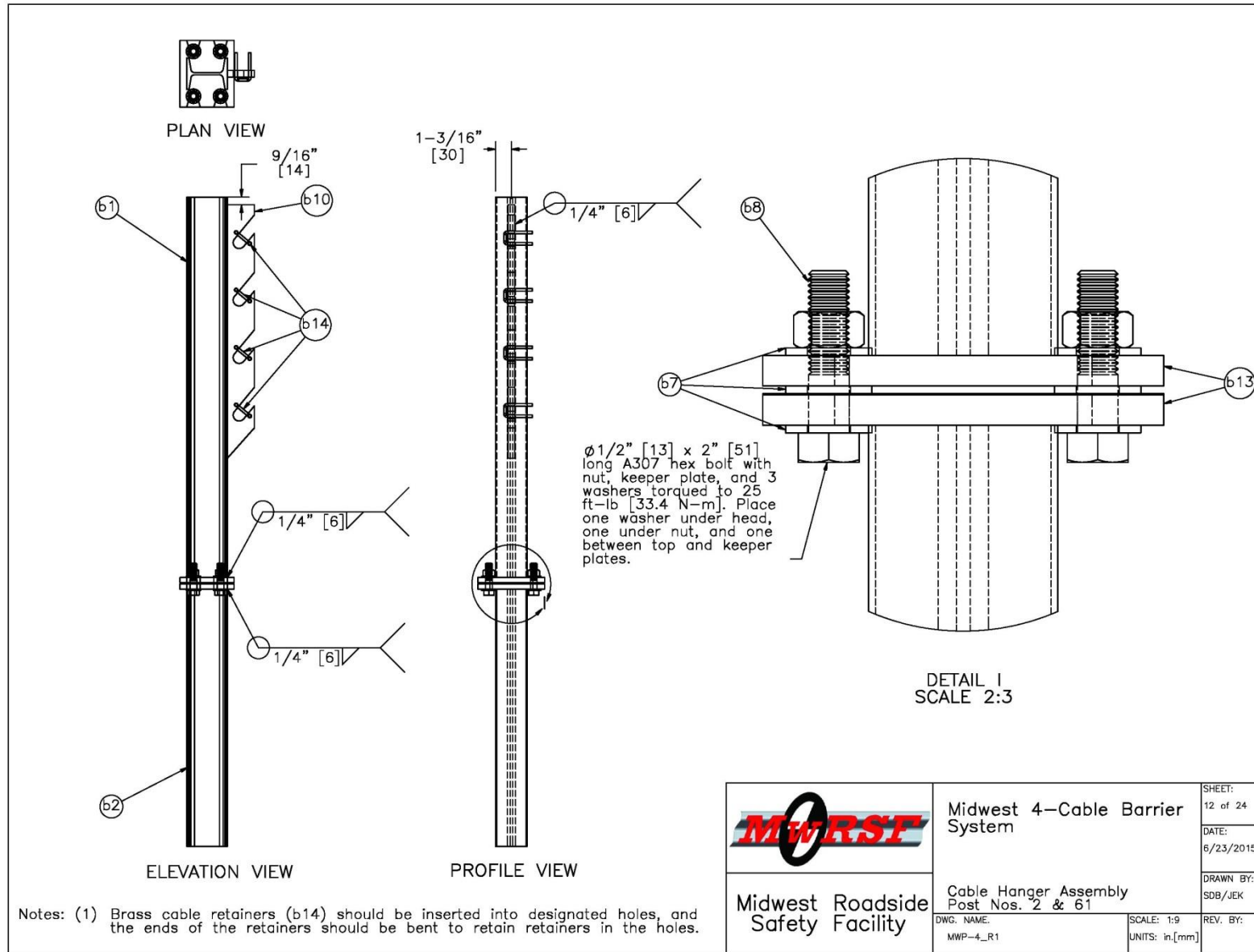


Figure 25. Cable Hanger Assembly, Post Nos. 2 and 61, Test No. MWP-4

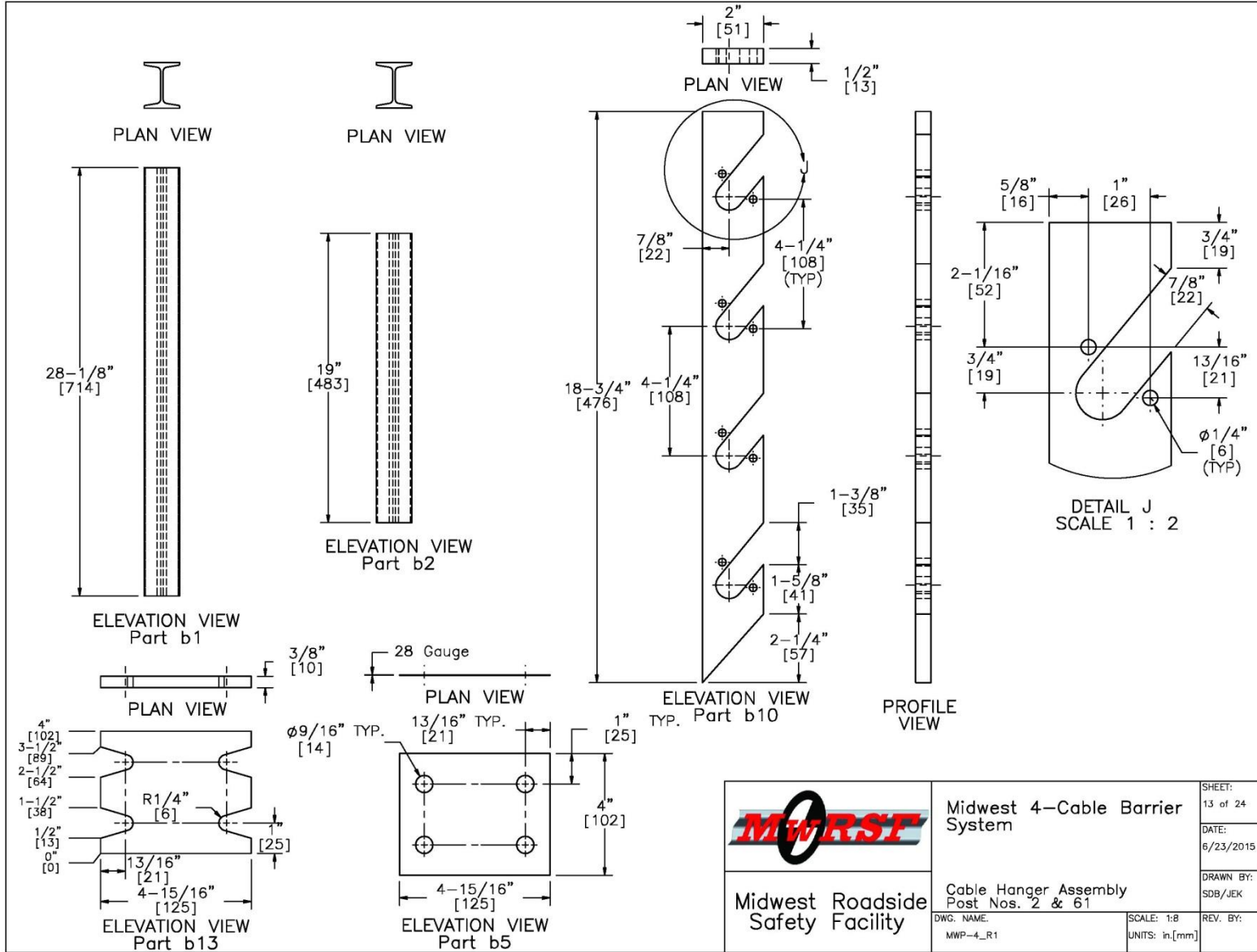



Figure 26. Cable Hanger Assembly, Post Nos. 2 and 61, Test No. MWP-4

 Midwest Roadside Safety Facility	Midwest 4-Cable Barrier System	SHEET: 13 of 24
	Cable Hanger Assembly Post Nos. 2 & 61	DATE: 6/23/2015
DWG. NAME: MWP-4_R1	SCALE: 1:8 UNITS: in.[mm]	DRAWN BY: SDB/JEK
		REV. BY:

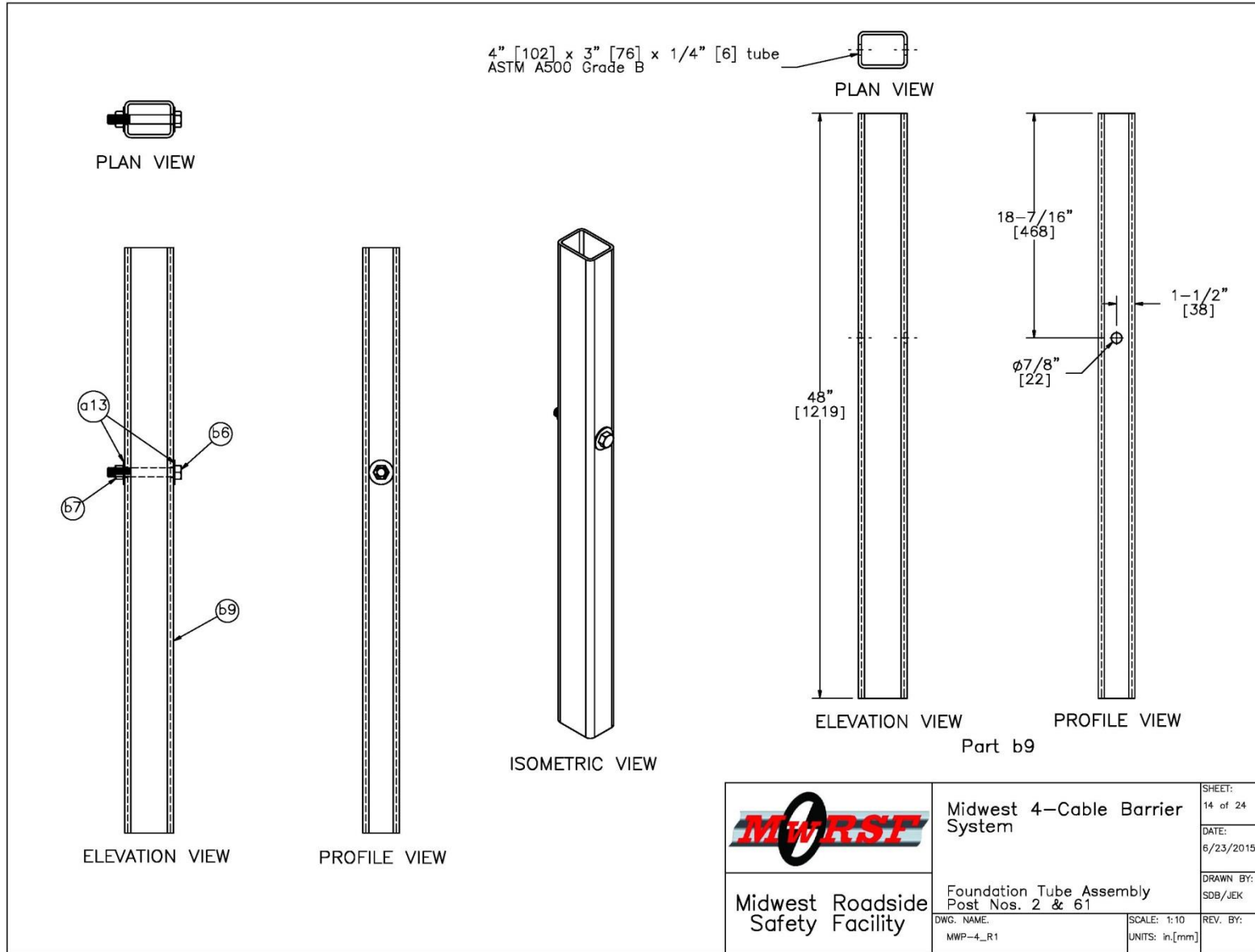


Figure 27. Foundation Tube Assembly, Post Nos. 2 and 61, Test No. MWP-4

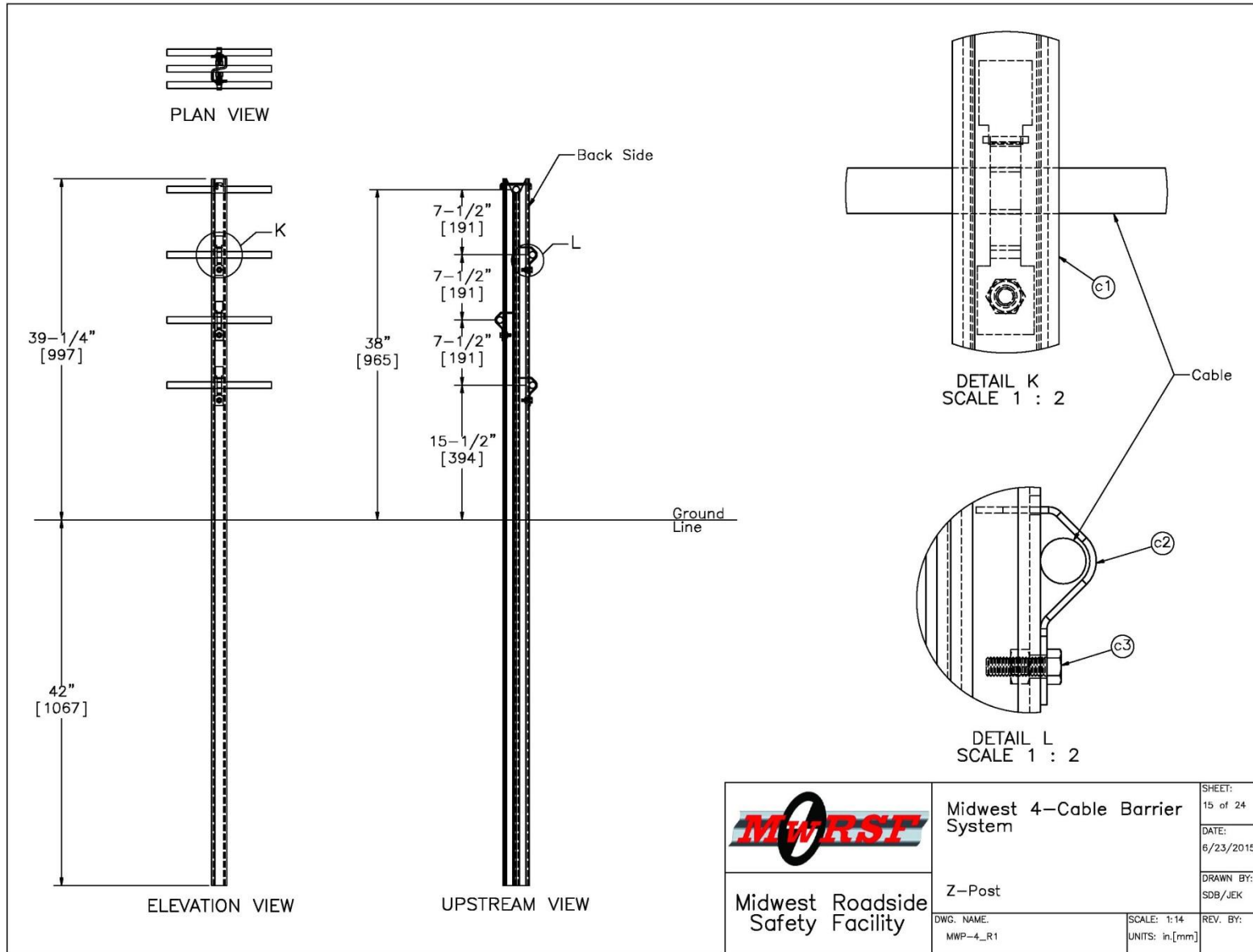


Figure 28. MWP Z-Post Details, Test No. MWP-4

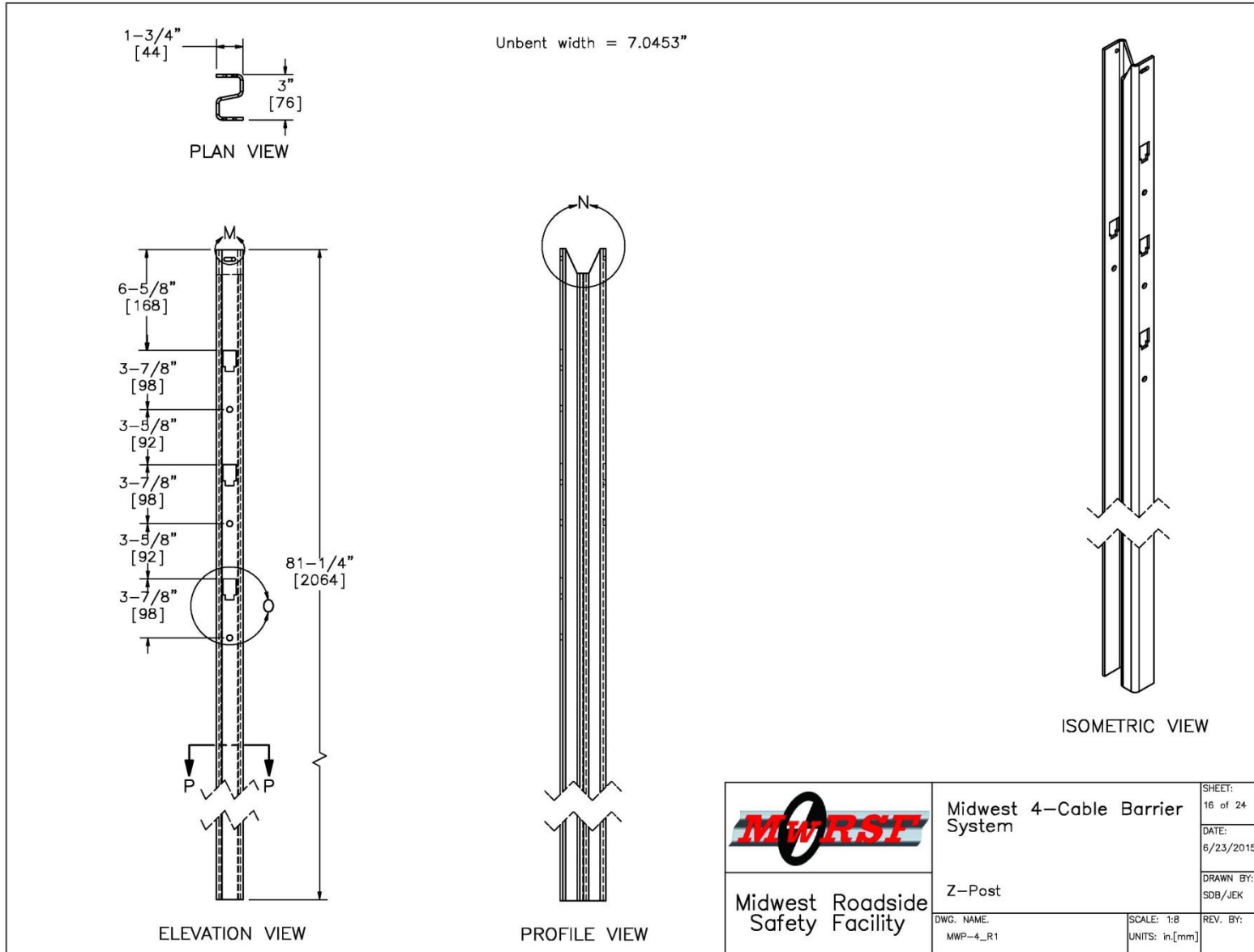


Figure 29. MWP Z-Post Details, Test No. MWP-4

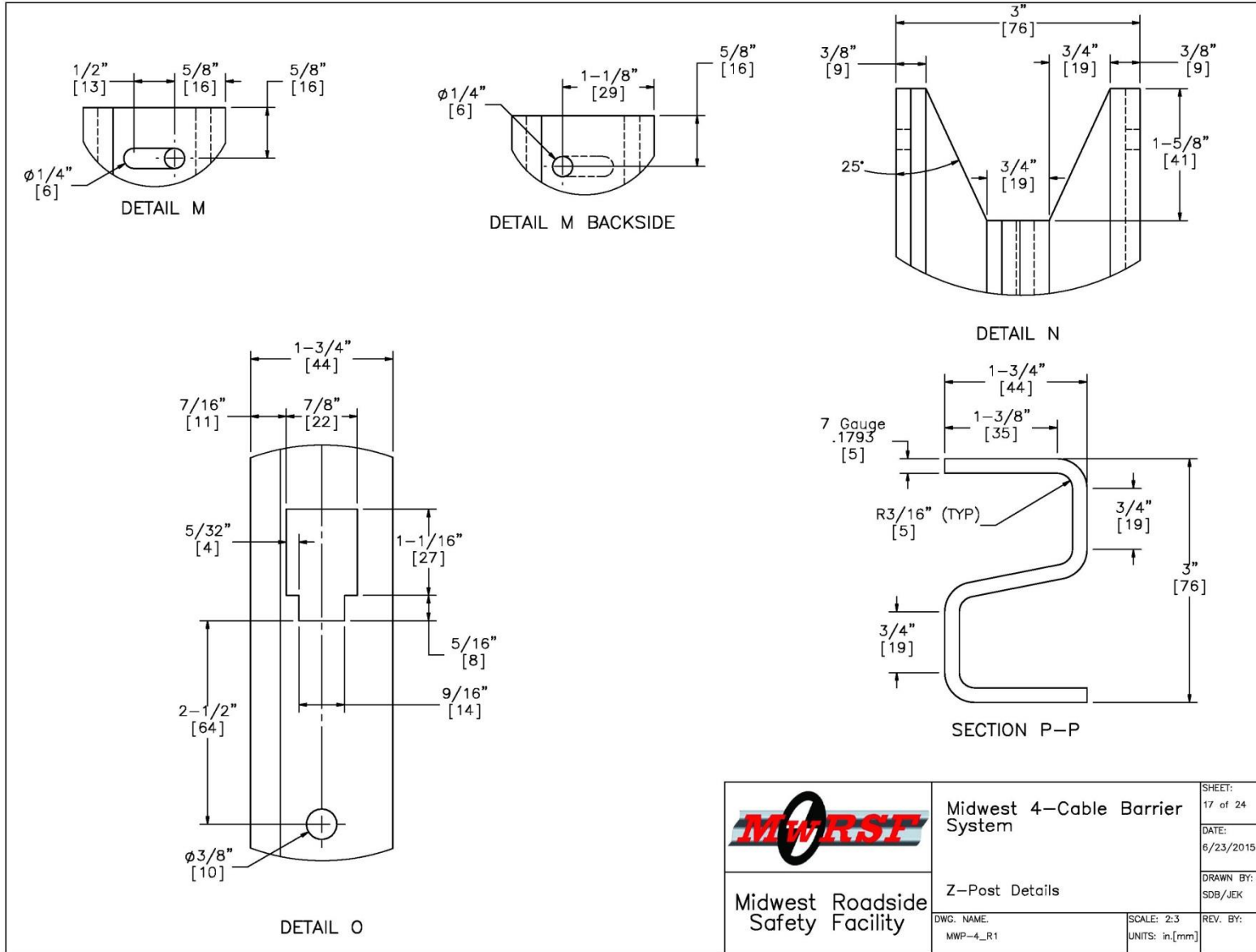


Figure 30. MWP Z-Post Details, Test No. MWP-4

50

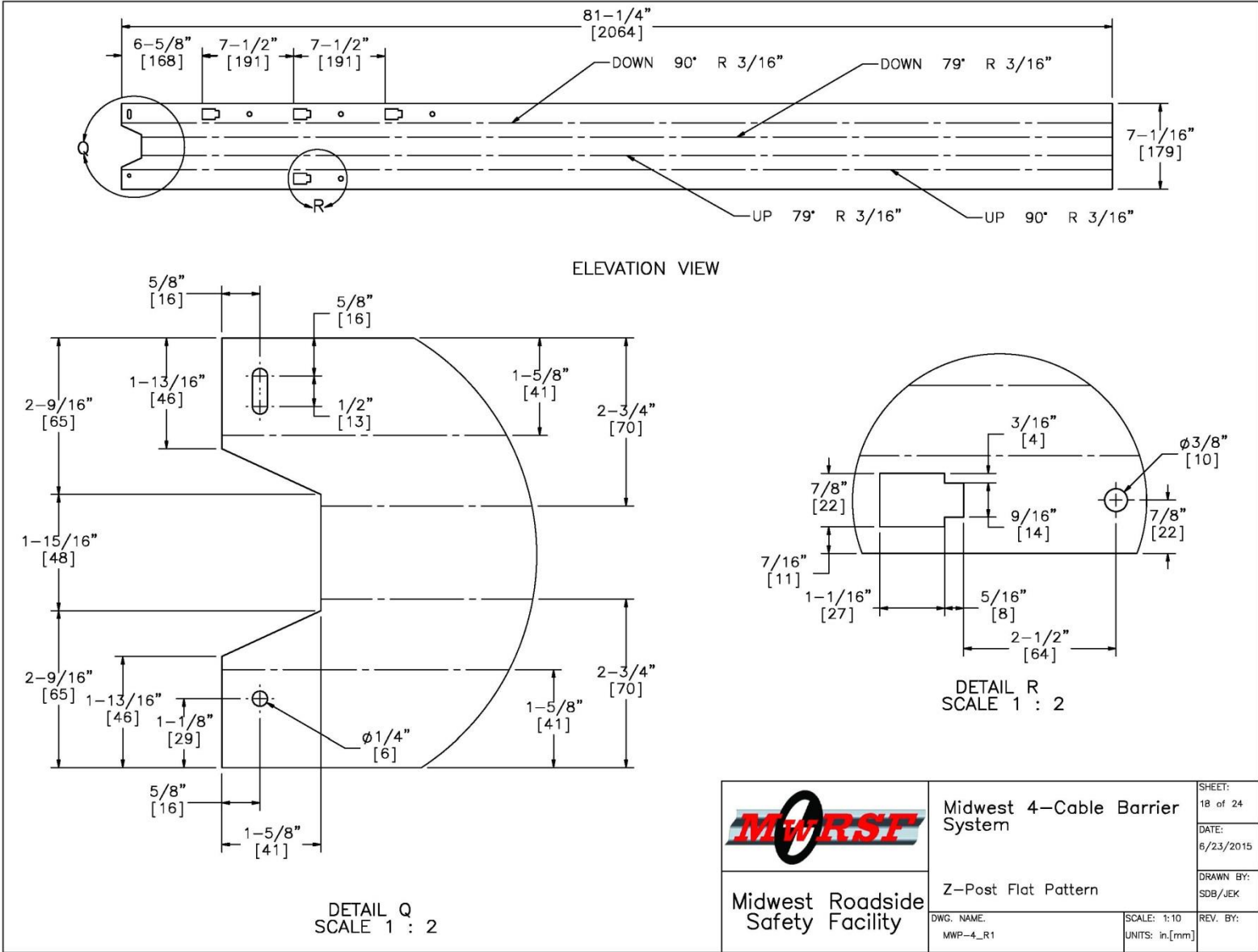


Figure 31. MWP Z-Post Details, Flat Pattern, Test No. MWP-4

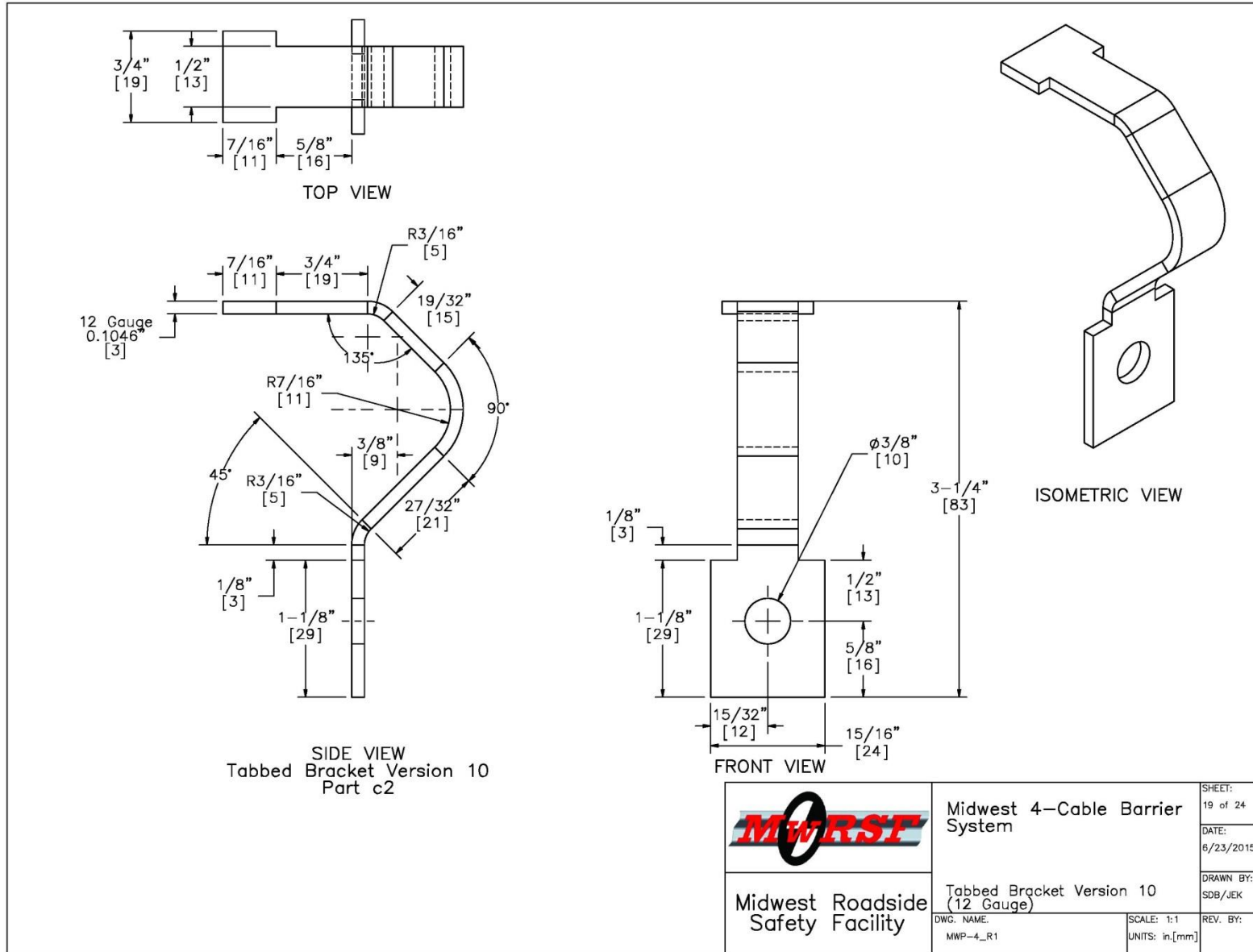
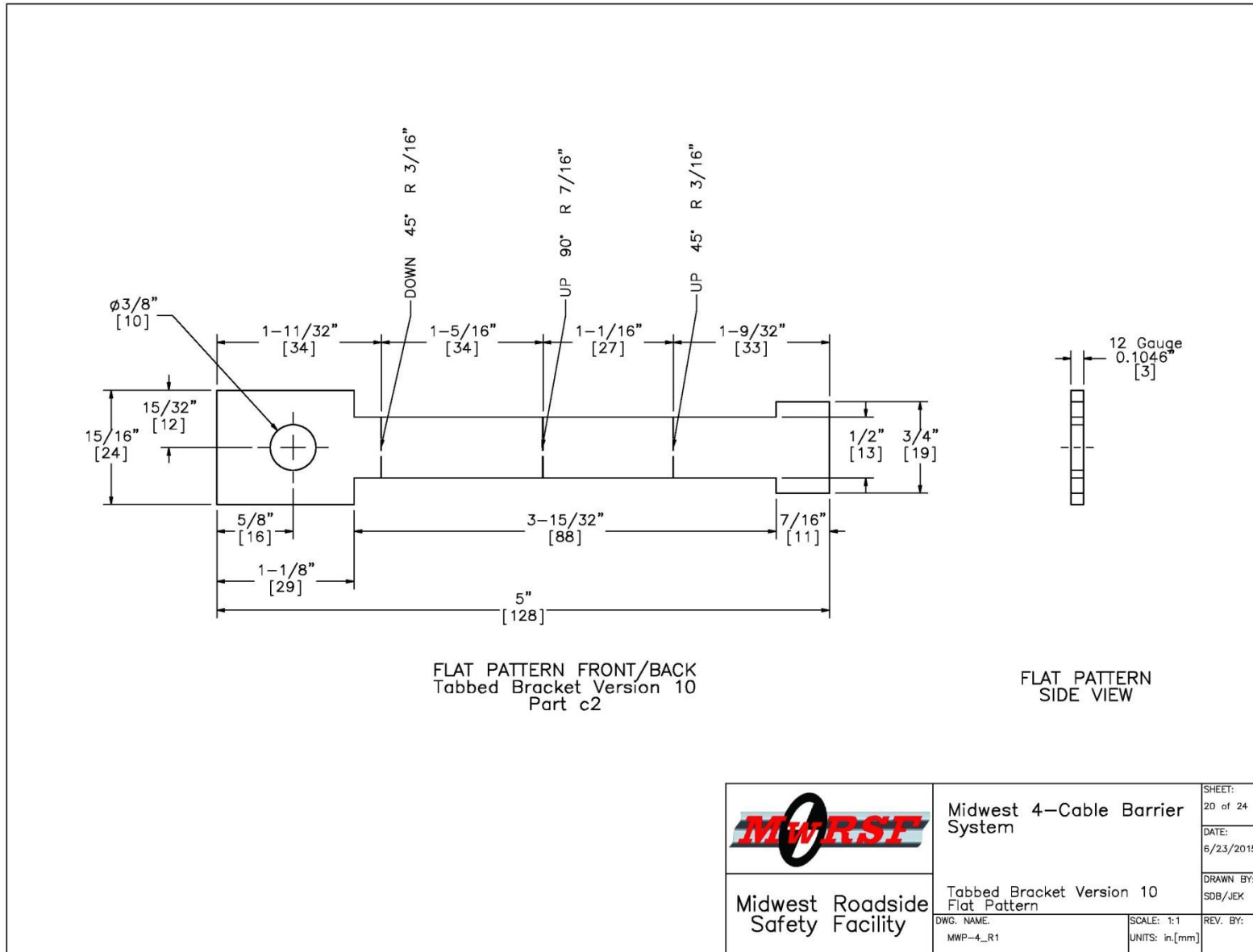


Figure 32. Tabbed Bracket Details, 12-Gauge, Test No. MWP-4




	Midwest 4-Cable Barrier System		SHEET: 20 of 24
	Tabbed Bracket Version 10 Flat Pattern		DATE: 6/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-4_R1	SCALE: 1:1 UNITS: in,[mm]	DRAWN BY: SDB/JEK
			REV. BY:

Figure 33. Tabbed Bracket Details, Flat Pattern, Test No. MWP-4

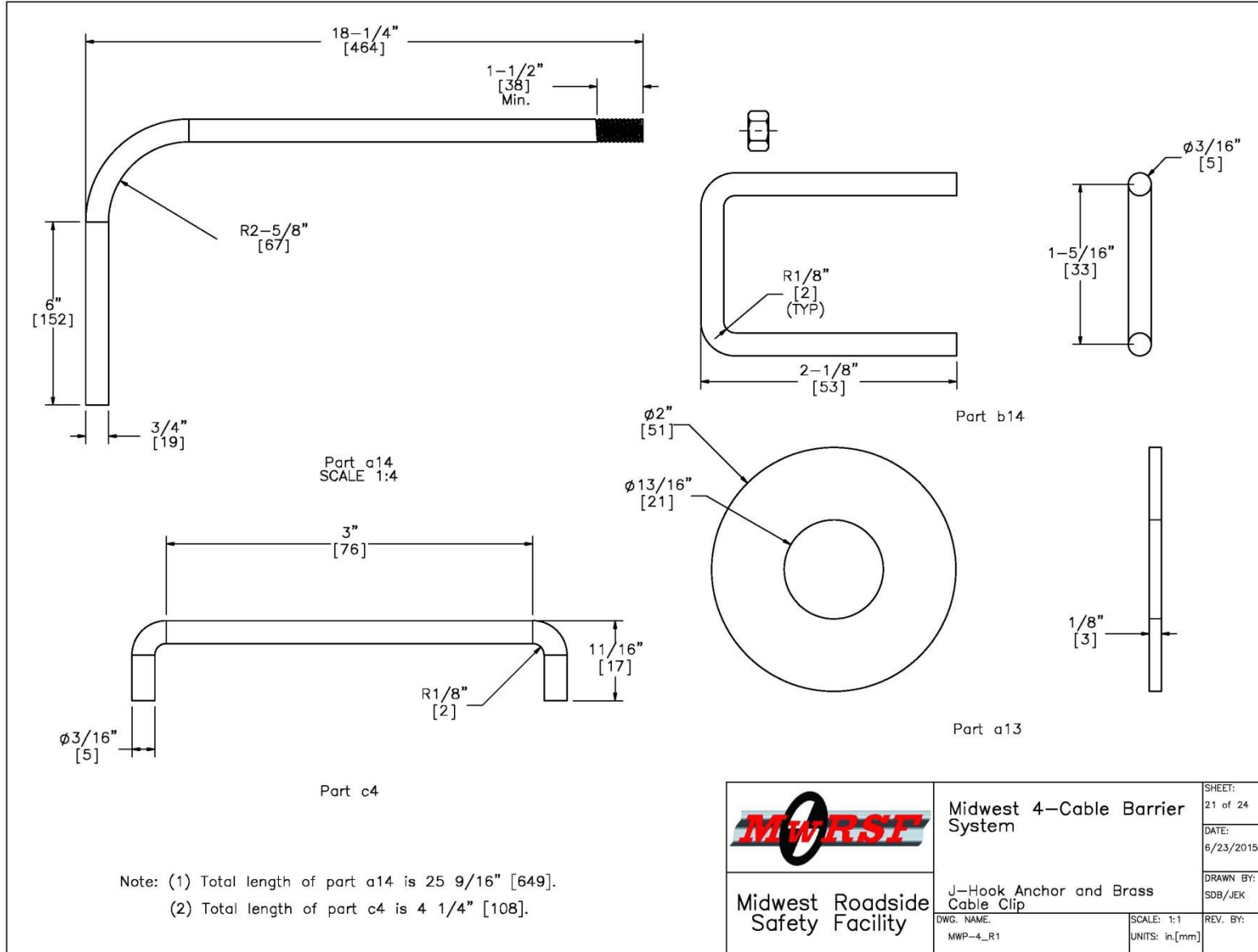


Figure 34. Brass Clips, Test No. MWP-4

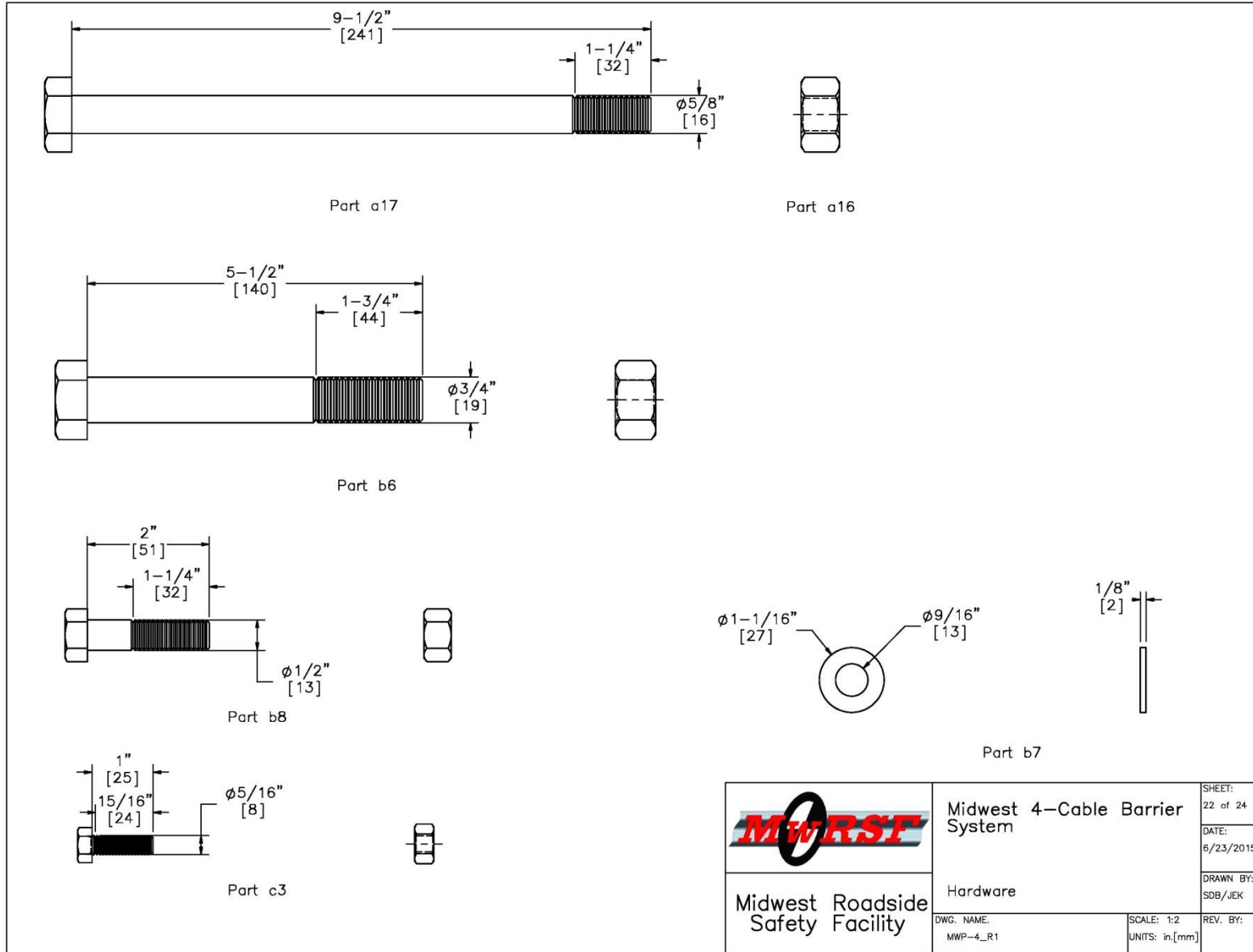


Figure 35. Hardware Details, Test No. MWP-4

Item No.	QTY.	Description	Material Specification
a1	2	Cable Anchor Base Plate	ASTM A36
a2	4	Exterior Cable Plate Gusset	ASTM A36
a3	6	Interior Cable Plate Gusset	ASTM A36
a4	2	Anchor Bracket Plate	ASTM A36
a5	2	3/16" [5] Dia. Brass Keeper Rod, 14" [356] long	Brass
a6	4	Release Gusset	A36 Steel
a7	2	Release Lever Plate	A36 Steel
a8	4	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Tube	ASTM A500 Gr. B
a9	8	CMB High Tension Anchor Plate Washer	ASTM A36
a10	2	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Connecting Tube	ASTM A 500 Gr. B
a11	2	3x10x0.5" [76x254x13] Kicker Plate	ASTM A36
a12	4	CT kicker – gusset	ASTM A36
a13	20	3/4" [19] Dia. Flat Washer	ASTM F844
a14	16	3/4" [19] Dia. UNC J–Hook Anchor and Hex Nut	J–Hook ASTM A449/Nut ASTM A563 DH
a15	2	1/4" [6] Dia. Aircraft Retaining Cable, 36" [914] long	7x19 Galv.
a16	2	5/8" [16] Dia. Heavy Hex Nut	ASTM A563C
a17	2	5/8" [16] Dia. UNC, 9 1/2" [241] Long Hex Bolt	ASTM A449 or SAE J429 Gr. 5
a18	2	24" [610] Dia. Concrete Anchor, 120" [3048] long	4,000 psi f'c
a19	16	#11 Straight Rebar, 114" [2896] long	Grade 60
a20	44	#4 Anchor Hoop Rebar with 21" [533] Dia.	Grade 60
b1	2	S3x5.7 [S76x8.5] Post by 28 1/8" [714]	ASTM A572 GR50–07, ASTM A709 GR50–09A, ASTM A992–06A
b2	2	S3x5.7 [S76x8.5] Post by 19" [483]	ASTM A572 GR50–07, ASTM A709 GR50–09A, ASTM A992–06A
b3	8	#3 Straight Rebar, 43" [1092] long	Grade 60
b4	22	7 1/4" [184] Dia. No. 3 Hoop Reinforcement	Grade 60
b5	2	2nd Post Keeper Plate, 28 Gauge	ASTM A36
b6	2	3/4" [19] Dia. UNC, 5 1/2" [140] Long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b7	24	1/2" [13] Dia. Washer with 1 1/16" [27] OD	ASTM F844
b8	8	1/2" [13] Dia. UNC, 2" [51] long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b9	2	4x3x1/4" [102x76x6] Foundation Tube, 48" [1168] long	ASTM A500 Grade B
b10	2	2nd Post Cable Hanger	ASTM A36
b11	2	2nd Post Anchor Aggregate 12 in, Depth	–
b12	2	12" Dia. 2nd Post Concrete Anchor, 46" long	4,000 psi f'c
b13	4	2nd Post Base Plate	ASTM A36
b14	8	3/16" [5] Dia. 5 1/4" [133] Long Brass Rod	ASTM B16–00

 Midwest Roadside Safety Facility	Midwest 4–Cable Barrier System	SHEET: 23 of 24 DATE: 6/23/2015 DRAWN BY: SDB/JEK
	Bill of Materials	DWG. NAME: MWP–4_R1 SCALE: NONE UNITS: in,[mm] REV. BY:

Figure 36. Bill of Materials, Test No. MWP-4

Item No.	QTY.	Description	Material Spec
c1	58	3"x1-3/4"x7 Gauge [76x44x4.6], 81 1/4" [2064] Long Bent MWP Z-Section Post	Hot-Rolled ASTM A1011 HSLA Gr. 50
c2	174	12 Gauge Tabbed Bracket - Version 10	Hot-Rolled ASTM A1011 HSLA Grade 50
c3	174	5/16" [8] Dia. UNC, 1" [25] Long Hex Cap Screw and Nut	Bolt SAE J429 Gr. 5 or ASTM A449/Nut ASTM A563 DH
c4	58	Straight Rod - ϕ 3/16" [5] Cable Clip	ASTM B16 Brass C36000 Half Hard (H02), ROUND. TS \geq 68.0 ksi, YS \geq 52.0 ksi
d1	1	3/4" [19] Dia. 3x7 Cable Guiderail	AASHTO M30-92(2000)/ASTM A741-98 Type 1 Class A coating except with Type 1 minimum breaking strength = 39 kips [173.5 kN]
d2	16	7/8" [22] Dia. Hex Nut	ASTM A563C
d3	28	Cable End Threaded Rod	ASTM A449
d4	24	Bennet Cable End Fitter	ASTM A47
d5	24	7/8" [22] Dia. Hex Nut	SAE J429 Gr. 5
e1	8	Bennet Short Threaded Turnbuckle	Not Specified
e2	8	Threaded Load Cell Coupler	N/A
e3	4	50,000-lb [222.4-kN] Load Cell	N/A


	Midwest 4-Cable Barrier System	SHEET: 24 of 24
	Bill of Materials	DATE: 6/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-4_R1	DRAWN BY: SDB/JEK
	SCALE: NONE	REV. BY:
	UNITS: in,[mm]	

Figure 37. Bill of Materials, Test No. MWP-4

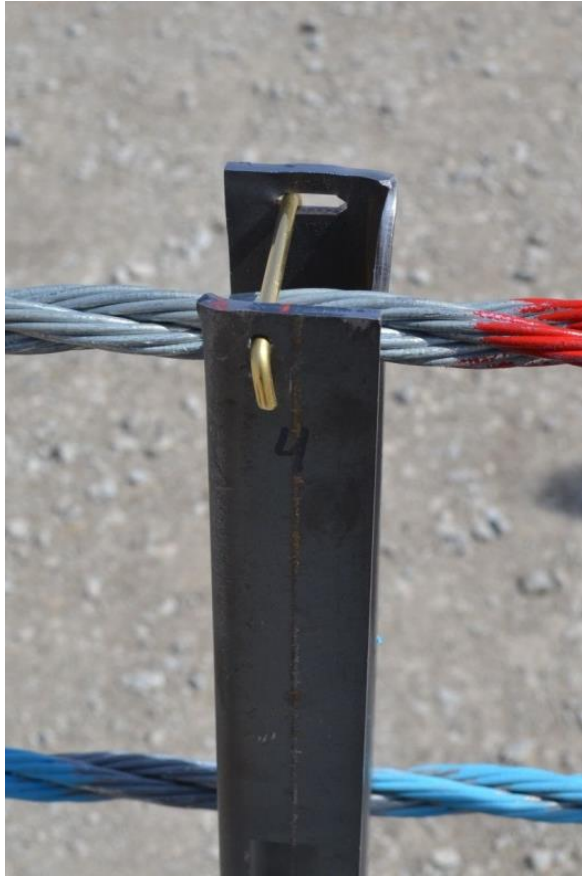


Figure 38. Test Installation Photographs, Test No. MWP-4

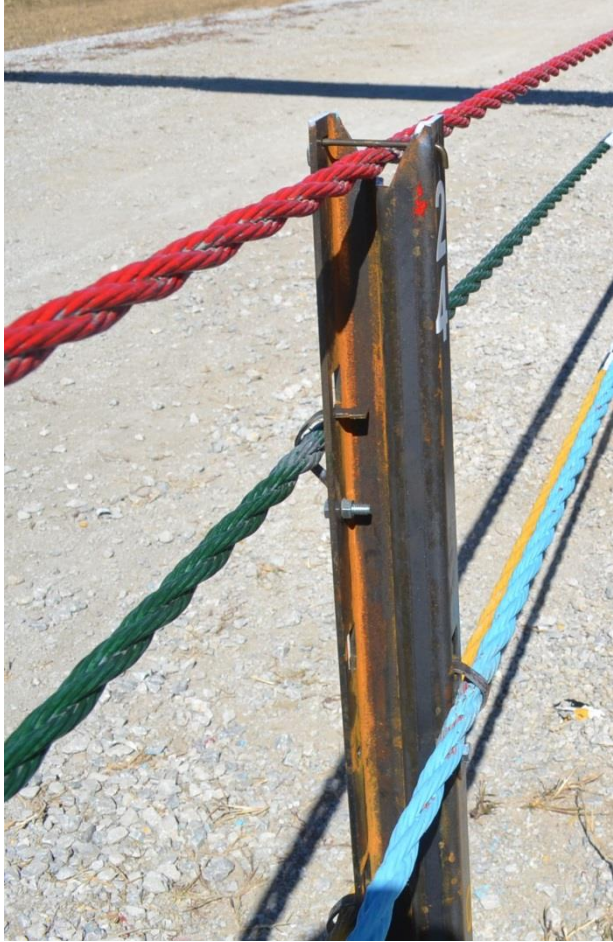


Figure 39. Test Installation Photographs, Test No. MWP-4

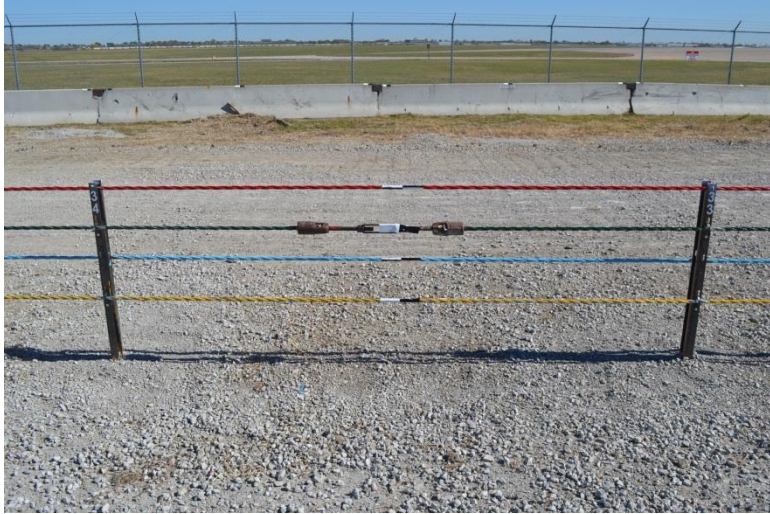
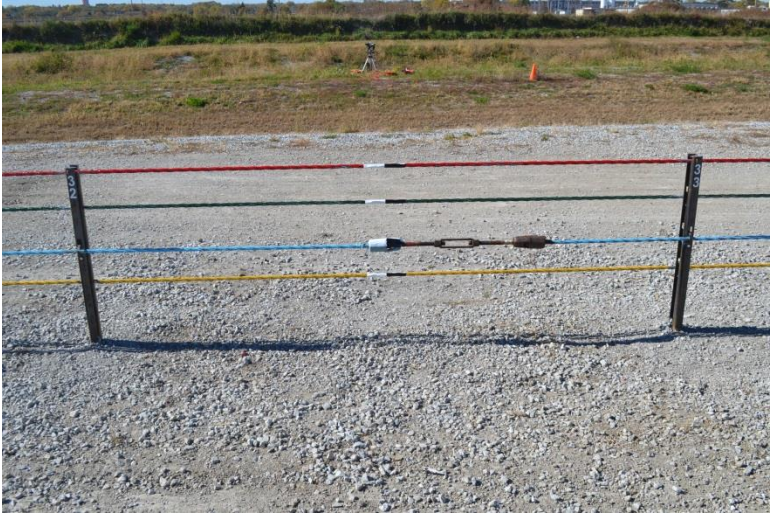


Figure 40. Test Installation Photographs, Test No. MWP-4



Figure 41. Test Installation Photographs, Test No. MWP-4

5 FULL SCALE CRASH TEST NO. MWP-4

5.1 Static Soil Test

Before full-scale crash test no. MWP-4 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The static test results, as shown in Appendix C, demonstrated a soil resistance above the baseline test limits. Thus, the soil provided adequate strength, and full-scale crash testing could be conducted on the barrier system.

5.2 Weather Conditions

Test no. MWP-4 was conducted on October 20, 2014 at approximately 2:30 p.m. The weather conditions, as per the National Oceanic and Atmospheric Administration (station 14939/LNK), were reported and are shown in Table 4.

Table 4. Weather Conditions, Test No. MWP-4

Temperature	74°F
Humidity	26%
Wind Speed	6 mph
Wind Direction	10° West of True North
Sky Conditions	Sunny
Visibility	6 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0 in.
Previous 7-Day Precipitation	0 in.

5.3 Test No. MWP-4

The 5,131-lb (2,327-kg) pickup truck impacted the high-tension, four-cable median barrier at a speed of 60.8 mph (97.8 km/h) and an angle of 26.1 degrees. A summary of the test results and sequential photographs are shown in Figure 42. Additional sequential photographs are shown in Figures 43 through 45. Documentary photographs of the crash test are shown in Figure 46.

5.4 Test Description

Initial vehicle impact was to occur 1 ft (0.3 m) upstream from post no. 25, as shown in Figure 47, which was selected according to proposed MASH updates. The actual point of impact was approximately 1.9 in. (48 mm) upstream from the target impact point. A sequential description of the impact events is contained in Table 5. The vehicle came to rest 144 ft - 10 in. (44.1 m) downstream from the point of impact, between post nos. 38 and 39. The vehicle trajectory and final position are shown in Figures 42 and 48.

Table 5. Sequential Description of Impact Events, Test No. MWP-4

TIME (sec)	EVENT
0.000	Vehicle left-front bumper contacted cable no. 2 upstream of post no. 25, and post no. 25 began to deflect backward.
0.004	Vehicle left-front bumper contacted post no. 25, and post no. 25 began to deflect downstream and bend backward.
0.010	Vehicle left headlight contacted cable no. 4 upstream of post no. 25, and vehicle left fender began to deform.
0.014	Vehicle left headlight contacted post no. 25.
0.022	Vehicle left-front tire contacted post no. 25.
0.024	Post no. 24 began to deflect backward.
0.026	Vehicle left fender contacted post no. 25 and cable no. 4, vehicle left headlight was shattered, and vehicle left-front tire began to override post no. 25.
0.028	Post no. 23 began to deflect backward.
0.030	Post no. 26 began to deflect backward.
0.036	Cable no. 4 detached from post no. 25.
0.038	Cable no. 3 detached from post no. 25.
0.040	Cable no. 2 detached from post no. 25.
0.046	Vehicle began to roll away from barrier, and post no. 24 began to twist downstream.
0.052	Post no. 27 began to deflect backward.
0.056	Vehicle grill began to deform.
0.068	Vehicle left-front tire overrode cable no. 1.
0.074	Post no. 22 began to deflect backward.
0.076	Vehicle left-front tire overrode post no. 25.
0.080	Cable no. 4 detached from post no. 26.
0.086	Cable no. 2 detached from post no. 26.
0.096	Vehicle left-front tire overrode cable no. 3, and post no. 28 began to deflect backward.
0.108	Cable no. 4 detached from post no. 27.

0.110	Cable no. 2 detached from post no. 27.
0.114	Vehicle began to yaw away from barrier, and the left-front tire ruptured.
0.124	Cable no. 2 detached from post no. 24.
0.128	Cable no. 4 detached from post no. 24.
0.136	Post no. 29 began to deflect backward.
0.140	Vehicle left-front bumper contacted post no. 26, and post no. 26 began to bend downstream.
0.156	Cable no. 2 detached from post no. 28.
0.164	Post no. 29 began to rotate backward, and cable no. 4 detached from post no. 28.
0.168	Cable no. 4 detached from post no. 23.
0.170	Cable no. 2 detached from post no. 29.
0.174	Post no. 30 began to deflect backward.
0.186	Vehicle left-rear tire overrode post no. 25 and became airborne.
0.192	Post no. 30 began to bend backward, and cable no. 4 detached from post no. 29.
0.210	Post no. 31 began to deflect backward, and cable no. 1 detached from post no. 27.
0.218	Vehicle left-rear tire overrode cable nos. 1 and 3.
0.222	Vehicle right-front tire overrode cable no. 1.
0.226	Cable no. 4 detached from post no. 31.
0.230	Vehicle right-front bumper contacted post no. 27, and post no. 27 began to bend downstream.
0.242	Vehicle began to roll toward the barrier.
0.252	Post no. 32 began to deflect backward.
0.258	Cable no. 4 detached from post no. 31.
0.268	Vehicle right-front tire overrode cable no. 3.
0.276	Cable no. 4 detached from post no. 32.
0.284	Post no. 33 began to deflect backward.
0.300	Cable no. 4 detached from post no. 33.
0.318	Post no. 34 began to bend backward.
0.328	Cable no. 4 detached from post no. 22.
0.330	Cable no. 4 detached from post no. 34.
0.342	Vehicle left-rear tire regained contact with ground.
0.374	Vehicle right-rear tire overrode cable no. 1, and cable no. 4 detached from post no. 21.
0.388	Post no. 35 began to bend backward.
0.394	Vehicle right-rear tire contacted post no. 27.
0.404	Post no. 36 began to bend backward.
0.414	Cable no. 4 detached from post no. 35.
0.422	Vehicle right-rear tire became airborne.
0.470	Vehicle was parallel to system.
0.516	Vehicle right-front tire became airborne.
0.560	Vehicle left-front tire overrode cable no. 2.
0.580	Cable no. 4 detached from post no. 20.
0.594	Vehicle began to yaw toward barrier.
0.662	Cable no. 4 detached from post no. 19.
0.704	Vehicle left-rear tire overrode cable no. 2.

0.912	Cable no. 4 detached from post no. 18.
0.914	Cable no. 1 detached from post no. 24.
1.038	Vehicle right-front tire regained contact with ground.
1.102	Vehicle right-rear tire regained contact with ground.
1.130	Vehicle right quarter panel contacted post no. 32 and began to deform, and cable no. 4 detached from post no. 36.
1.160	Vehicle right-front tire ruptured.
1.210	Vehicle was yawing away from barrier.
1.900	Vehicle right-front bumper impacted post no. 36, causing it to bend downstream.
2.092	Vehicle right-front bumper impacted post no. 37, causing it to bend downstream.
2.403	Vehicle right-front bumper impacted post no. 38, causing it to bend downstream.
2.815	Vehicle right-front bumper impacted post no. 39, causing it to bend downstream.
3.310	Vehicle came to rest 144-ft 10-in. (44.1 m) downstream from impact with right-front tire on top of a bent over post no. 39.

5.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 49 through 59. Barrier damage consisted of bent posts, disengaged cables, and deformed brackets. At its final resting position, the vehicle was still in contact with the cables. Cable nos. 1 and 2 were beneath the vehicle, cable no. 4 was on the impact side of the vehicle, and cable no. 3 was on the non-impact side of the vehicle.

Cable no. 4 disengaged from post nos. 18 through 40 due to fracture of the brass keeper rods. Cable no. 3 disengaged from post nos. 25, 27, 32 and 33, as well as post nos. 36 through 39. Cable no. 2 disengaged from post nos. 15 through 40. Cable no. 1 disengaged from post nos. 24, 26, 29, and post nos. 36 through 39. Nearly all of the releases of cable nos. 1 through 3 were due to the tabs rotating through the key to release the cables vertically. However, the release of cable no. 2 at post no. 37 was due to bracket fracture at the tab. Displacement of the cable splices were documented, but they were deemed small. The maximum displacement within a splice measured ½ in. (13 mm) at the load cell splice found in cable no. 4.

Post nos. 17 through 40 deformed in bending and twisting. The posts typically twisted upstream and bent backward. Post nos. 25 through 27 and 36 through 39 exhibited the greatest

deformations, with post nos. 36 through 39 partially or fully bent to the ground line due to vehicle override. Post no. 2 was bent slightly downstream from forces on the anchor.

The maximum dynamic barrier deflection of the system was 200 in. (5,080 mm) near post no. 28, and the working width of the system was 201.3 in. (5,113 mm), as determined from high-speed video analysis. The upstream anchor was displaced ¼ in. (6 mm) downstream. The downstream anchor did not show signs of displacement.

5.6 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 60 and 61. The maximum occupant compartment deformations are listed in Table 6 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH-established deformation limits were violated. Complete occupant compartment and vehicle deformations as well as the corresponding locations are provided in Appendix D.

Table 6. Maximum Occupant Compartment Deformations by Location, Test No. MWP-4

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	¼ (6)	≤9 (229)
Floor Pan & Transmission Tunnel	¼ (6)	≤12 (305)
Side Front Panel (in Front of A-Pillar)	¼ (6)	≤12 (305)
Side Door (Above Seat)	¼ (6)	≤12 (305)
Side Door (Below Seat)	1 (25)	≤9 (229)
Roof	0 (0)	≤12 (305)

The majority of the vehicle damage was concentrated on the left-front corner and left side of the vehicle where impact occurred. The left-front bumper was partially disengaged. The left fender and left-front bumper separated by 2½ in. (64 mm). The left fender was crushed 3½ in. (89 mm) inward between the left headlight and wheel well. There was a 7-in. (178-mm) buckle

at the top of the left wheel well. There was a 1-in. (25-mm) separation between the left fender and the hood. The left-front door separated in the front by 2½ in. (64 mm), along the top by ¾ in. (19 mm), and along the bottom of the door by 1 in. (25 mm). The left-front door also overlapped the left-rear door. Both the left headlight and fog-light disengaged. There was a 5½-in. (140-mm) buckle at the bottom rear of the left-rear wheel well. The left-rear bumper separated 1½ in. (38 mm) from the left quarter panel, and the left taillight separated ¾ in. (19 mm) from the quarter panel. There was a gap of ½ in. (13 mm) between the left-front door and fender. The right headlight was shattered but remained attached. There was a 5-in. (127-mm) deep crush at the front of the right-front wheel well, in the fender. The right-front tire was deflated.

There were contact marks from cables along both the left and right sides of the vehicle. There were sheet metal tears of varying lengths on the back of the right-rear wheel well, the right-rear tire rim, the right-front bumper, the left-rear bumper, the left fender along the back of the left-front wheel well, and the left-front door. There were several cuts in the right quarter panel. Dents occurred at the wheel wells, tire rims, front bumper, and left-front door and quarter panel. Gouging occurred on both rear wheel wells and tire rims, as well as the left-front tire rim. Kinking occurred along the bottom of the left-front door, the right-rear wheel well, and the rear bumper.

5.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 7. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 7. The results of the occupant risk analysis, as determined from the accelerometer data, are also summarized in Figure 42. The

recorded data from the accelerometers and the rate transducers are shown graphically in Appendix E.

Table 7. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MWP-4

Evaluation Criteria		Transducer		MASH Limits
		DTS (primary)	SLICE 2	
OIV ft/s (m/s)	Longitudinal	-9.38 (-2.86)	-9.12 (-2.78)	≤ 40 (12.2)
	Lateral	8.37 (2.55)	8.66 (2.64)	≤ 40 (12.2)
ORA g's	Longitudinal	-8.78	-8.96	≤ 20.49
	Lateral	-5.33	4.99	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	-14.69	-14.94	≤ 75
	Pitch	-4.04	-4.13	≤ 75
	Yaw	41.57	41.34	not required
THIV ft/s (m/s)		11.81 (3.60)	12.24 (3.73)	not required
PHD g's		9.29	9.52	not required
ASI		0.43	0.40	not required

5.8 Load Cells and String Potentiometers

The pertinent data from the load cells and string potentiometer were extracted from the bulk signal and analyzed using the transducers' calibration factors. The maximum displacement of the upstream anchor was recorded as 0.73 in. (19 mm), while a summary of the maximum cable loads can be found in Table 8. The recorded data and analyzed results are detailed in Appendix F. The exact moment of impact could not be determined from the transducer data, as impact may have occurred prior to observing a measurable signal in the electronic data. Thus, the

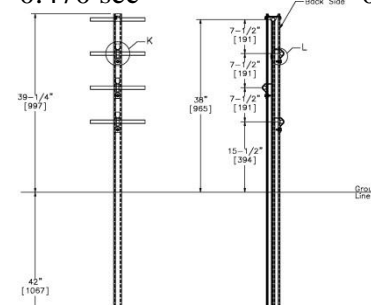
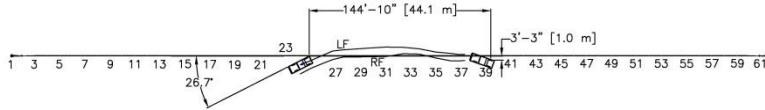
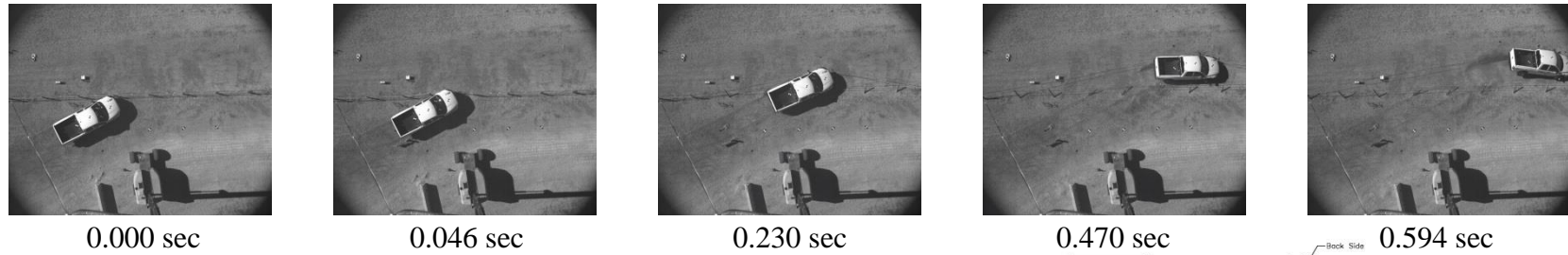
extracted data curves should not be taken as a precise time after impact, but rather a general timeline between events within the data curve itself.

Table 8. Maximum Cable Loads, Test No. MWP-4

Cable Location	Sensor Location	Maximum Cable Load		Time (sec)
		kips	kN	
Combined Cable Load	Upstream of Impact	39.35	175.04	0.5187
Cable No. 4	Upstream of Impact	18.19	80.91	0.7970
Cable No. 3	Upstream of Impact	7.99	35.54	0.0604
Cable No. 2	Upstream of Impact	18.42	81.94	0.5290
Cable No. 1	Upstream of Impact	5.13	22.82	0.0518

5.9 Discussion

The analysis of the test results for test no. MWP-4 showed that the high-tension four-cable median barrier adequately contained and redirected the 2270P, with controlled lateral displacements of the barrier. There were no detached elements or fragments which showed potential for penetrating the occupant compartment or which presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate or ride over the barrier, and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix E, were deemed acceptable because they did not adversely influence occupant risk safety criteria or cause rollover. After impact, the vehicle was captured and retained within the system, so there was no exit information. Therefore, test no. MWP-4, conducted on the four-cable high-tension median barrier system, was determined to be acceptable according to the MASH safety performance criteria for test designation no. 3-11.



- Test AgencyMwRSF
- Test Number..... MWP-4
- Date 10/20/14
- MASH Test Designation 3-11
- Test Article..... Four Cable Median Barrier
- Total Length 604 ft (184.1 m)
- Key Component - Cable
 - Size 3x7, 3/4-in. (19-mm) diameter
 - Cable Heights 15 1/2, 23, 30 1/2, 38 in. (394 mm, 584 mm, 775 mm, 965 mm)
- Key Component - MWP
 - Dimensions 3 x 1 1/4 x 83 in. (76 x 44 x 2,108 mm)
 - Spacing 10 ft (3.05 m)
- Soil Type Compacted, coarse, crushed limestone
- Vehicle Make /Model..... 2008 Dodge Ram
 - Curb 5,140 lb (2,331 kg)
 - Test Inertial..... 4,967 lb (2,253 kg)
 - Gross Static..... 5,131 lb (2,327 kg)
- Impact Conditions
 - Speed 60.8 mph (97.8 km/h)
 - Angle 26.1 deg
 - Impact Location..... 13.9 in. (0.35 m) upstream of Post no. 25
- Impact Severity (IS) 118.6 kip-ft (160.8 kJ) > 106 kip-ft (143.7 kJ)
- Exit Conditions
 - Speed NA
 - Angle NA
- Exit Box Criterion NA (Did not exit system)
- Vehicle Stability..... Satisfactory
- Vehicle Stopping Distance 144 ft - 10 in. (44.1 m)
- Vehicle Damage..... Moderate
 - VDS [8] 11-LFQ-4
 - CDC [9] 11-LYEN-3
 - Maximum Interior Deformation 1 in. (25 mm)

- Test Article Damage Moderate
- Maximum Test Article Deflections
 - Permanent Set 57 in. (1,448 mm)
 - Dynamic 200 in. (5,080 mm)
 - Working Width..... 201.3 in. (5,113 mm)
- Transducer Data

Evaluation Criteria		Transducer		MASH Limit
		DTS (primary)	SLICE-2	
OIV ft/s (m/s)	Longitudinal	-9.38 (-2.86)	-9.12 (-2.78)	≤ 40 (12.2)
	Lateral	8.37 (2.55)	8.66 (2.64)	≤ 40 (12.2)
ORA g's	Longitudinal	-8.78	-8.96	≤ 20.49
	Lateral	-5.33	4.99	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	-14.69	-14.94	≤ 75
	Pitch	-4.04	-4.13	≤ 75
	Yaw	41.57	41.34	not required
THIV – ft/s (m/s)		11.81 (3.60)	12.24 (3.73)	not required
PHD – g's		9.29	9.52	not required
ASI		0.43	0.40	not required

Figure 42. Summary of Test Results and Sequential Photographs, Test No. MWP-4



0.000 sec



0.020 sec



0.040 sec



0.092 sec



0.124 sec



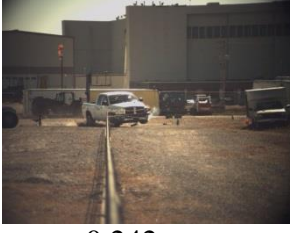
0.192 sec



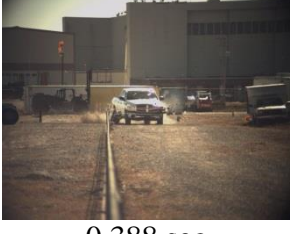
0.000 sec



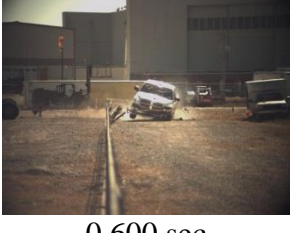
0.114 sec



0.242 sec



0.388 sec



0.600 sec



1.038 sec

Figure 43. Additional Sequential Photographs, Test No. MWP-4



0.000 sec



0.078 sec



0.156 sec



0.242 sec



0.422 sec



0.576 sec



0.000 sec



0.036 sec



0.080 sec



0.114 sec



0.198 sec



0.242 sec

Figure 44. Additional Sequential Photographs, Test No. MWP-4

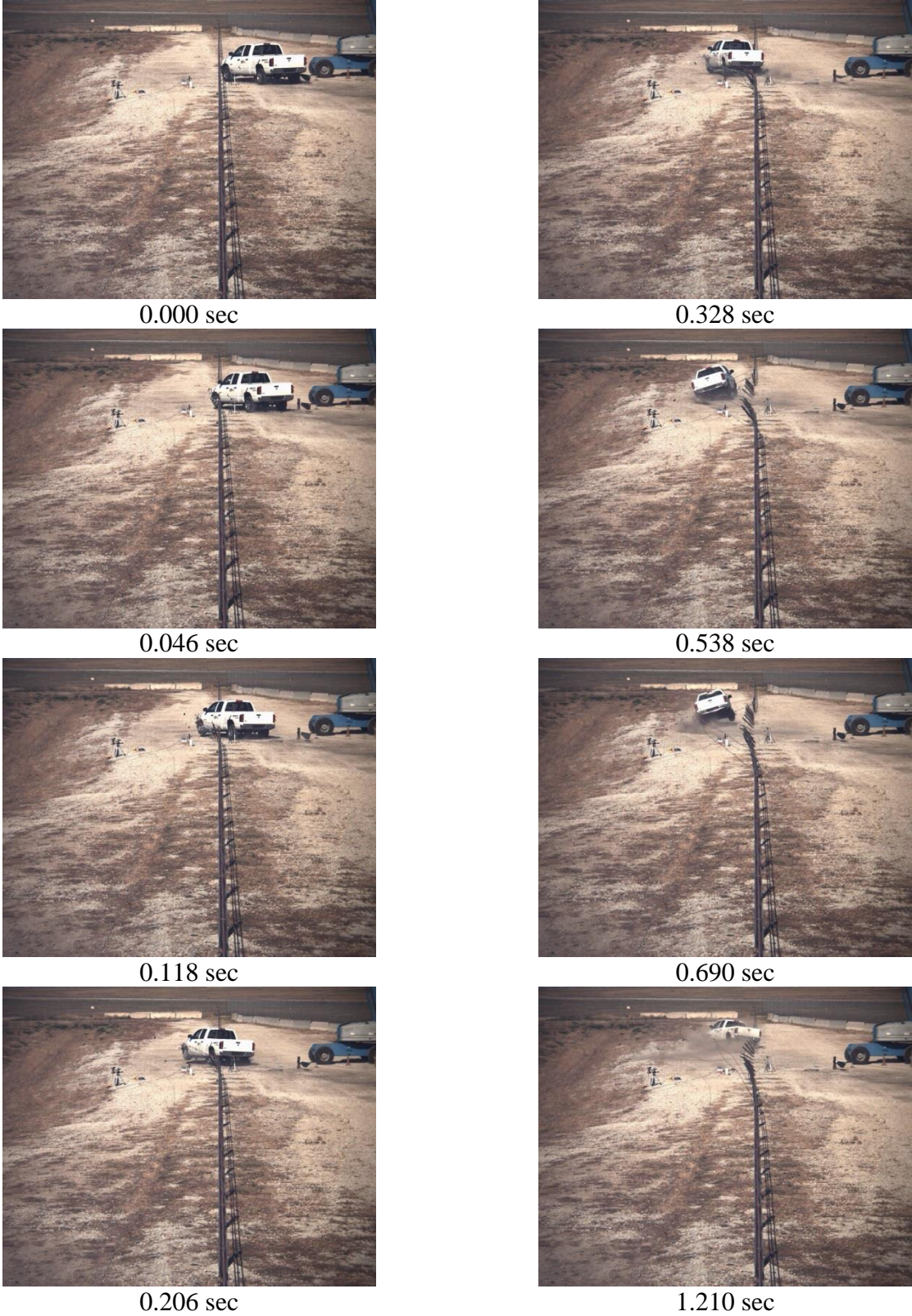


Figure 45. Additional Sequential Photographs, Test No. MWP-4



Figure 46. Documentary Photographs, Test No. MWP-4



Figure 47. Impact Location, Test No. MWP-4



Figure 48. Vehicle Final Position and Trajectory, Test No. MWP-4



Figure 49. System Damage, Test No. MWP-4



Figure 50. System Damage, End Anchorages, Test No. MWP-4



Figure 51. System Damage, Cable Brackets, Test No. MWP-4

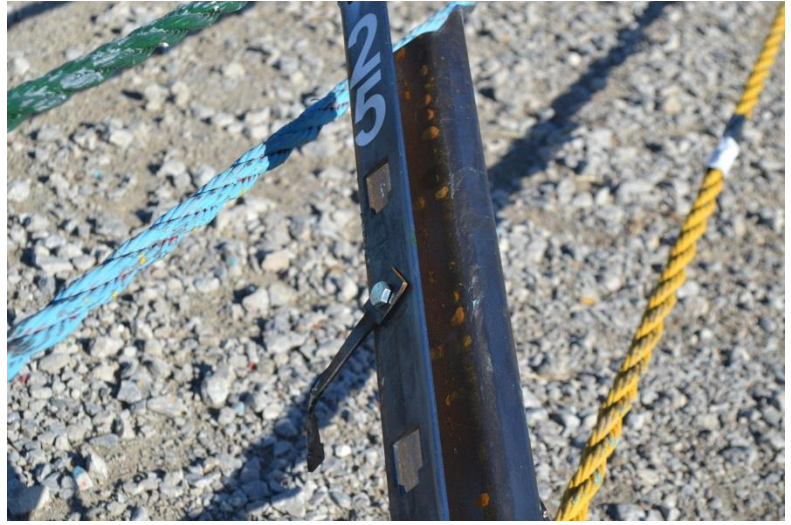
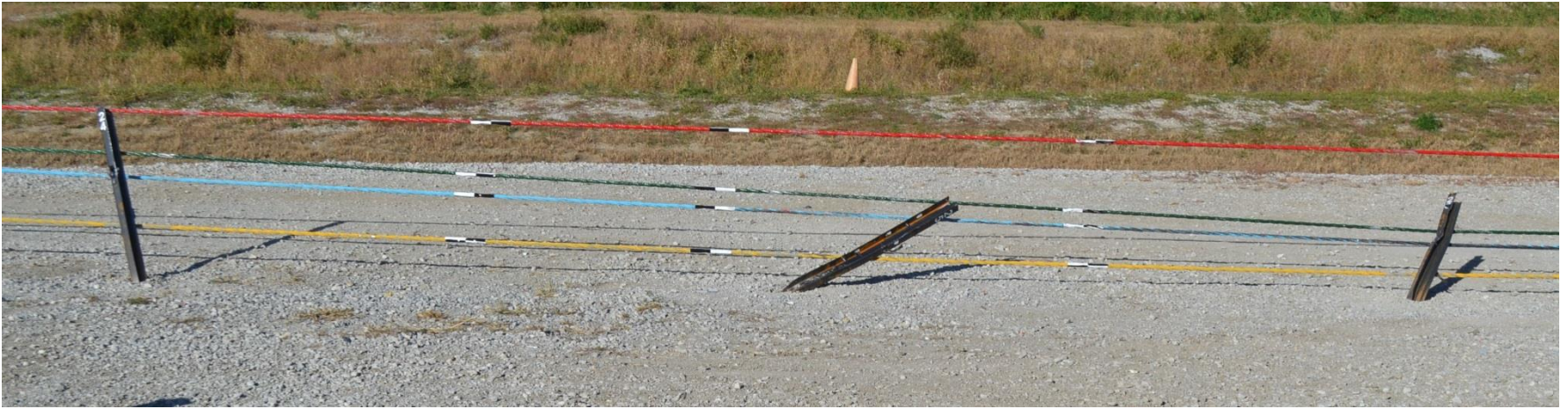


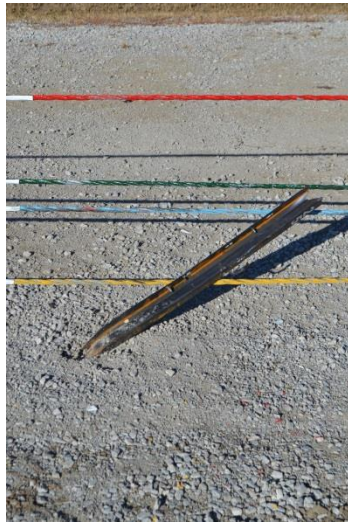
Figure 52. System Damage, Cable Brackets, Test No. MWP-4



Figure 53. System Damage, Brass Rods, Test No. MWP-4



Post No. 24



Post No. 25



Post No. 26

Figure 54. System Damage, Post Nos. 24 through 26, Test No. MWP-4



Post No. 27



Post No. 28



Post No. 29

Figure 55. System Damage, Post Nos. 27 through 29, Test No. MWP-4



Post No. 30



Post No. 31



Post No. 32

Figure 56. System Damage, Post Nos. 30 through 32, Test No. MWP-4



Post No. 33



Post No. 34



Post No. 35

Figure 57. System Damage, Post Nos. 33 through 35, Test No. MWP-4



Post No. 36



Post No. 37



Post No. 38

Figure 58. System Damage, Post Nos. 36 through 38, Test No. MWP-4



Post No. 39



Post No. 40



Post No. 41

Figure 59. System Damage, Post Nos. 39 through 41, Test No. MWP-4



Figure 60. Vehicle Damage, Test No. MWP-4



Figure 61. Vehicle Damage, Test No. MWP-4

6 DESIGN DETAILS TEST NO. MWP-6

The four-cable median barrier system used for test no. MWP-6 was nearly identical to that used in test no. MWP-4, as shown in Figures 62 through 85. The targeted impact location for test no. MWP-6 was 4 ft (1.2 m) upstream from post no. 32, as shown in Figure 62. The system was mirrored so that cable nos. 1 and 3 were on impact side and cable no. 2, the critical capture cable, was on the non-impact side of the barrier, as shown in Figure 76. MASH requires that cable barrier systems be tested with cable tensions set to the recommended tension at 100 degrees Fahrenheit. A cable tensioning chart was developed as a function of ambient air temperature for use when installing the barrier system, as shown in Table 3. Thus, the cables were tensioned to a pre-load of 2,500 lb (11.1 kN).

The typical post spacing was reduced to 8 ft (2.4 m), while the system length remained the same. This change resulted in an increased number of line posts, tallying to 72. The spacing between posts no. 68 and 69 was 12 ft (3.7 m), while the anchors remained in the same locations. The longitudinal location of the special 12-ft (3.7-m) post spacing was selected to occur outside of the vehicle contact region and away from the system anchorage. Cable splices were shifted downstream into the new impact region, between post nos. 36 and 41, as shown in Figure 63. The load cell locations were relocated to between post nos. 6 and 8. Details for the load cells, threaded rods, turnbuckles, end fittings, and rod couplers are provided in Figure 67. Photographs of the test installation are shown in Figures 86 to 89. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix A.

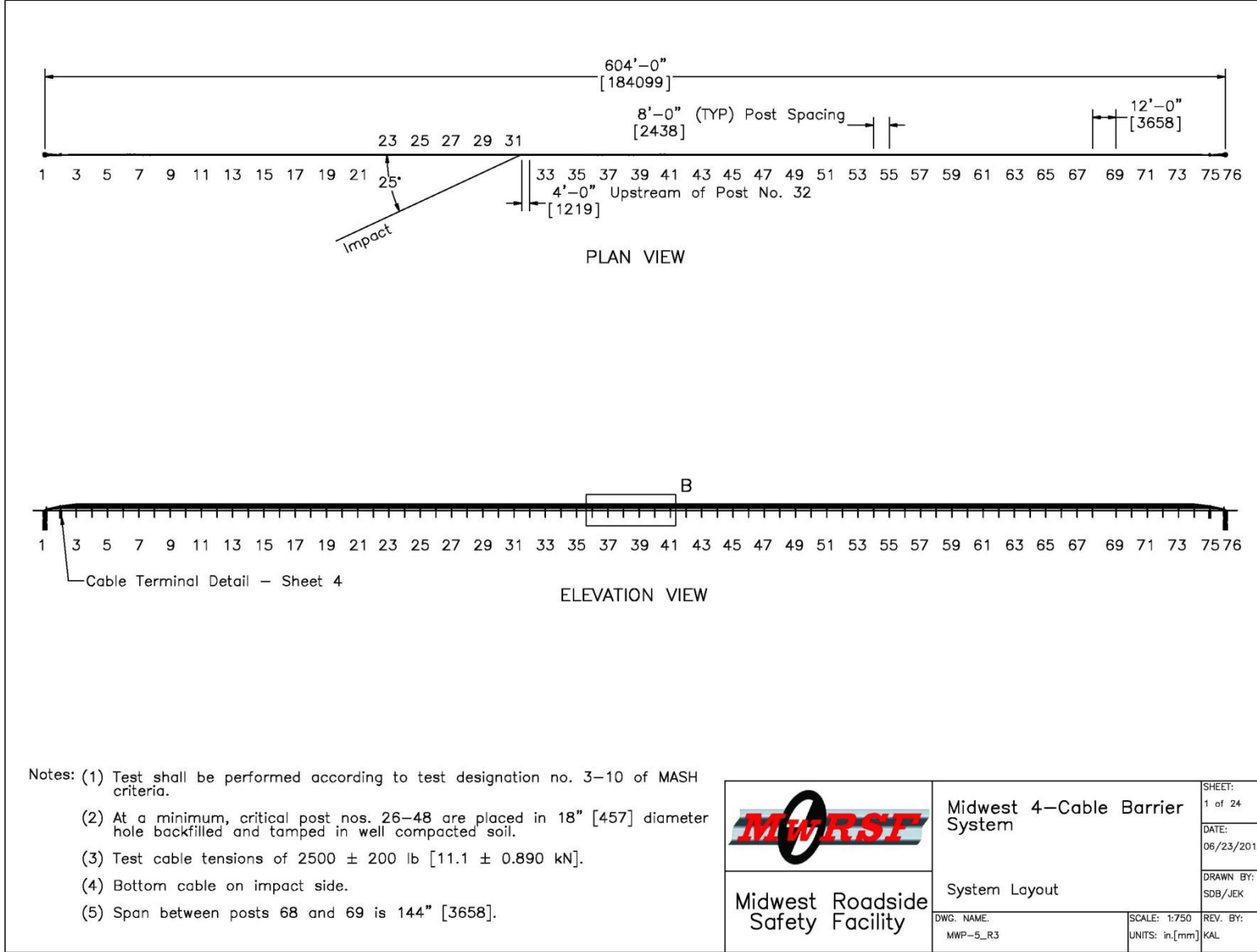


Figure 62. Test Installation Layout, Test No. MWP-6

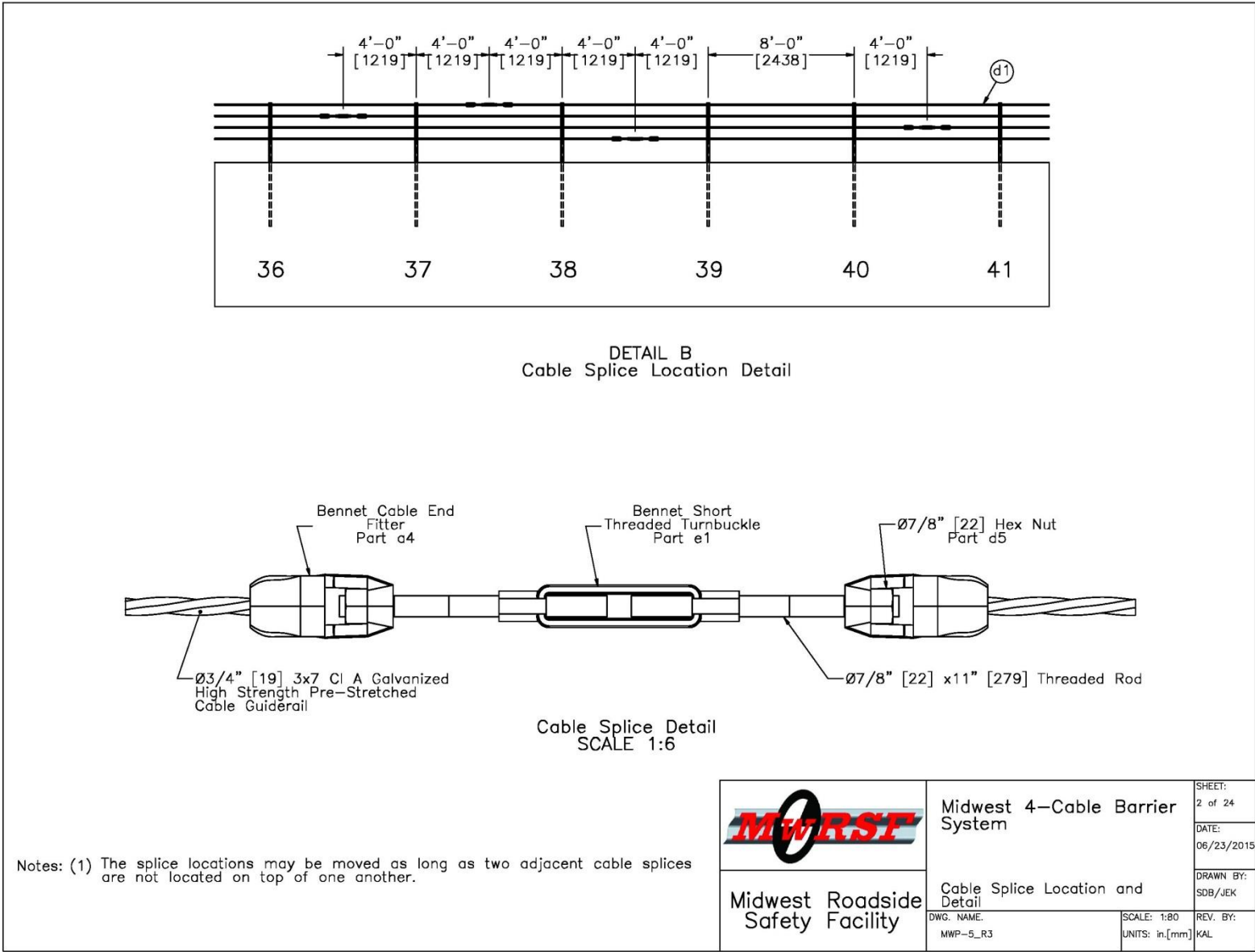


Figure 63. Cable Splice Location and Detail, Test No. MWP-6

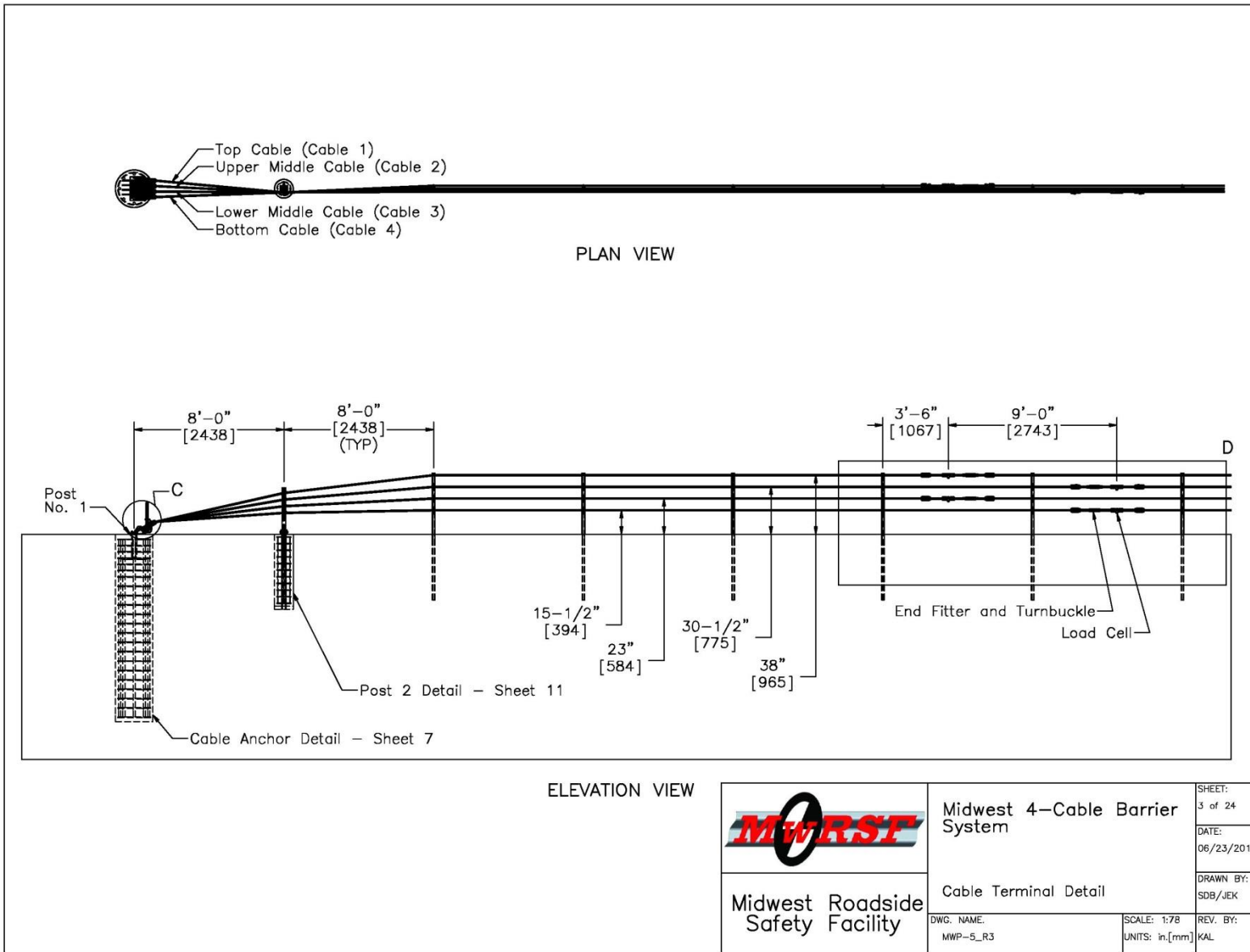


Figure 64. Cable Terminal Detail, Test No. MWP-6

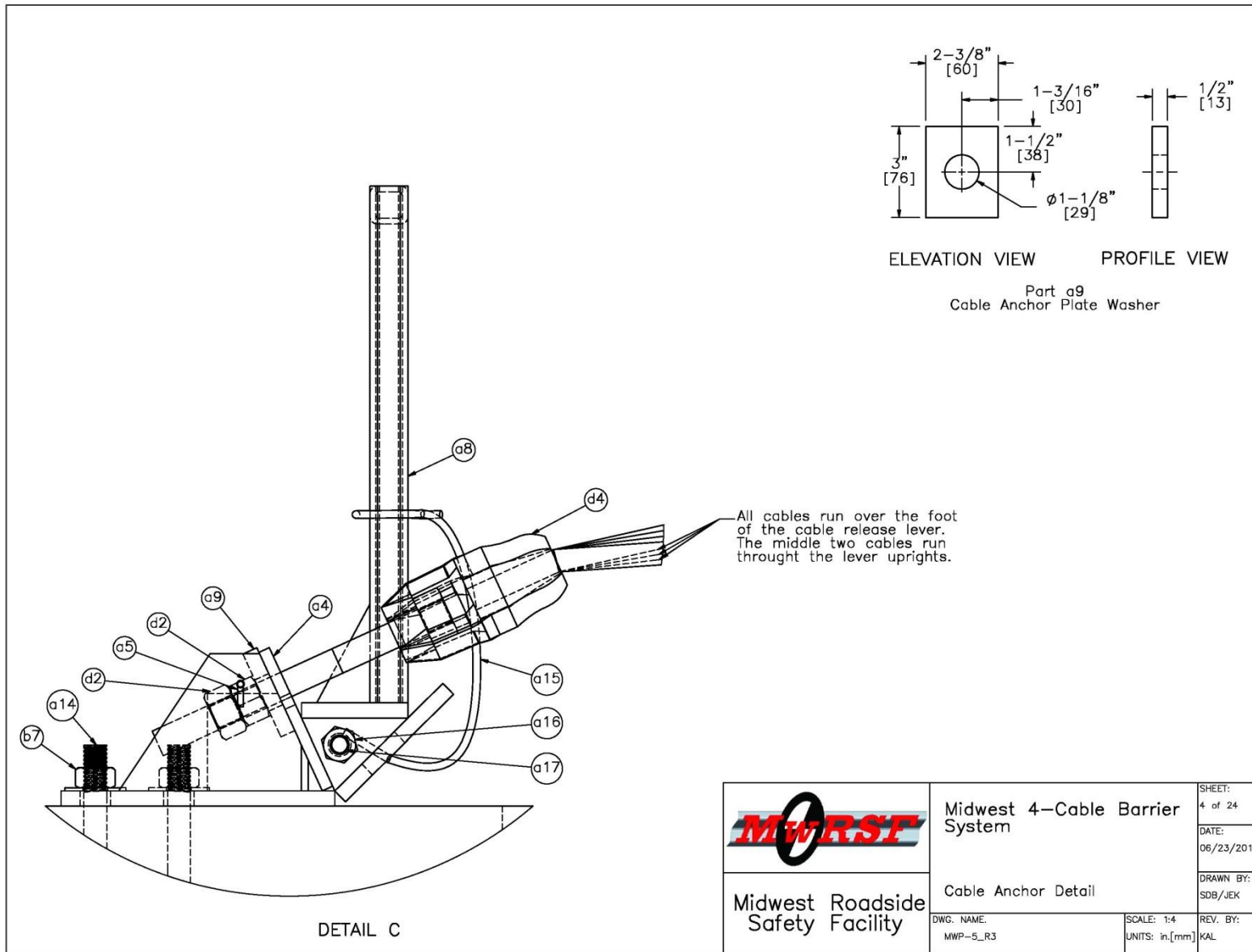



Figure 65. Cable Anchor Detail, Test No. MWP-6

	Midwest 4-Cable Barrier System	SHEET: 4 of 24
	Cable Anchor Detail	DATE: 06/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-5_R3	DRAWN BY: SDB/JEK
	SCALE: 1:4 UNITS: in, [mm]	REV. BY: KAL

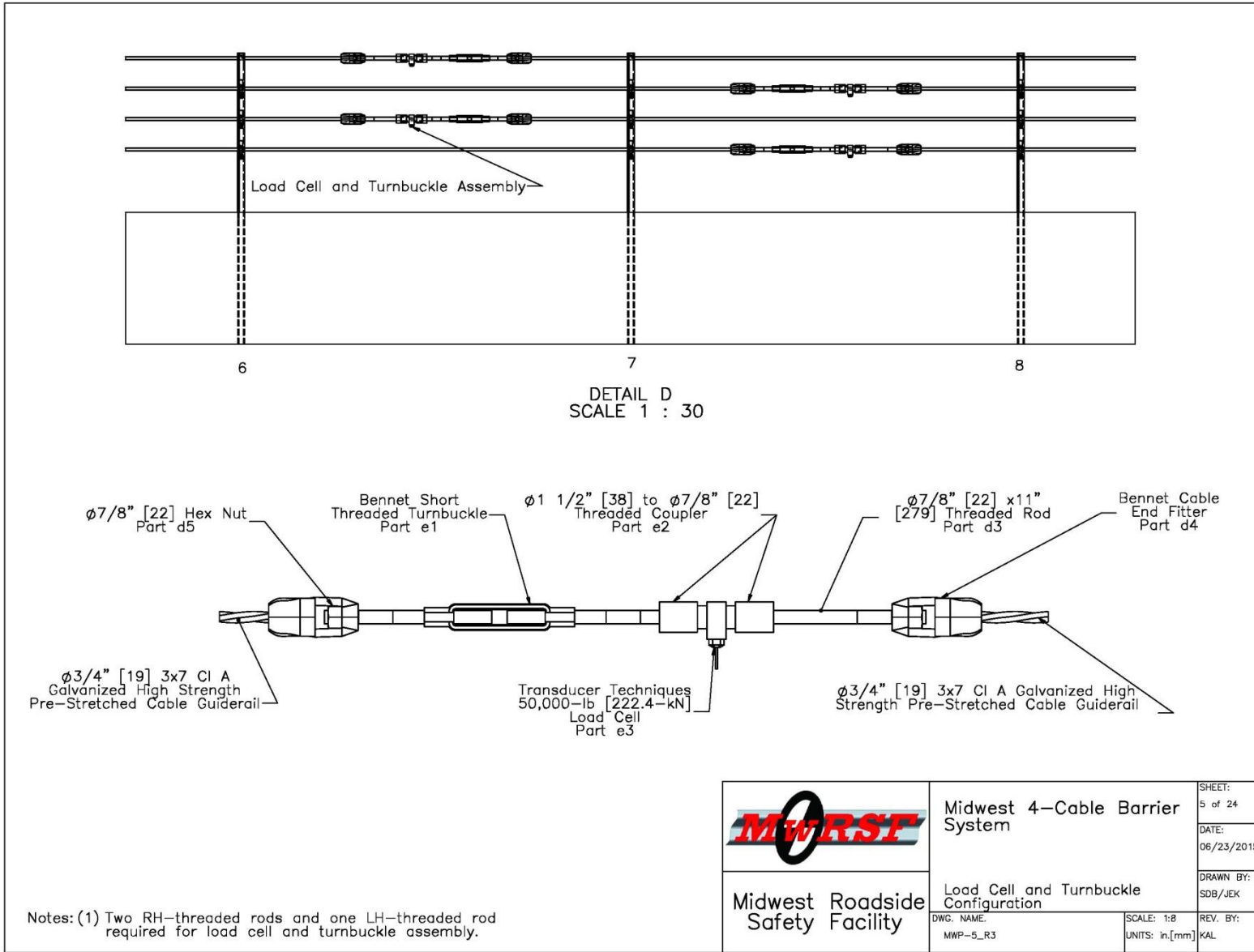


Figure 66. Load Cell and Turnbuckle Configuration, Test No. MWP-6

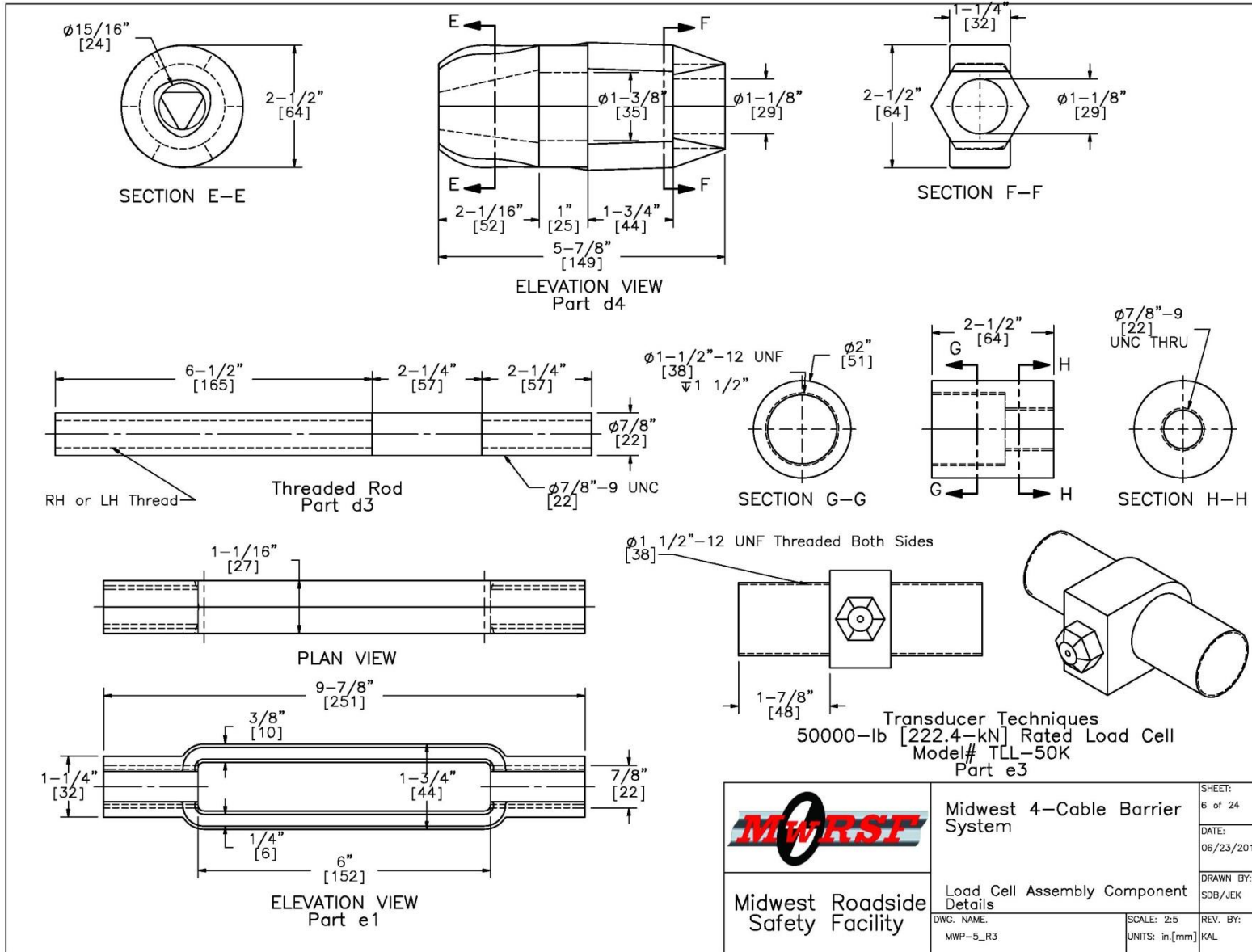


Figure 67. Load Cell Assembly Component Details, Test No. MWP-6

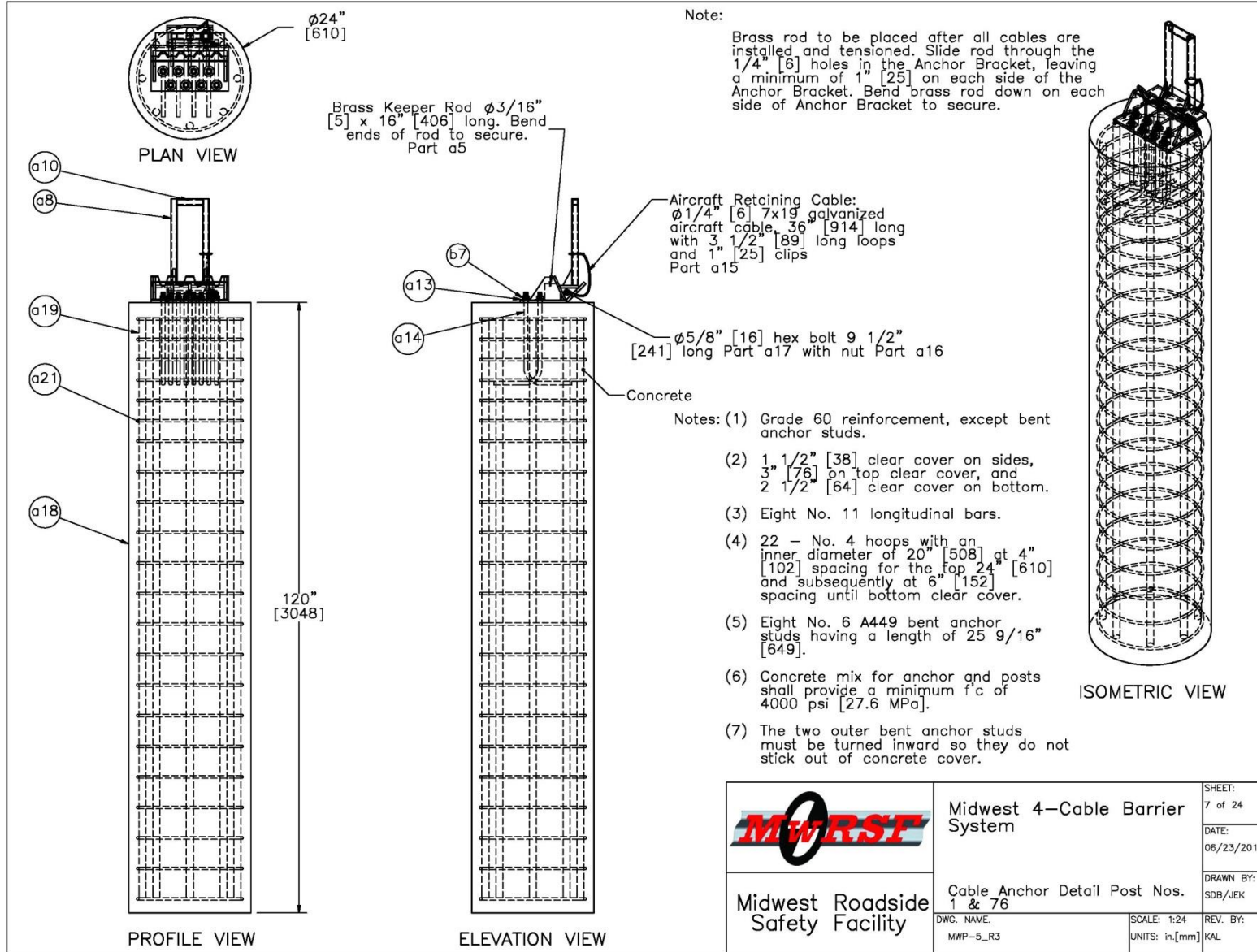


Figure 68. Cable Anchor Detail, Post Nos. 1 and 76, Test No. MWP-6

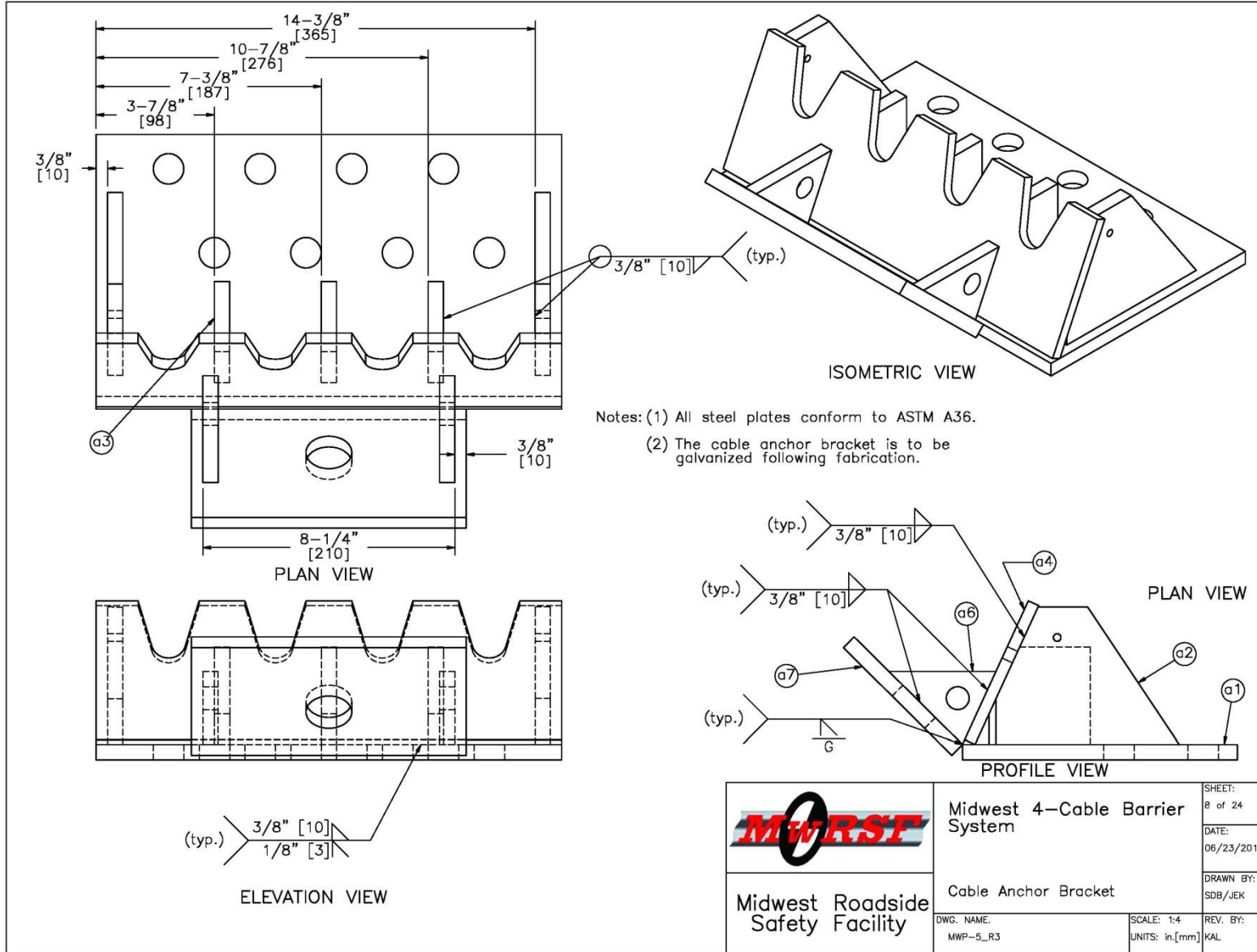


Figure 69. Cable Anchor Bracket, Test No. MWP-6

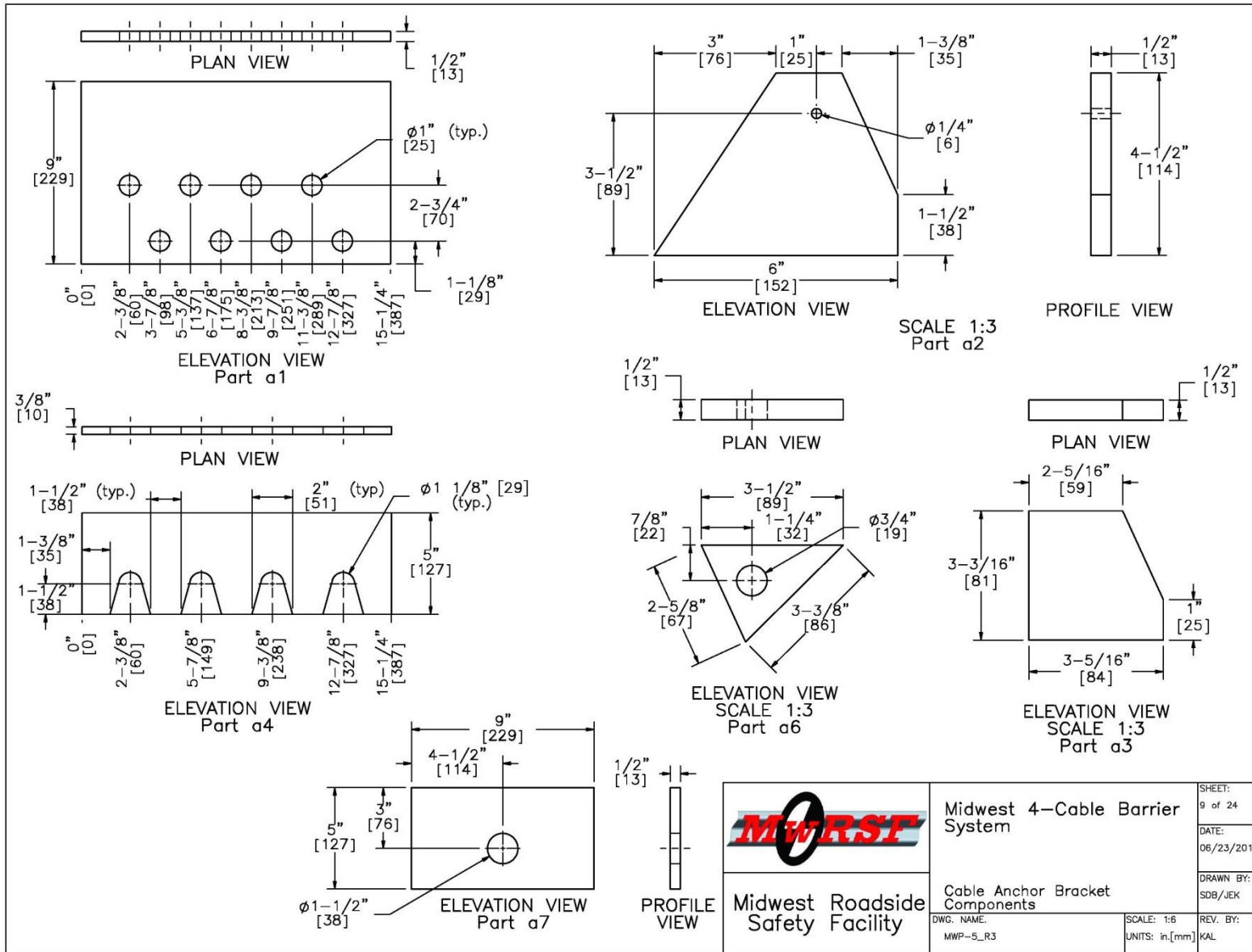



Figure 70. Cable Anchor Bracket Components, Test No. MWP-6

	Midwest 4-Cable Barrier System	SHEET: 9 of 24
	Cable Anchor Bracket Components	DATE: 06/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-5_R3	DRAWN BY: SDB/JEK
	SCALE: 1:6 UNITS: in,[mm]	REV. BY: KAL

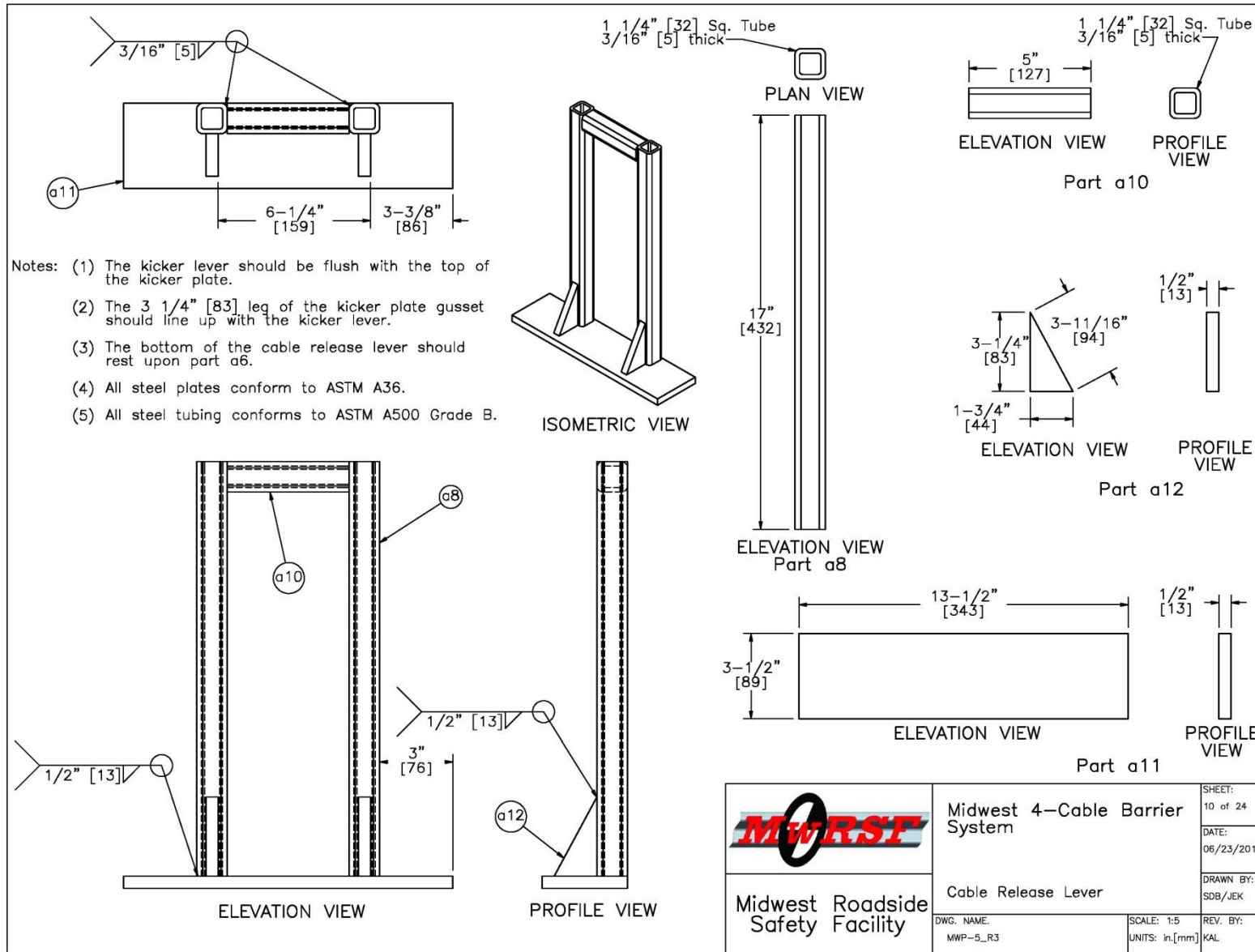



Figure 71. Cable Release Lever, Test No. MWP-6

 Midwest Roadside Safety Facility	Midwest 4-Cable Barrier System	SHEET: 10 of 24
	Cable Release Lever	DATE: 06/23/2015
DWG. NAME: MWP-5_R3	SCALE: 1:5 UNITS: in, [mm]	DRAWN BY: SDB/JEK
		REV. BY: KAL

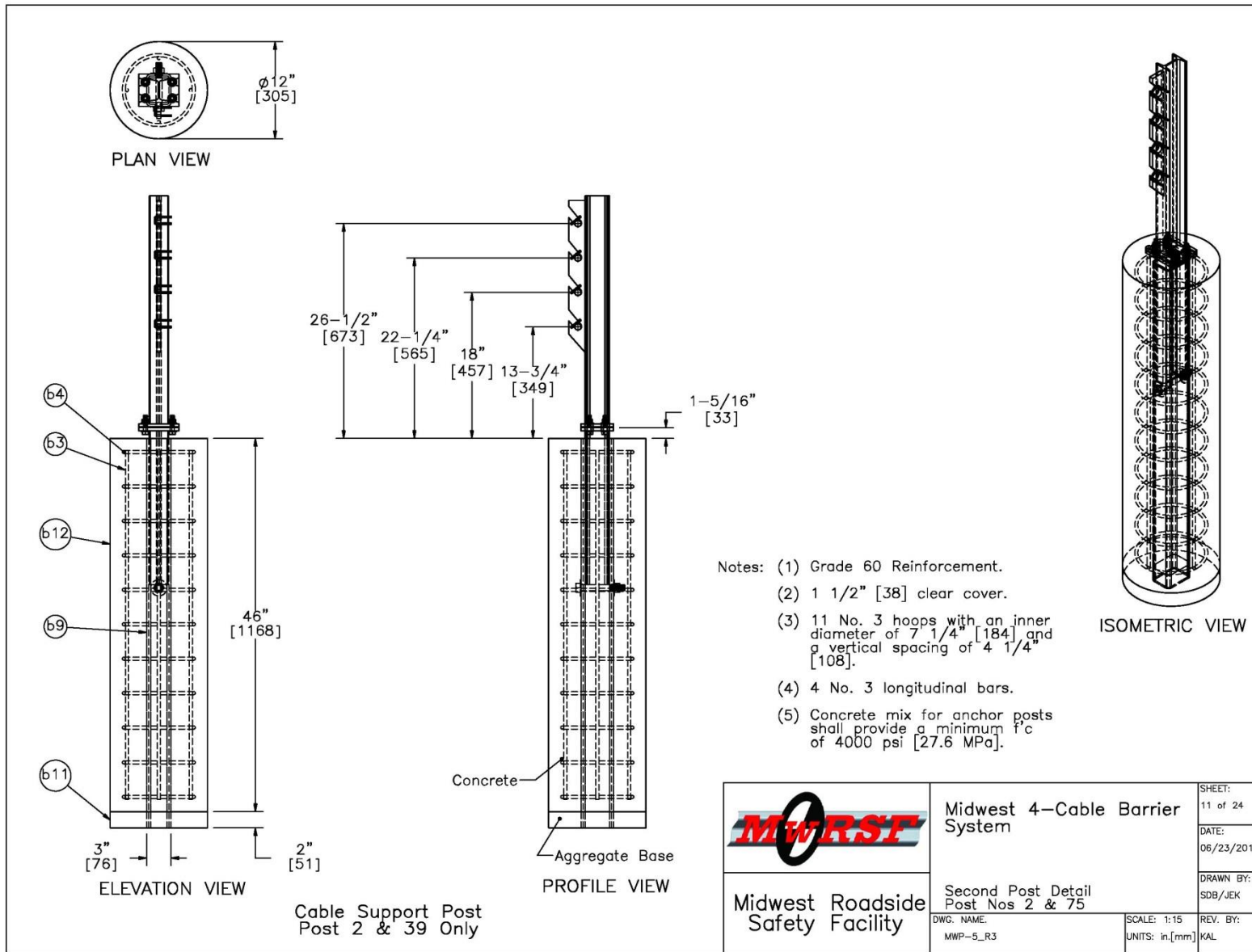


Figure 72. Second Post Details, Post Nos. 2 and 75, Test No. MWP-6

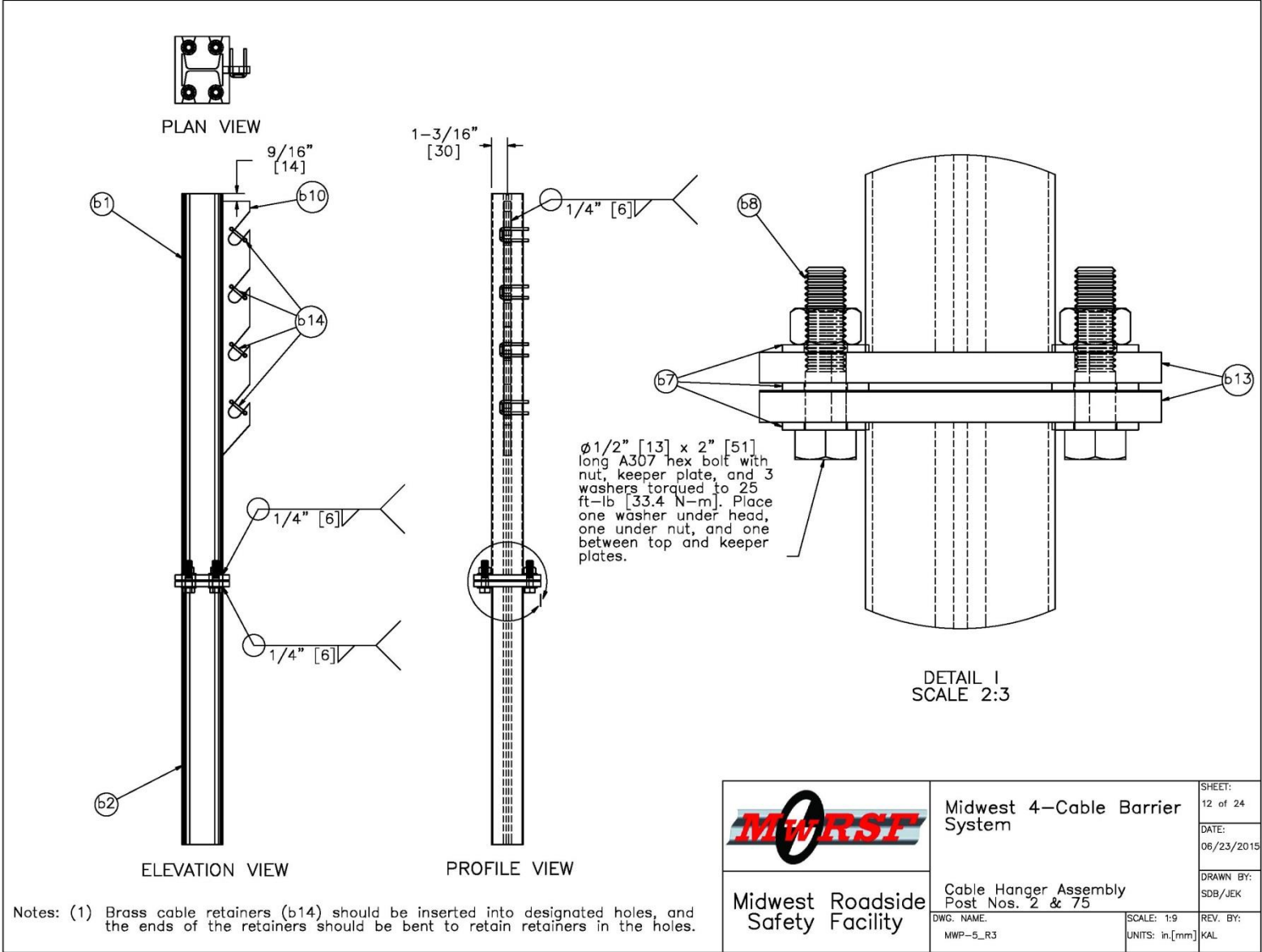


Figure 73. Cable Hanger Assembly, Post Nos. 2 and 75, Test No. MWP-6

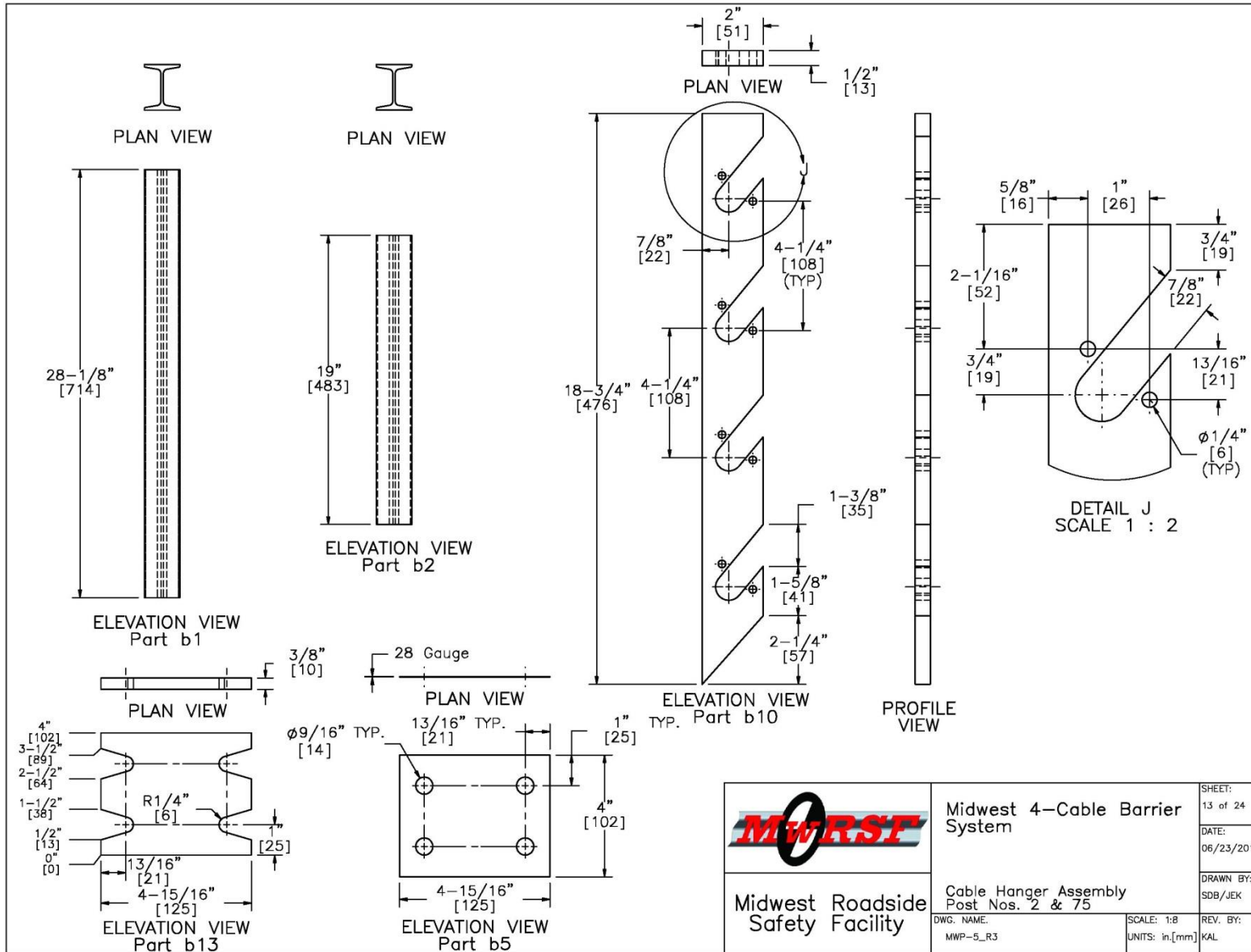


Figure 74. Cable Hanger Assembly, Post Nos. 2 and 75, Test No. MWP-6

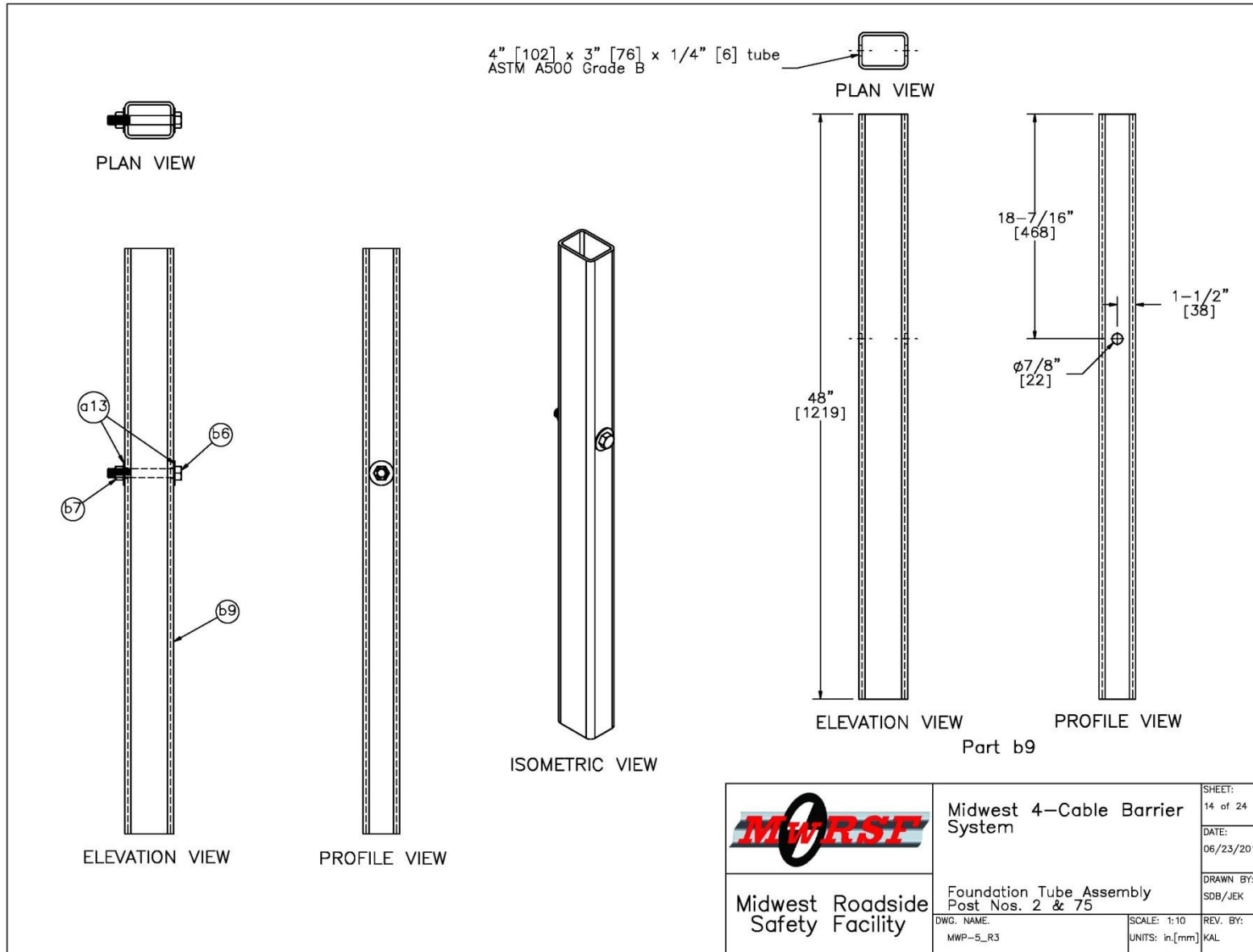
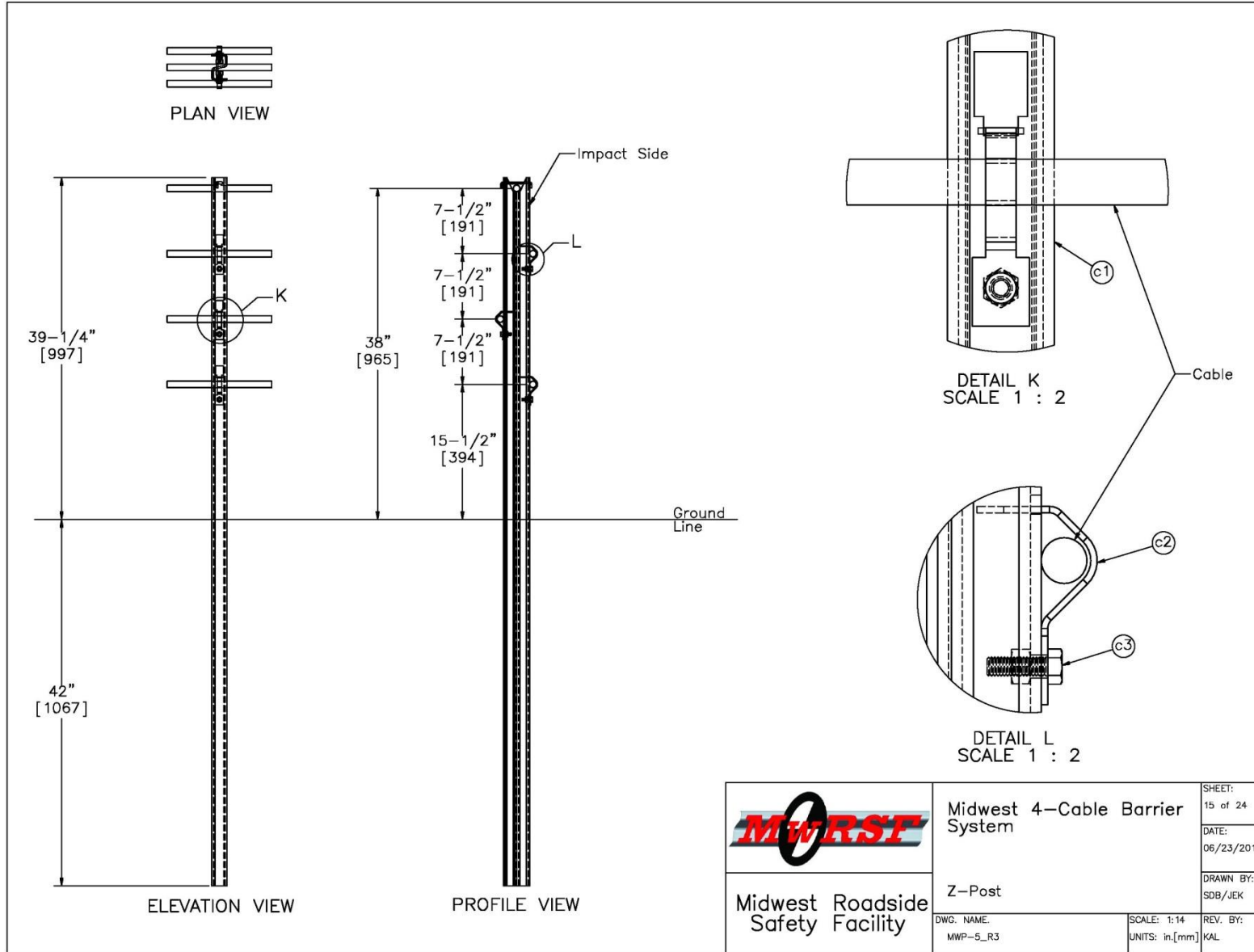


Figure 75. Foundation Tube Assembly, Post Nos. 2 and 75, Test No. MWP-6



	Midwest 4-Cable Barrier System		SHEET: 15 of 24
	Z-Post		DATE: 06/23/2015
Midwest Roadside Safety Facility			DRAWN BY: SDB/JEK
DWG. NAME: MWP-5_R3	SCALE: 1:14 UNITS: in, [mm]	REV. BY: KAL	

Figure 76. MWP Z-Post Details, Test No. MWP-6

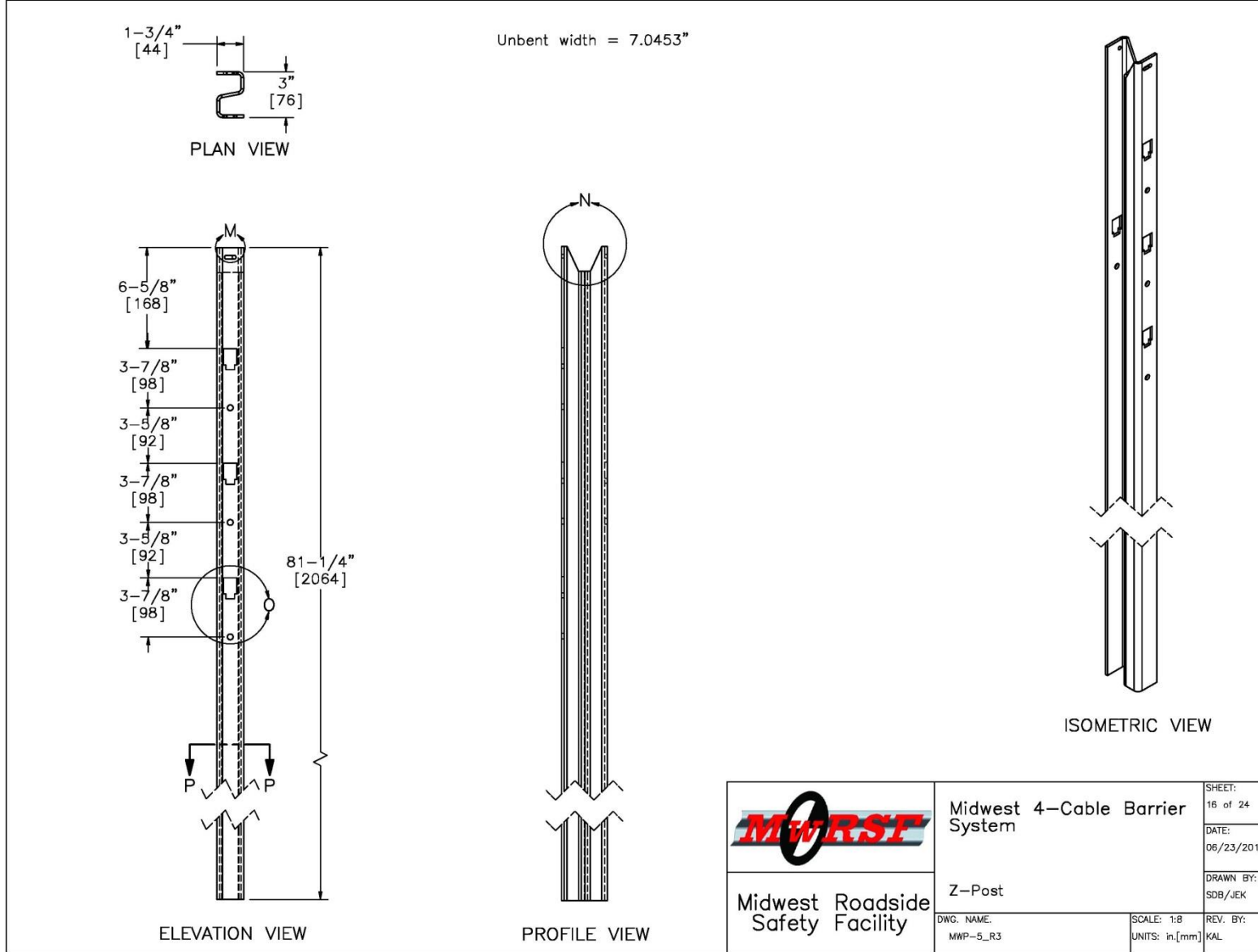


Figure 77. MWP Z-Post Details, Test No. MWP-6

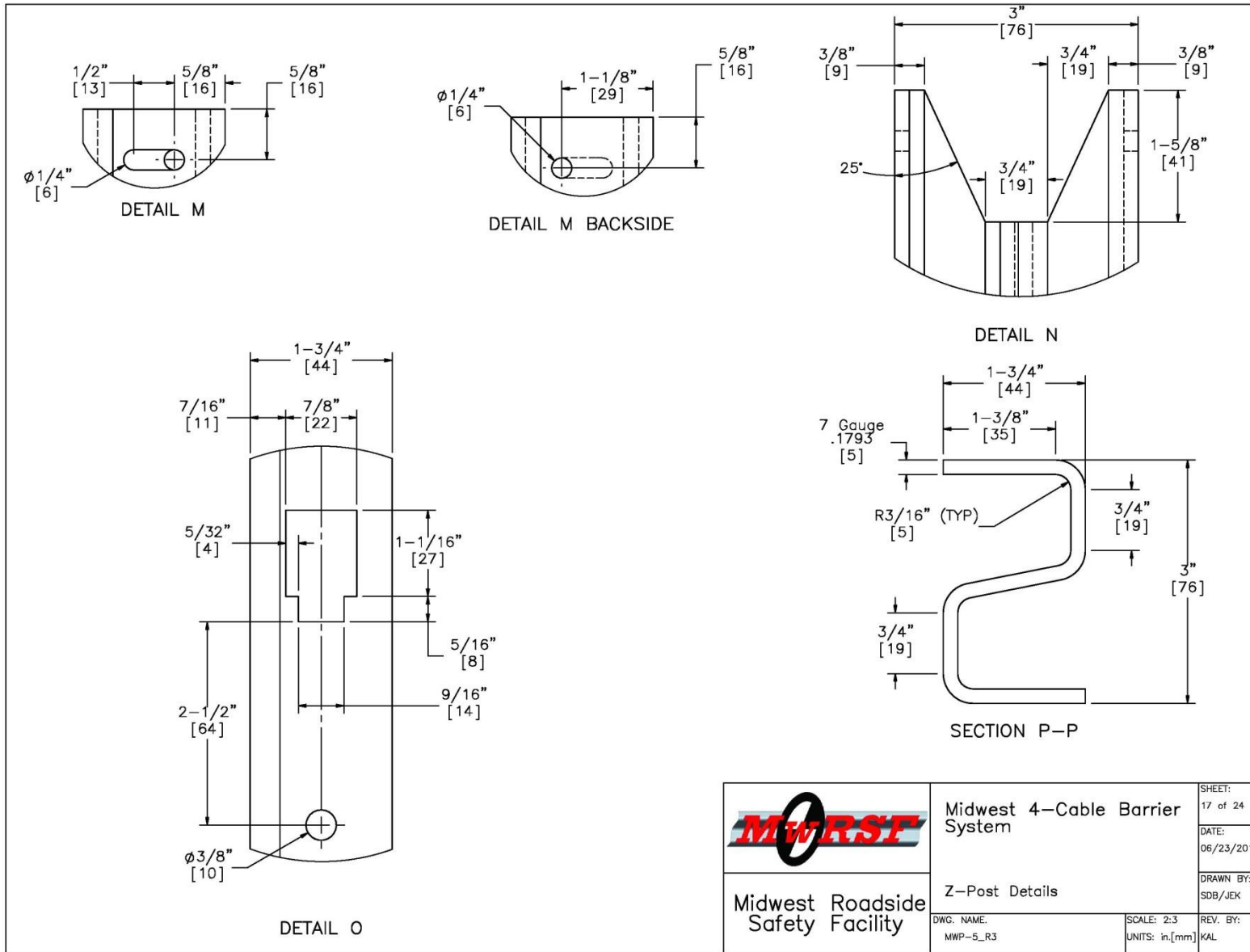


Figure 78. MWP Z-Post Details, Test No. MWP-6

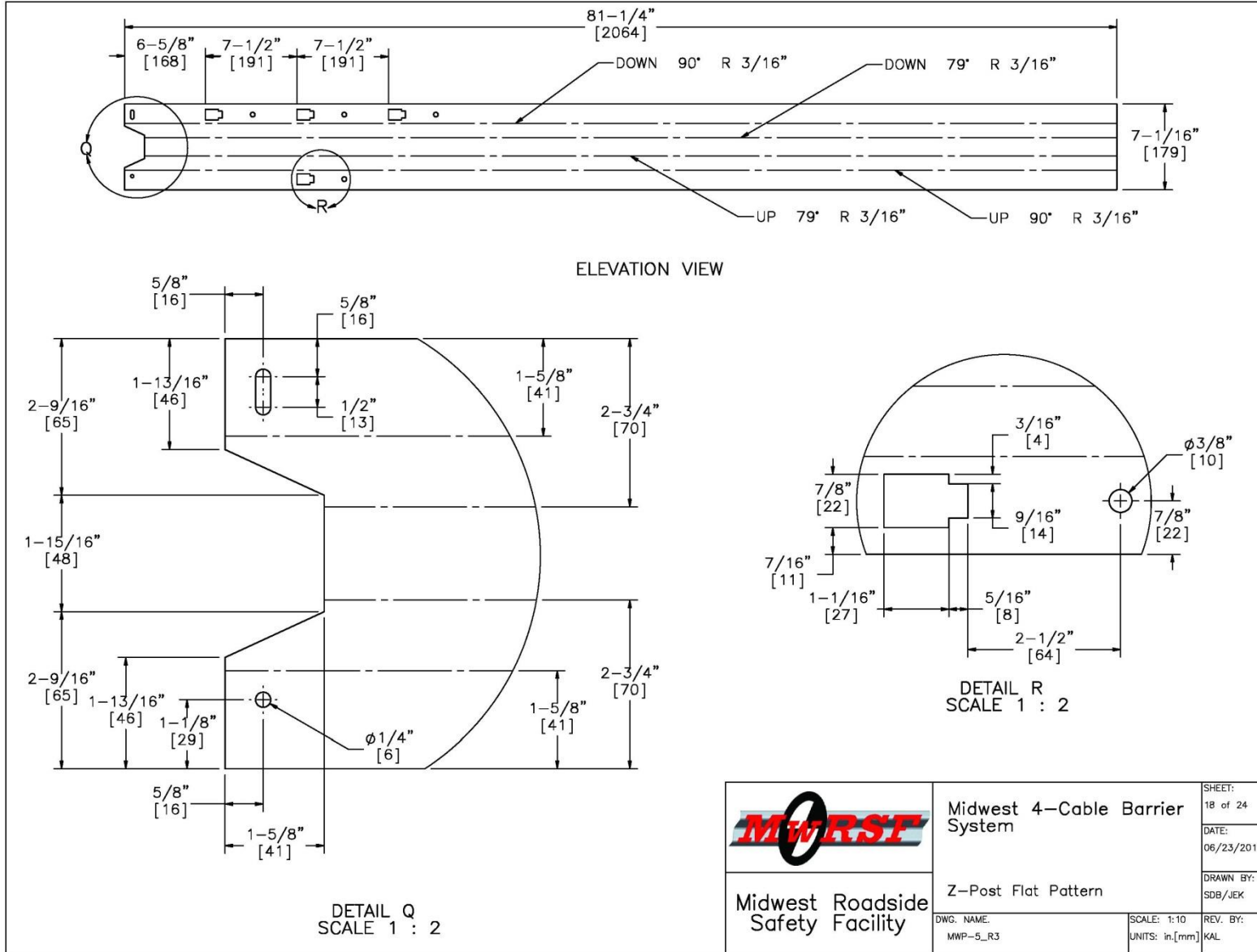


Figure 79. MWP Z-Post Details, Flat Pattern, Test No. MWP-6

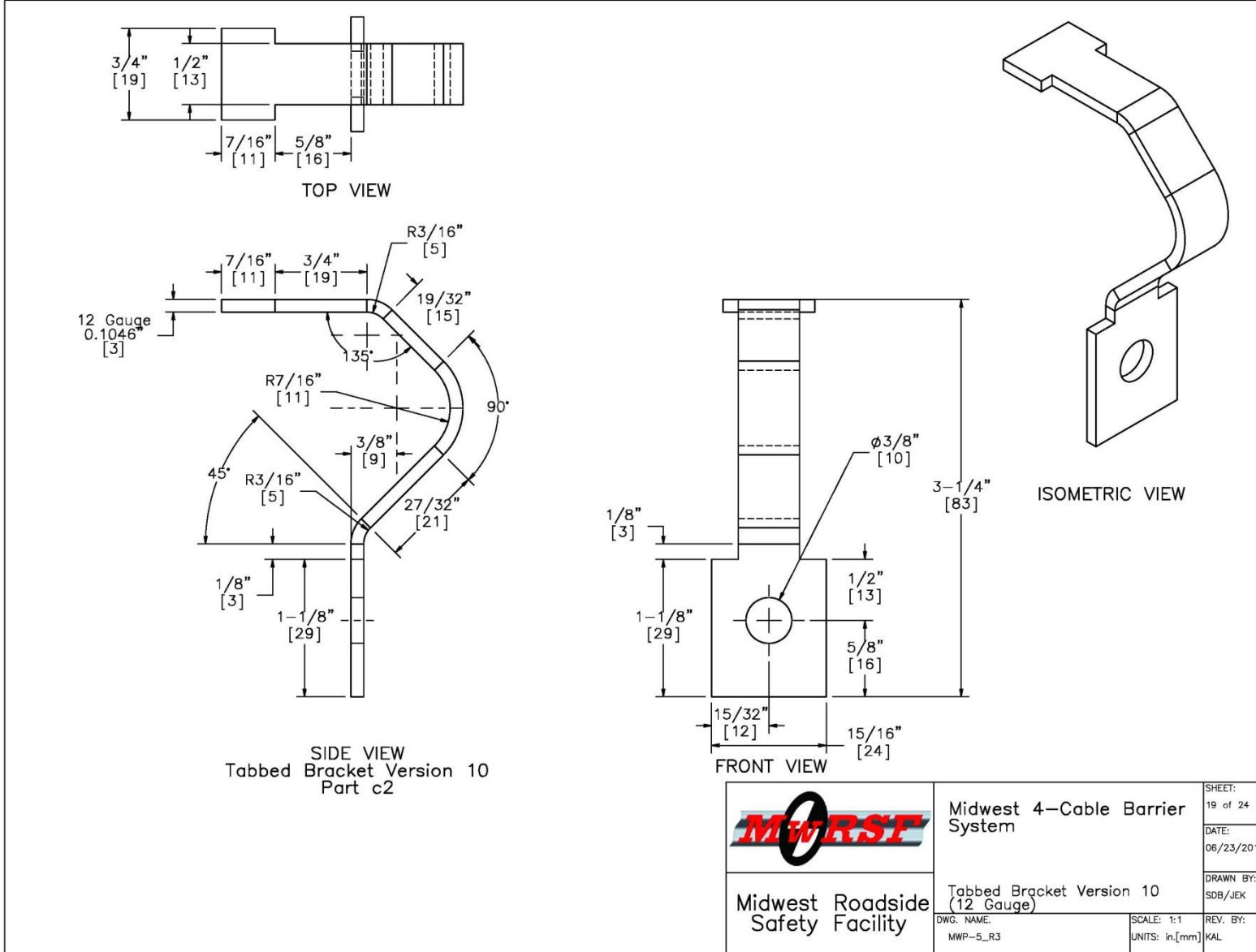


Figure 80. Tabbed Bracket Details, 12-Gauge, Test No. MWP-6

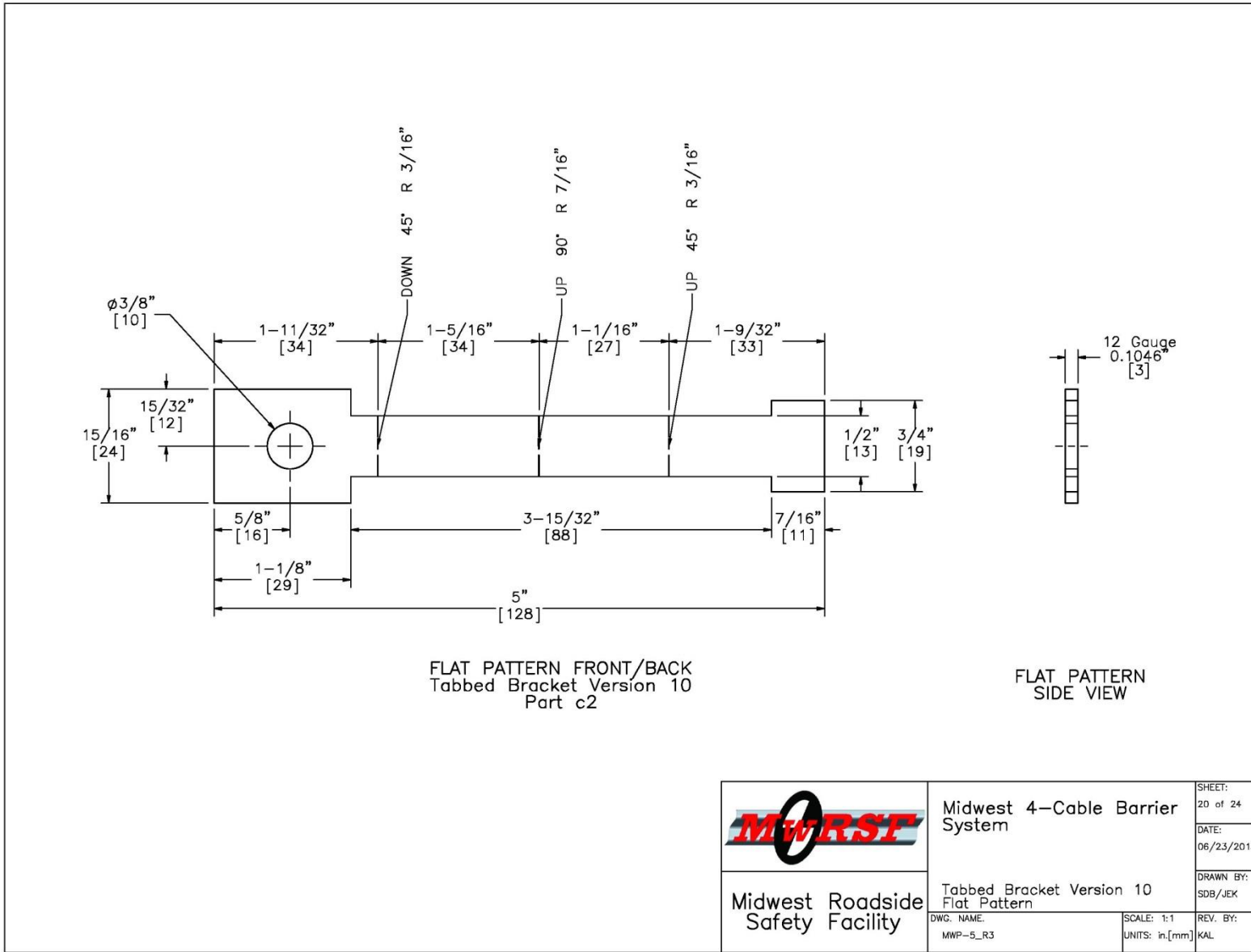


Figure 81. Tabbed Bracket Details, Flat Pattern, Test No. MWP-6

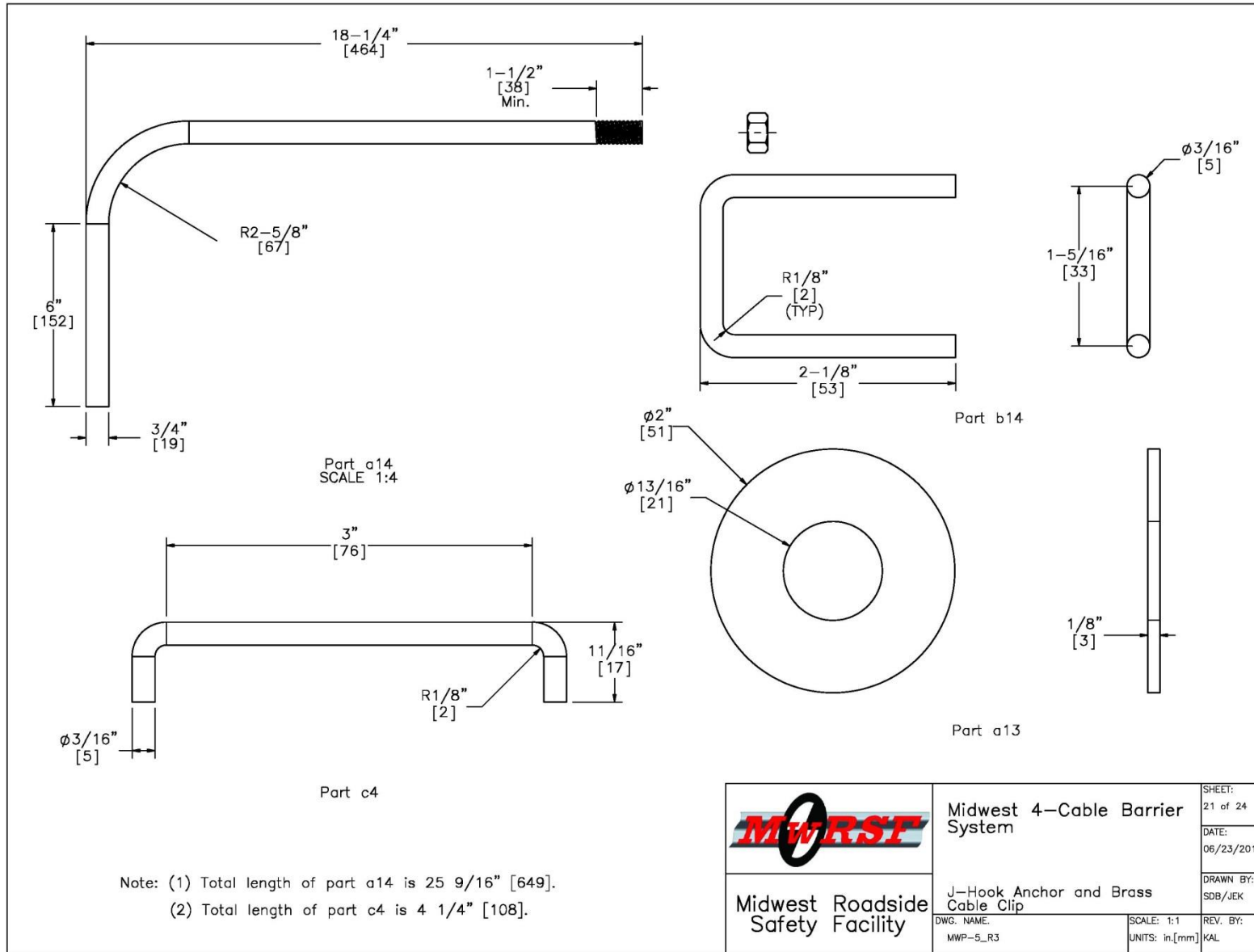


Figure 82. J-Hook Anchor and Brass Clips, Test No. MWP-6

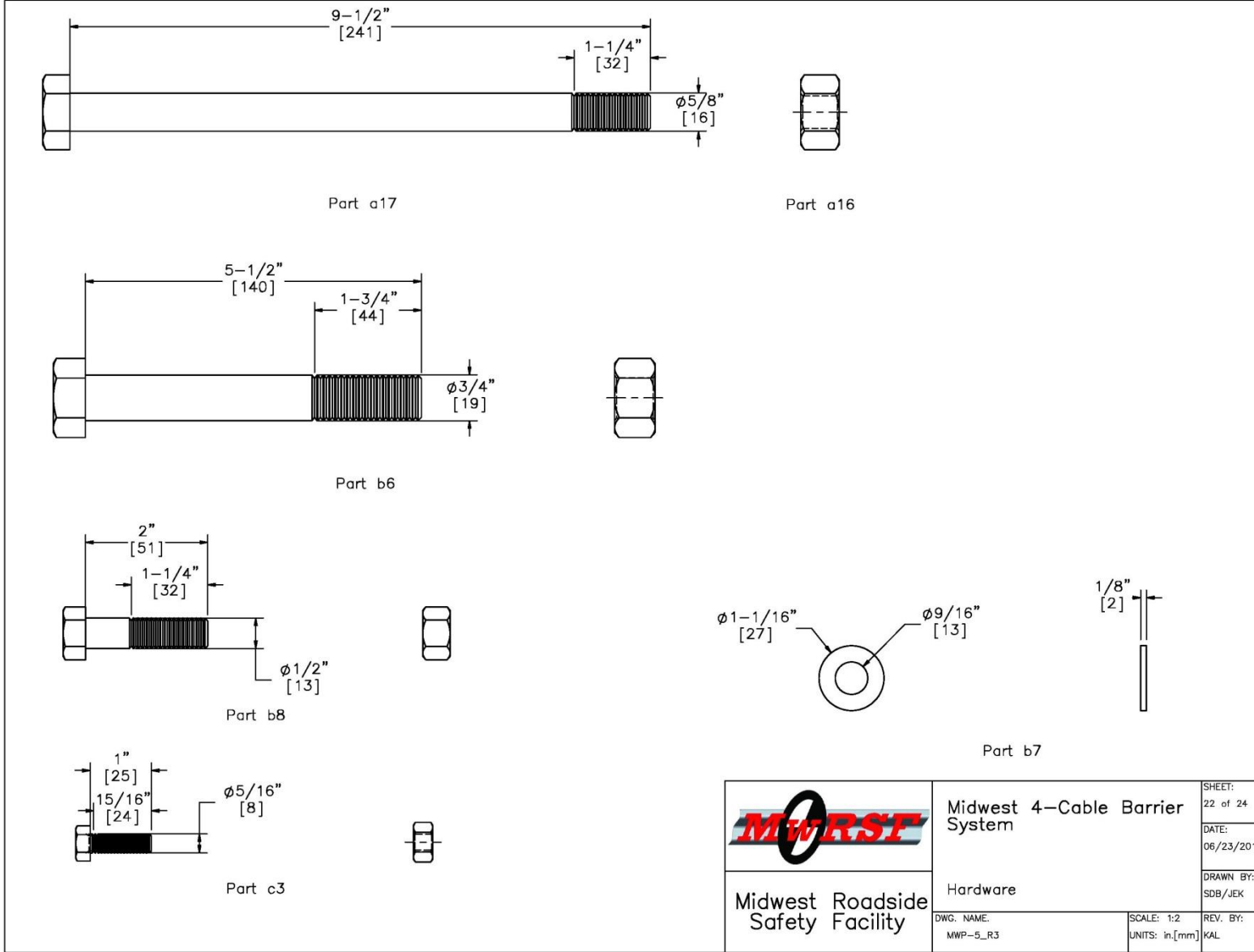


Figure 83. Hardware Details, Test No. MWP-6

Item No.	QTY.	Description	Material Specification
a1	2	Cable Anchor Base Plate	ASTM A36
a2	4	Exterior Cable Plate Gusset	ASTM A36
a3	6	Interior Cable Plate Gusset	ASTM A36
a4	2	Anchor Bracket Plate	ASTM A36
a5	2	3/16" [5] Dia. Brass Keeper Rod, 14" [356] long	Brass
a6	4	Release Gusset	A36 Steel
a7	2	Release Lever Plate	A36 Steel
a8	4	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Tube	ASTM A500 Gr. B
a9	8	CMB High Tension Anchor Plate Washer	ASTM A36
a10	2	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Connecting Tube	ASTM A 500 Gr. B
a11	2	3x10x0.5" [76x254x13] Kicker Plate	ASTM A36
a12	4	CT kicker – gusset	ASTM A36
a13	20	3/4" [19] Dia. Flat Washer	ASTM F844
a14	16	3/4" [19] Dia. UNC J-Hook Anchor and Hex Nut	J-Hook ASTM A449/Nut ASTM A563 DH
a15	2	1/4" [6] Dia. Aircraft Retaining Cable, 36" [914] long	7x19 Galv.
a16	2	5/8" [16] Dia. Heavy Hex Nut	ASTM A563C
a17	2	5/8" [16] Dia. UNC, 9 1/2" [241] Long Hex Bolt	ASTM A449 or SAE J429 Gr. 5
a18	2	24" [610] Dia. Concrete Anchor, 120" [3048] long	4,000 psi f'c
a19	16	#11 Straight Rebar, 114" [2896] long	Grade 60
a20	44	#4 Anchor Hoop Rebar with 21" [533] Dia.	Grade 60
b1	2	S3x5.7 [S76x8.5] Post by 28 1/8" [714]	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A
b2	2	S3x5.7 [S76x8.5] Post by 19" [483]	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A
b3	8	#3 Straight Rebar, 43" [1092] long	Grade 60
b4	22	7 1/4" [184] Dia. No. 3 Hoop Reinforcement	Grade 60
b5	2	2nd Post Keeper Plate, 28 Gauge	ASTM A36
b6	2	3/4" [19] Dia. UNC, 5 1/2" [140] Long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b7	24	1/2" [13] Dia. Washer with 1 1/16" [27] OD	ASTM F844
b8	8	1/2" [13] Dia. UNC, 2" [51] long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b9	2	4x3x1/4" [102x76x6] Foundation Tube, 48" [1168] long	ASTM A500 Grade B
b10	2	2nd Post Cable Hanger	ASTM A36
b11	2	2nd Post Anchor Aggregate 12 in, Depth	-
b12	2	12" Dia. 2nd Post Concrete Anchor, 46" long	4,000 psi f'c
b13	4	2nd Post Base Plate	ASTM A36
b14	8	3/16" [5] Dia. 5 1/4" [133] Long Brass Rod	ASTM B16-00


 Midwest Roadside Safety Facility	Midwest 4-Cable Barrier System	SHEET: 23 of 24 DATE: 06/23/2015 DRAWN BY: SDB/JEK
	Bill of Materials	DWG. NAME: MWP-5_R3 SCALE: NONE UNITS: in,[mm] REV. BY: KAL

Figure 84. Bill of Materials, Test No. MWP-6

Item No.	QTY.	Description	Material Spec
c1	72	3"x1-3/4"x7 Gauge [76x44x4.6], 81 1/4" [2064] Long Bent MWP Z-Section Post	Hot-Rolled ASTM A1011 HSLA Gr. 50
c2	216	12 Gauge Tabbed Bracket - Version 10	Hot-Rolled ASTM A1011 HSLA Grade 50
c3	216	5/16" [8] Dia. UNC, 1" [25] Long Hex Cap Screw and Nut	Bolt SAE J429 Gr. 5 or ASTM A449/Nut ASTM A563 DH
c4	72	Straight Rod - ϕ 3/16" [5] Cable Clip	ASTM B16 Brass C36000 Half Hard (H02), ROUND. TS \geq 68.0 ksi, YS \geq 52.0 ksi
d1	1	3/4" [19] Dia. 3x7 Cable Guiderail	AASHTO M30-92(2000)/ASTM A741-98 Type 1 Class A coating except with Type 1 minimum breaking strength = 39 kips [173.5 kN]
d2	16	7/8" [22] Dia. Hex Nut	ASTM A563C
d3	28	Cable End Threaded Rod	ASTM A449
d4	24	Bennet Cable End Fitter	ASTM A47
d5	24	7/8" [22] Dia. Hex Nut	SAE J429 Gr. 5
e1	8	Bennet Short Threaded Turnbuckle	Not Specified
e2	8	Threaded Load Cell Coupler	N/A
e3	4	50,000-lb [222.4-kN] Load Cell	N/A


	Midwest 4-Cable Barrier System	SHEET: 24 of 24
	Bill of Materials	DATE: 06/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-5_R3	DRAWN BY: SDB/JEK
	SCALE: NONE	REV. BY: KAL
	UNITS: in, [mm]	

Figure 85. Bill of Materials, Test No. MWP-6



Figure 86. Test Installation Photographs, Test No. MWP-6



Figure 87. Test Installation Photographs, Test No. MWP-6

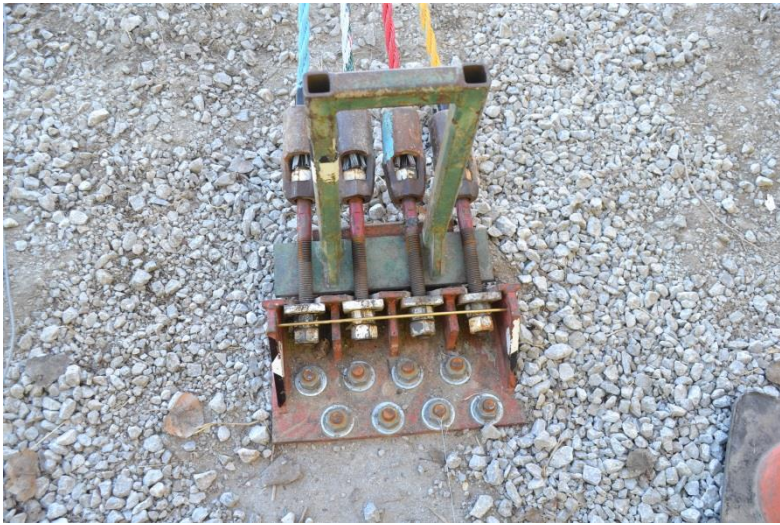


Figure 88. Test Installation Photographs, Test No. MWP-6



Figure 89. Test Installation Photographs, Test No. MWP-6

7 FULL SCALE CRASH TEST NO. MWP-6

7.1 Static Soil Test

Before full-scale crash test no. MWP-6 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The soil for this test was partially frozen, making it difficult to get a full range of soil strength up to 15 in. of deflection. The winch utilized to load the post actually reached its capacity, prior to reaching 15 in. (381 mm) of displacement. The winch capacity is over 2.5 times the required strength. Note that weak posts used in cable barrier systems do not rotate in strong soil. Instead, weak posts yield at the ground line in both frozen and unfrozen strong soils configured with compacted crushed limestone. Thus, the frozen soil condition was considered acceptable for this cable barrier test. The static test results, as shown in Appendix C, demonstrated a soil resistance above the baseline test limits. Thus, the soil provided adequate strength, and full-scale crash testing could be conducted on the barrier system.

7.2 Weather Conditions

Test no. MWP-6 was conducted on January 16, 2015 at approximately 2:30 p.m. The weather conditions, as per the National Oceanic and Atmospheric Administration (station 14939/LNK), were reported and are shown in Table 9.

Table 9. Weather Conditions, Test No. MWP-6

Temperature	59°F
Humidity	31%
Wind Speed	15 mph
Wind Direction	40° West of True South
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0 in.
Previous 7-Day Precipitation	0 in.

7.3 Test No. MWP-6

The 2,572-lb (1,167-kg) small car impacted the high-tension, four-cable median barrier at a speed of 63.5 mph (102.2 km/h) and at an angle of 24.9 degrees. A summary of the test results and sequential photographs are shown in Figure 90. Additional sequential photographs are shown in Figures 91 and 92. Documentary photographs of the crash test are shown in Figure 93.

7.4 Test Description

Initial vehicle impact was to occur at a midspan location, or 4 ft (1.2 m) upstream from post no. 32, as shown in Figure 94, which was selected according to MASH guidelines. The actual point of impact was approximately 4.5 in. (114 mm) upstream from the target impact point. A sequential description of the impact events is contained in Table 10. The vehicle came to rest 234 ft - 6 in. (71.5 m) downstream from the point of impact. The vehicle trajectory and final position are shown in Figures 90 and 95.

Table 10. Sequential Description of Impact Events, Test No. MWP-6

TIME (sec)	EVENT
0.000	Vehicle left-front bumper contacted cable no. 2 between post nos. 31 and 32, and front bumper began to deform.
0.006	Vehicle left-front bumper contacted cable no. 1 between post nos. 31 and 32.
0.008	Vehicle hood and left headlight contacted cable no. 3 between post nos. 31 and 32.
0.018	Post no. 32 began to deflect backward and downstream, and post no. 31 began to deflect backward.
0.020	Cable no. 3 detached from post no. 32.
0.022	Vehicle hood began to deform and post no. 33 began to deflect upstream.
0.024	Post no. 33 began to deflect backward.
0.028	Vehicle left side mirror contacted cable no. 4.
0.030	Cable no. 3 detached from post no. 31.
0.034	Vehicle left A-pillar contacted cable no. 3.
0.038	Vehicle front bumper contacted post no. 32.
0.042	Vehicle left A-pillar contacted cable no. 4.
0.044	Cable no. 4 detached from post no. 32.
0.046	Vehicle hood contacted cable no. 4, and post no. 30 began to deflect backward.
0.056	Cable no. 3 detached from post no. 33.

0.062	Vehicle left A-pillar began to deform, post no. 31 began to bend backward, and post no. 34 began to deflect backward.
0.066	Post no. 29 began to deflect downstream.
0.080	Vehicle left-front tire overrode cable no. 1, cable no. 2 detached from post no. 33, and cable no. 3 detached from post no. 34.
0.082	Vehicle left side mirror detached.
0.086	Cable no. 3 detached from post no. 29.
0.092	Vehicle left-front tire overrode cable no. 1, and post no. 29 began to deflect backward.
0.098	Cable no. 2 detached from post no. 34, and cable no. 3 detached from post no. 35.
0.102	Post no. 35 began to deflect backward.
0.108	Vehicle left-front door began to deform.
0.112	Post no. 36 began to deflect backward, and cable no. 4 detached from post no. 31.
0.114	Vehicle began to yaw away from barrier.
0.116	Vehicle right-front bumper contacted post no. 33, and cable no. 3 detached from post no. 36.
0.120	Cable no. 4 detached from post no. 31.
0.122	Cable no. 4 detached from post no. 33.
0.130	Cable no. 2 detached from post no. 36.
0.136	Vehicle began to pitch upward.
0.138	Cable no. 3 detached from post no. 28.
0.146	Post no. 37 began to deflect backward.
0.160	Post no. 28 began to deflect backward, and cable no. 3 detached from post no. 37.
0.162	Vehicle left-rear tire overrode cable no. 1.
0.164	Cable no. 4 detached from post no. 34.
0.166	Cable no. 4 detached from post no. 30.
0.174	Vehicle underrode cable nos. 3 and 4 while cables were in contact with roof. Vehicle roof began to deform.
0.176	Cable no. 4 detached from post no. 35.
0.180	Vehicle right-front tire overrode cable no. 1.
0.182	Cable no. 3 detached from post no. 27.
0.194	Cable no. 4 detached from post no. 29.
0.196	Cable no. 4 detached from post no. 36.
0.216	Cable no. 4 detached from post no. 37.
0.244	Post no. 34 began to bend backward.
0.270	Vehicle right-rear tire overrode cable no. 1.
0.352	Cable no. 2 detached from post no. 37
0.456	Vehicle was parallel to system.
0.490	Vehicle left headlight became detached.
0.678	Vehicle right-rear door contacted post no. 38.
0.742	Vehicle was yawing away from barrier.
0.752	Vehicle right-side mirror contacted cable no. 4.
0.764	Vehicle rear bumper detached.
0.794	Vehicle began to roll toward barrier.
0.800	Vehicle bumper impacted post no. 39, and post no. 39 bent downstream.
0.830	Vehicle right-front tire became airborne.

0.920	Vehicle bumper impacted post no. 40, and post no. 40 bent downstream.
0.930	Vehicle right-front tire overrode cable no. 3 as it came back across system.
1.508	Vehicle underrode cable no. 4.
1.602	Vehicle was parallel to system.
1.642	Vehicle exited system.
6.800	Vehicle came to a stop 234.5 ft (71.5 m) downstream from impact.

7.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 96 through 104. Barrier damage consisted of bent posts, disengaged cables, and bent and fractured brackets. At its final resting position, the vehicle was no longer in contact with the system.

Cable no. 4 disengaged from post nos. 29 through 52 due to fracturing of the brass keeper rods. Cable no. 3 disengaged from post nos. 24 through 49. Cable no. 2 disengaged from post nos. 32 through 40. Cable no. 1 disengaged from post nos. 32, 33, as well as from post nos. 35 through 39. Two of the brackets that released cable no. 2 fractured at the neck of the bracket. All of the other brackets released cable nos. 1 through 3 through rotation of the bracket tab through the key, allowing cables to release vertically. Displacement of the cable within the splices was documented. The maximum cable displacement within a splice was ½ in. (13 mm), found on the load cell splice located upstream from impact on cable no. 2.

Post nos. 30 through 41 had varying degrees of plastic deformations in the form of bending and twisting. The majority of the posts twisted to face downstream and/or bent back and downstream. In addition, post nos. 32, 33, as well as post nos. 38 through 40 had contact marks due to the vehicle overriding the posts.

The maximum dynamic barrier deflection was 89 in. (2,261 mm), and the working width of the system was 90.5 in. (2,299 mm), as determined from high-speed video analysis. Neither the upstream or downstream anchors showed signs of displacement.

7.6 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 105 through 110. The maximum occupant compartment deformations are listed in Table 11 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH-established deformation limits were violated. Complete occupant compartment and vehicle deformations as well as the corresponding locations are provided in Appendix D.

Table 11. Maximum Occupant Compartment Deformations by Location, Test No. MWP-6

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	0.5 (13)	≤9 (229)
Floor Pan & Transmission Tunnel	1.3 (33)	≤12 (305)
Side Front Panel (in Front of A-Pillar)	0.1 (3)	≤12 (305)
Side Door (Above Seat)	0.2 (5)	≤12 (305)
Side Door (Below Seat)	0.0 (0)	≤9 (229)
Roof	1 (25)	≤4 (102)

The majority of the vehicle damage was concentrated on the left-front corner and left side of the vehicle where impact occurred, although other notable damage was found on the right-front corner. The vehicle's left and right headlights were both disengaged. The lower front bumper, the plastic portion of the rear bumper, both side mirrors, and the right-rear door handle were also disengaged. There was a 2½-in. (64 -mm) gap between the hood and the bumper, and a 4-in. (102-mm) gap between the fender and hood on the left side. The left fender was bent backward 9 in. (229 mm), folding into the vehicle on the bottom, resulting in a 14-in. (356-mm) buckle beginning above the left-front tire. There was also a 9x6-in. (229x152-mm) dent on the right-front door and fender. Three quarters of the left-front wheel well was removed from the vehicle. There was a 1½-in. (38-mm) long tear in the deflated left-front tire. The lower 16 in.

(406 mm) of the left fender as well as the lower 11 in. (279 mm) of the front half of the left-front vehicle door had been torn off. The left-front door was separated from the roof by $\frac{3}{8}$ in. (10 mm). There was a $\frac{3}{4}$ in. (19 mm) gap between the right fender and right-front door and a 1 in. (25 mm) gap between the right fender and hood.

Contact marks from cables covered a majority of the vehicle – specifically on the front bumper, left side of the hood and left fender, left-front wheel rim, bottom of the left-rear door, on the right-rear door, along both A-pillars and on the entire roof. The majority of these contact marks were accompanied by gouges. The worst gouging occurred along the A-pillars, where the gouging on the left A-pillar caused the windshield to crack. Spider-web cracking occurred adjacent to the left-front A-pillar and propagated outward, extending as far as the center of the windshield.

Tears occurred on the plastic portion of the front bumper. There was also a 19-in. (483-mm) by 5-in. (127-mm) tear in the left front door, 11 in. (279 mm) above the bottom of the door. Dents were noted on the lower front bumper, on the front of the hood, at the left-front corner of the roof, along the bottom right side of the vehicle, on the right fender, and on the right-front door.

The floorpan was torn in several locations. A 7.5-in. (191-mm) long floorpan tear was located on the left side of the transmission hump, and a 4-in. (102-mm) long tear was on the right side of the transmission hump extending backward from a hole in the floorpan. These tears can be seen on the interior of the vehicle in Figure 107 and from the undercarriage in Figure 108. Although the occupant compartment deformations were within the bounds set by MASH, the occupant compartment penetrations via floorpan tears were unacceptable. The spare tire area of the trunk also had a 4-in. (102-mm) long tear, as shown in Figure 109. While not part of the

occupant compartment, this trunk damage still raises concern. Additional scrapes and gouges were found on the floorpan and vehicle undercarriage, as shown in Figure 110.

7.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 12. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 12. The results of the occupant risk analysis, as determined from the accelerometer data, are also summarized in Figure 90. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix G.

Table 12. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MWP-6

Evaluation Criteria		Transducer		MASH Limits
		SLICE 1 (primary)	SLICE 2	
OIV ft/s (m/s)	Longitudinal	-11.98 (-3.65)	-11.98 (-3.65)	≤ 40 (12.2)
	Lateral	11.25 (3.43)	10.14 (3.09)	≤ 40 (12.2)
ORA g's	Longitudinal	-6.77	-6.26	≤ 20.49
	Lateral	5.77	6.78	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	-19.60	-16.97	≤ 75
	Pitch	4.52	-3.02	≤ 75
	Yaw	46.04	45.35	not required
THIV ft/s (m/s)		16.27 (4.96)	14.86 (4.53)	not required
PHD g's		6.86	7.12	not required
ASI		0.42	0.43	not required

7.8 Load Cells and String Potentiometers

The pertinent data from the load cells and string potentiometer were extracted from the bulk signal and analyzed using each transducer’s calibration factor. The upstream anchor showed no displacement. A summary of the maximum cable loads can be found in Table 13. The recorded data and analyzed results are detailed in Appendix H. The exact moment of impact could not be determined from the transducer data, as impact may have occurred prior to observing a measurable signal in the electronic data. Thus, the extracted data curves should not be taken as a precise time after impact, but rather a general timeline between events within the data curve itself.

Table 13. Maximum Cable Loads, Test No. MWP-6

Cable Location	Sensor Location	Maximum Cable Load		Time (sec)
		kip	kN	
Combined Cable Load	Upstream of Impact	32.99	146.75	0.1249
Cable No. 4	Upstream of Impact	7.14	31.76	1.0997
Cable No. 3	Upstream of Impact	7.76	34.52	0.1521
Cable No. 2	Upstream of Impact	18.94	84.25	0.3838
Cable No. 1	Upstream of Impact	11.66	51.87	0.0442

7.9 Discussion

The analysis of the test results for test no. MWP-6 showed that the high-tension, four-cable median barrier contained and redirected the 1100C vehicle, with controlled lateral displacements of the barrier. The test vehicle did not penetrate or ride over the barrier, and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix G, were deemed acceptable, because they did not adversely influence occupant risk safety criteria or cause rollover. After impact, the vehicle trajectory was limited by the barrier system and brought to a rest 234 ft - 6 in. (71.5 m)

downstream from the point of impact. As the vehicle overrode the system posts, the posts tore the floorpan in two separate locations. The tears indicated that the top of these posts could have penetrated into the occupant compartment. Therefore, test no. MWP-6, conducted on the four-cable median barrier, was determined to be unacceptable according to the MASH safety performance criteria for test designation no. 3-10.



0.000 sec



0.092 sec



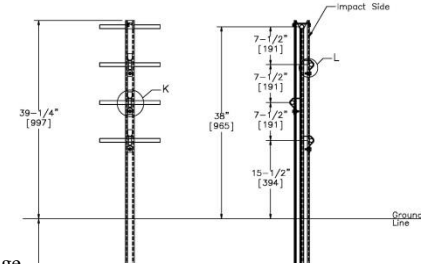
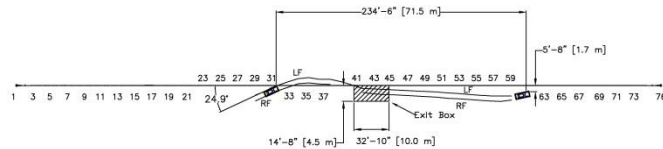
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- Test AgencyMwRSF
- Test Number..... MWP-6
- Date01/16/2015
- MASH Test Designation3-10
- Test Article..... Four Cable Median Barrier
- Total Length 604 ft (184.1 m)
- Key Component - Cable
 - Size..... 3x7, 3/4-in. (19-mm) diameter
 - Cable Heights 15½, 23, 30½, 38 in. (394 mm, 584 mm, 775 mm, 965 mm)
- Key Component - MWP
 - Dimensions..... 3 x 1¾ x 81¼ in. (76 x 44 x 2,064 mm)
 - Spacing..... 8 ft (2.44 m)
- Soil TypeCompacted, coarse, crushed limestone
- Vehicle Make /Model.....2009 Kia Rio
 - Curb.....2,295 lb (1,041 kg)
 - Test Inertial.....2,405 lb (1,091 kg)
 - Gross Static.....2,572 lb (1,167 kg)
- Impact Conditions
 - Speed63.5 mph (102.2 km/h)
 - Angle 24.9 deg
 - Impact Location.....4 ft - 4.5 in. (1.33 m) upstream of Post No. 32
- Impact Severity (IS)57.3 kip-ft (77.7 kJ) > 51 kip-ft (69.1 kJ)
- Exit Conditions
 - Speed24.3 mph (39.1 km/h)
 - Angle 1 deg
- Exit Box CriterionPass
- Vehicle Stability..... Satisfactory
- Vehicle Stopping Distance234 ft - 6 in. (71.5 m)
- Vehicle Damage..... Extensive
 - VDS [8]11-FL-6
 - CDC [9].....11-FDAK-8
 - Maximum Interior Deformation 1.52 in. (39 mm)

- Test Article Damage Moderate
- Maximum Test Article Deflections
 - Permanent Set46¼ in. (1,175 mm)
 - Dynamic89 in. (2,261 mm)
 - Working Width.....90.5 in. (2,299 mm)
- Transducer Data

Evaluation Criteria		Transducer		MASH Limit
		SLICE-1 (primary)	SLICE-2	
OIV ft/s (m/s)	Longitudinal	-11.98 (-3.65)	-11.98 (-3.65)	≤ 40 (12.2)
	Lateral	11.25 (3.43)	10.14 (3.09)	≤ 40 (12.2)
ORA g's	Longitudinal	-6.77	-6.26	≤ 20.49
	Lateral	5.77	6.78	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	-19.60	-16.97	≤ 75
	Pitch	4.52	-3.02	≤ 75
	Yaw	46.04	45.35	not required
THIV – ft/s (m/s)		16.27 (4.96)	14.86 (4.53)	not required
PHD – g's		6.86	7.12	not required
ASI		0.42	0.43	not required

Figure 90. Summary of Test Results and Sequential Photographs, Test No. MWP-6



0.000 sec



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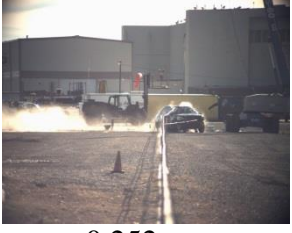
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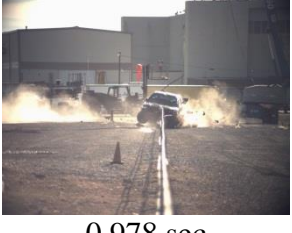
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Figure 91. Additional Sequential Photographs, Test No. MWP-6



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0.930 sec



1.508 sec

Figure 92. Additional Sequential Photographs, Test No. MWP-6



Figure 93. Documentary Photographs, Test No. MWP-6



Figure 94. Impact Location, Test No. MWP-6



Figure 95. Vehicle Final Position and Trajectory Marks, Test No. MWP-6



Figure 96. System Damage, Test No. MWP-6



Figure 97. System Damage, End Anchorages, Test No. MWP-6

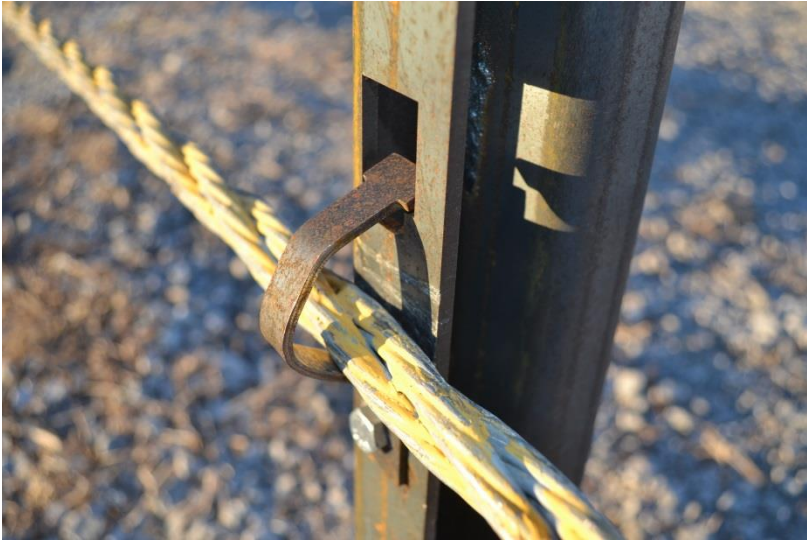


Figure 98. System Damage, Cable Brackets, Test No. MWP-6



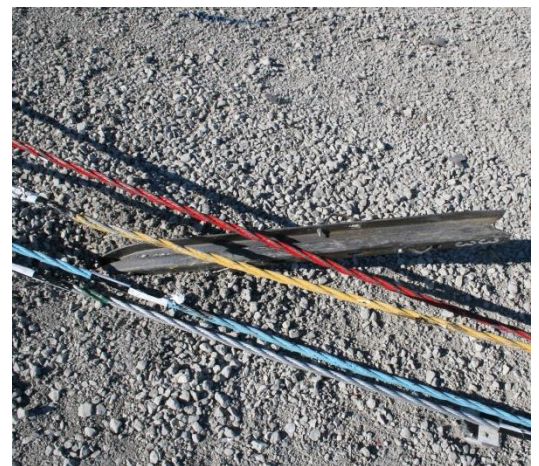
Figure 99. Example System Damage, Brass Rods, Test No. MWP-6



Post No. 31

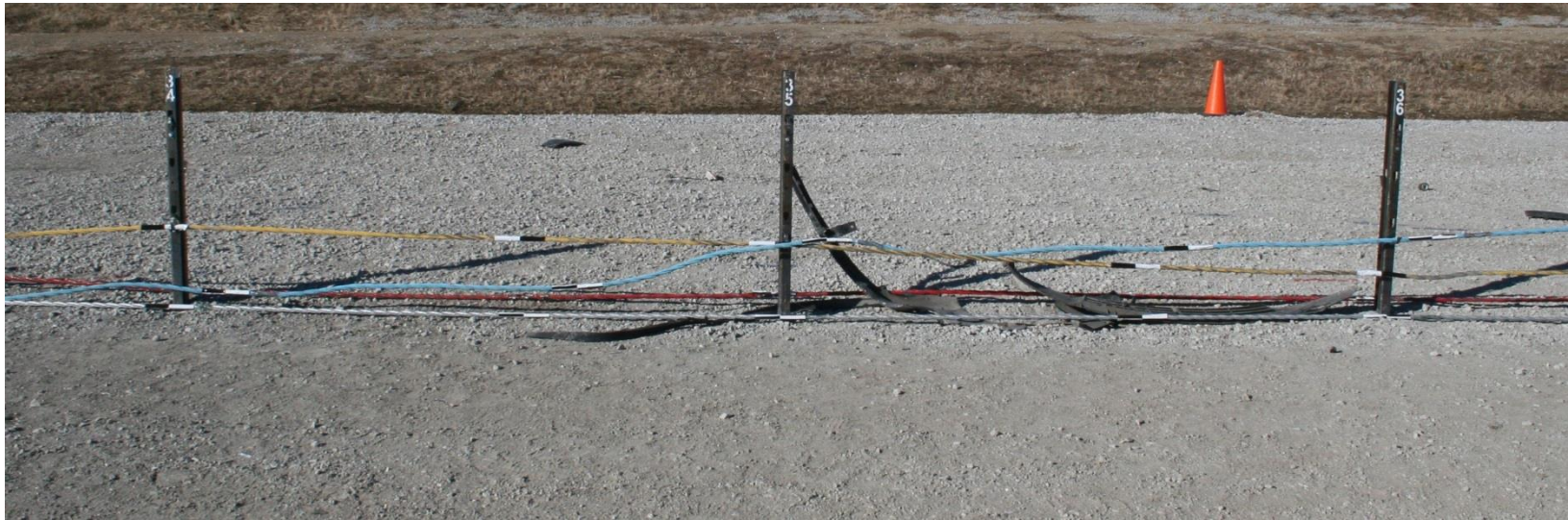


Post No. 32



Post No. 33

Figure 100. System Damage, Post Nos. 31 through 33, Test No. MWP-6



Post No. 34



Post No. 35



Post No. 36

Figure 101. System Damage, Post Nos. 34 through 36, Test No. MWP-6



Post No. 37

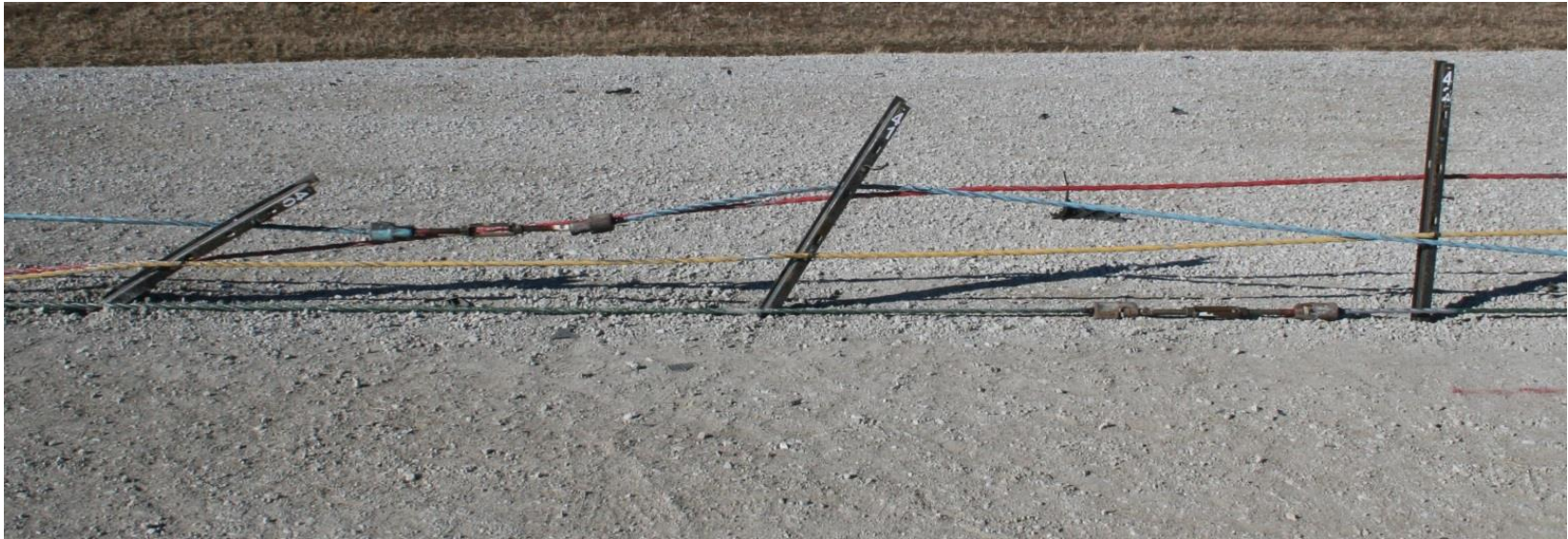


Post No. 38

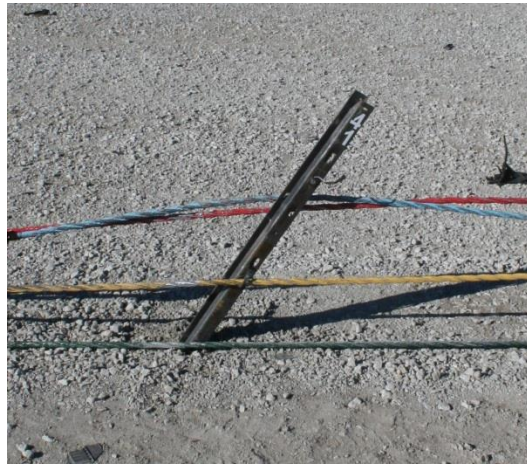


Post No. 39

Figure 102. System Damage, Post Nos. 37 through 39, Test No. MWP-6



Post No. 40



Post No. 41



Post No. 42

Figure 103. System Damage, Post Nos. 40 through 42, Test No. MWP-6

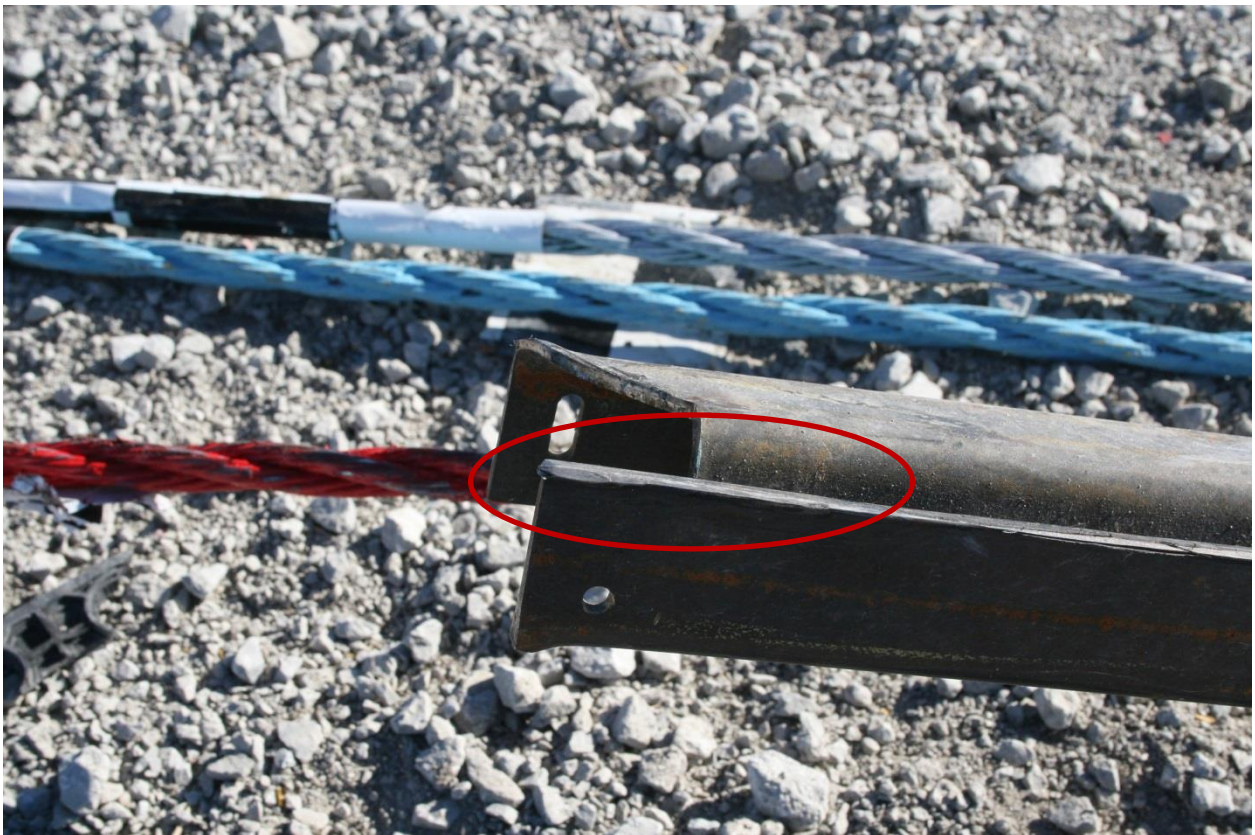


Figure 104. Post Contact Marks, Test No. MWP-6

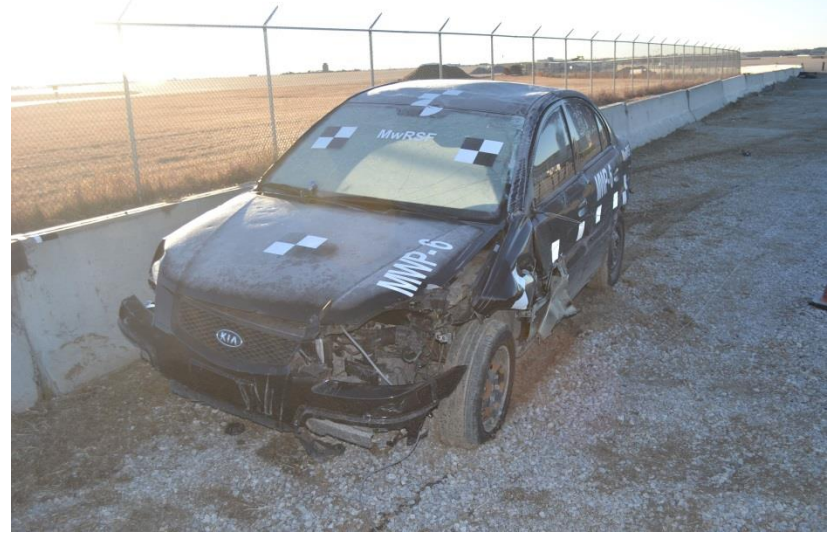


Figure 105. Vehicle Damage, Test No. MWP-6



Figure 106. Vehicle Damage, Test No. MWP-6



Figure 107. Occupant Compartment Damage, Test No. MWP-6



Figure 108. Occupant Compartment Penetration, Test No. MWP-6



Figure 109. Spare Tire Compartment Penetration, Test No. MWP-6

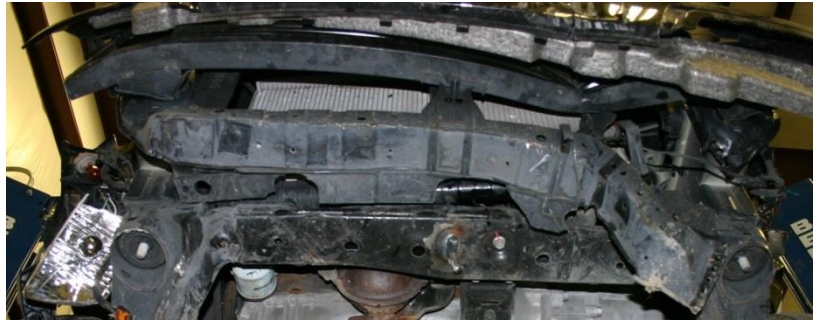


Figure 110. Additional Undercarriage Damage, Test No. MWP-6

8 DESIGN DETAILS TEST NO. MWP-7

8.1 Proposed System Modifications

Following the unsuccessful system performance in test no. MWP-6, the researchers brainstormed several potential design changes to mitigate floorpan penetrations. Analysis of the vehicle undercarriage and contact marks on both the system posts and the vehicle suggested that the floorpan tears were created as the post was overridden by the vehicle and the edges of the post scraped along the bottom of the vehicle. Contact marks from both the left and right flanges when bending about the weak axis of the post were visible in the deformed floorpan. A review of these contact marks indicated that the tearing was primarily caused by the free edges of the post, as shown in Figures 104 and 108.

In order to mitigate the floorpan tearing, several design modifications were proposed to the line posts. These options included:

1. a reduction of the weak-axis capacity of the post to lower the upward force exerted by the post on the floorpan, which could be achieved through the addition of weakening holes, reducing the thickness of the post, or altering the post cross-sectional geometry.
2. adding a fillet radius to the post corners to remove sharp corners at the top of the post.
3. treating of the post edges through edge rounding or hemming.
4. adding edge or corner protectors to the upper portion of the post.
5. developing a new post section without free edges.

An alteration of the post cross-section and a reduction in the weak-axis bending capacity of the post were both deemed good options, but they were anticipated to require a significant amount of research and development prior to proceeding with a modified design. Treatment of the sheet metal edges through rounding or hemming was also considered, but it was thought to be costly with respect to edge rounding. Hemming was eliminated due to complications with

hemming sheet steel as thick as 7 gauge (5 mm). The addition of edge or corner protectors to the upper portion of the post was believed to be an effective option. However, the additional component and potential cost made it initially less attractive. Thus, the addition of a fillet radius to the corners of the post was chosen to mitigate the floorpan tears. It was believed that removal of sharp corners near the top of the post would mitigate the stress concentrations imparted to the floorpan, while providing for minimal modification of the MWP post. As such, a $\frac{5}{8}$ -in. (16-mm) radius was added to the top corners of the free edges of the MWP post, and a $\frac{1}{4}$ -in. (6-mm) radius was added to the top corners of the V-notch in the center of the post.

8.2 System Design Details

The four-cable median barrier system used for test no. MWP-7 was nearly identical to that used in test no. MWP-6, as shown in Figures 111 through 137. The targeted impact location, post spacing, and cable orientation for test no. MWP-7 remained the same as used in test no. MWP-6. The cables were tensioned to MASH specifications, as in the other tests, using the cable tensioning chart shown in Table 3. Thus, the cables were tensioned to a pre-load of 2,500 lb (11.1 kN).

The system layout for test no. MWP-7 is shown in Figure 111. For test no. MWP-7, post nos. 24 through 47 were substituted with a modified MWP that had rounded edges at its top in an attempt to reduce the likelihood of tearing the floorboard and penetrating into the occupant compartment. These modifications are detailed in Figures 129 through 131. Photographs of the test installation are shown in Figures 138 to 141. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix A.

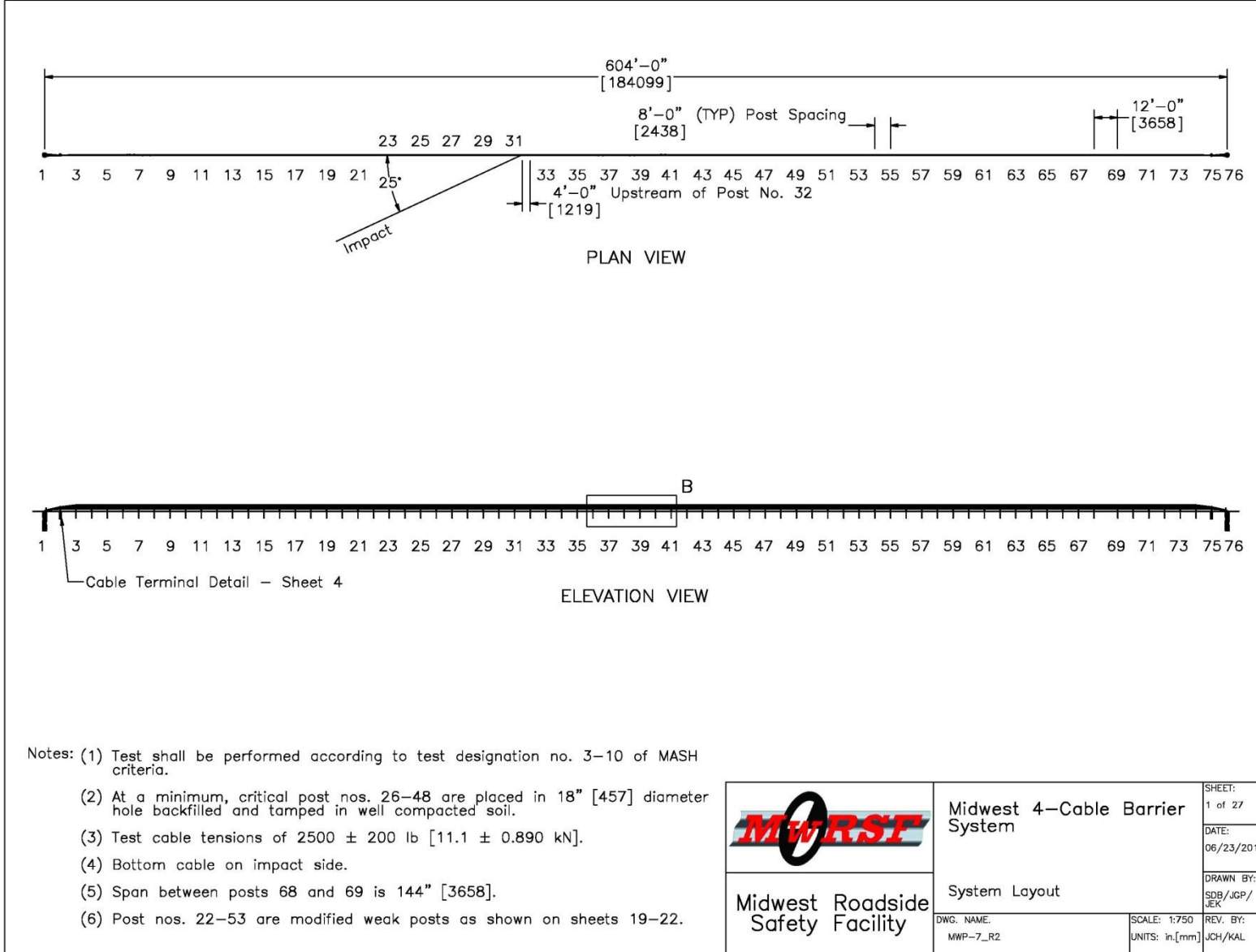


Figure 111. Test Installation Layout, Test No. MWP-7

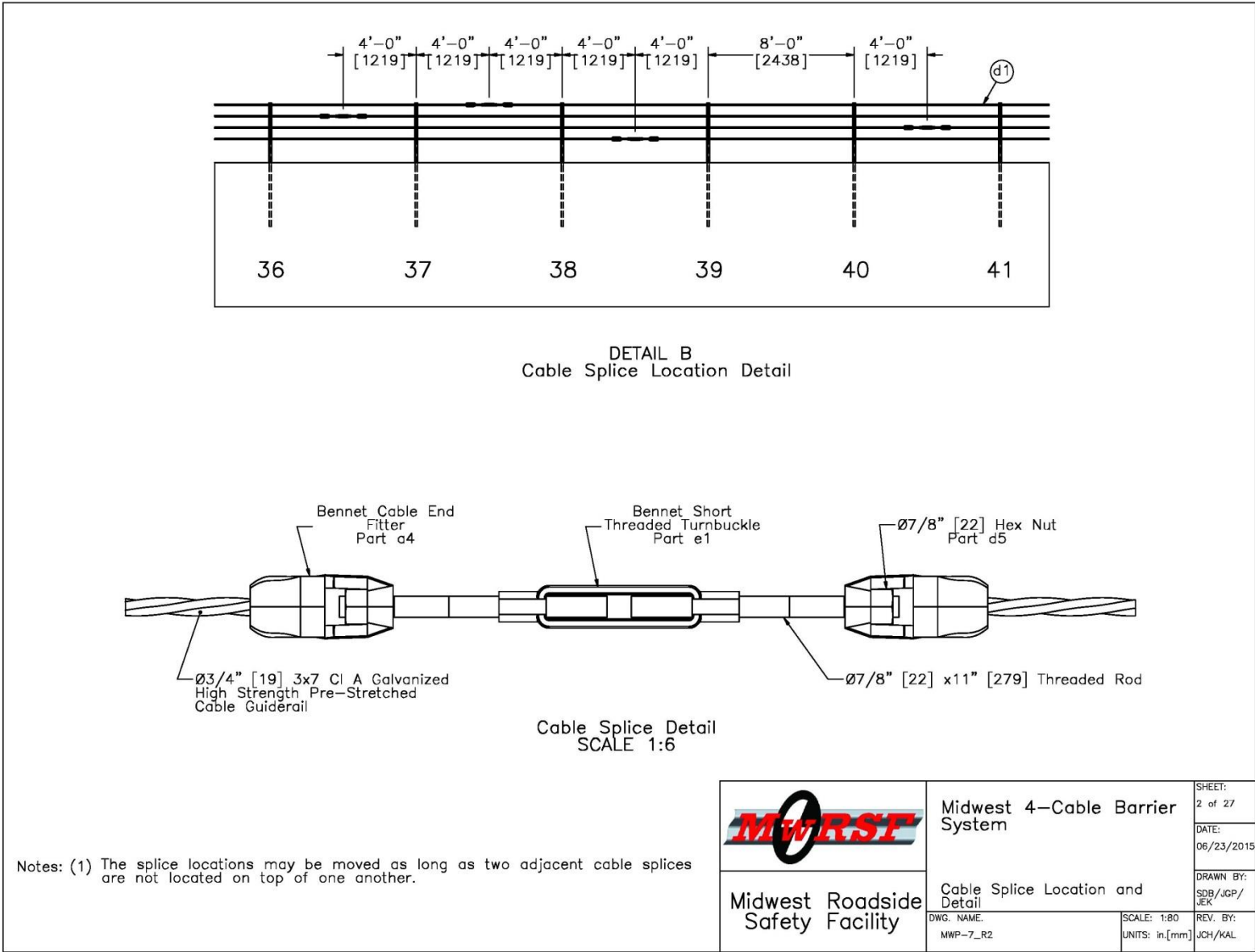


Figure 112. Cable Splice Location and Detail, Test No. MWP-7

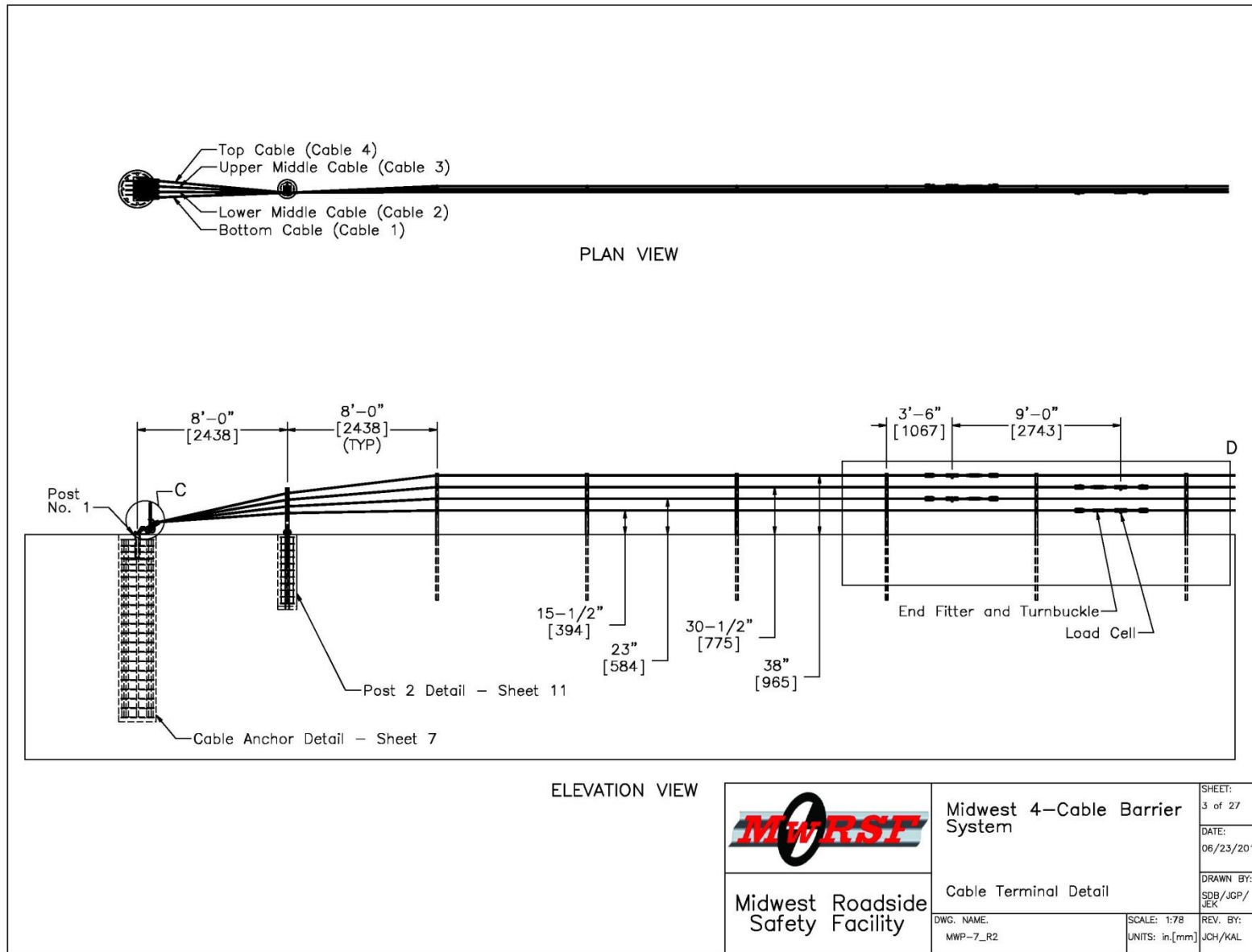


Figure 113. Cable Terminal Detail, Test No. MWP-7

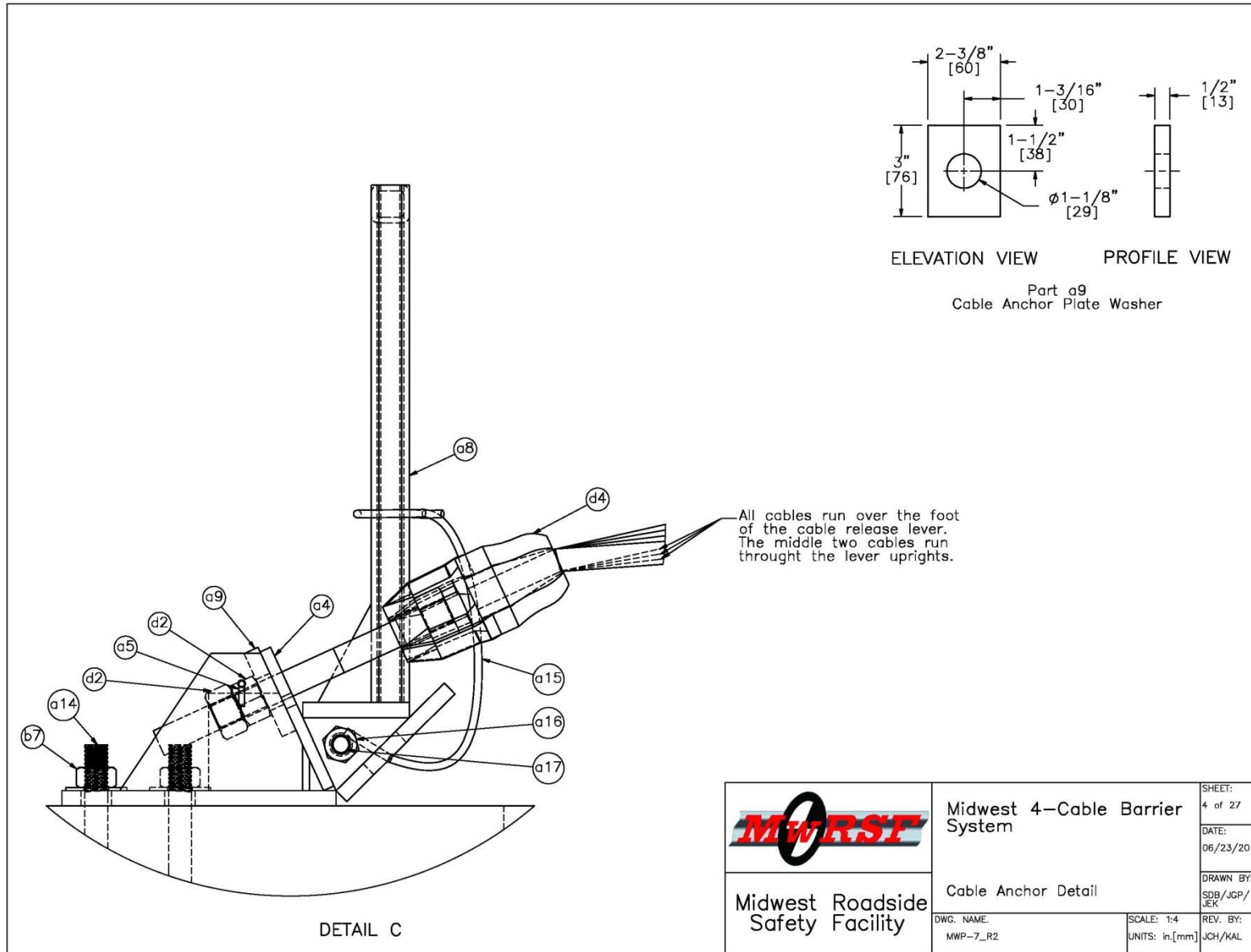


Figure 114. Cable Anchor Detail, Test No. MWP-7

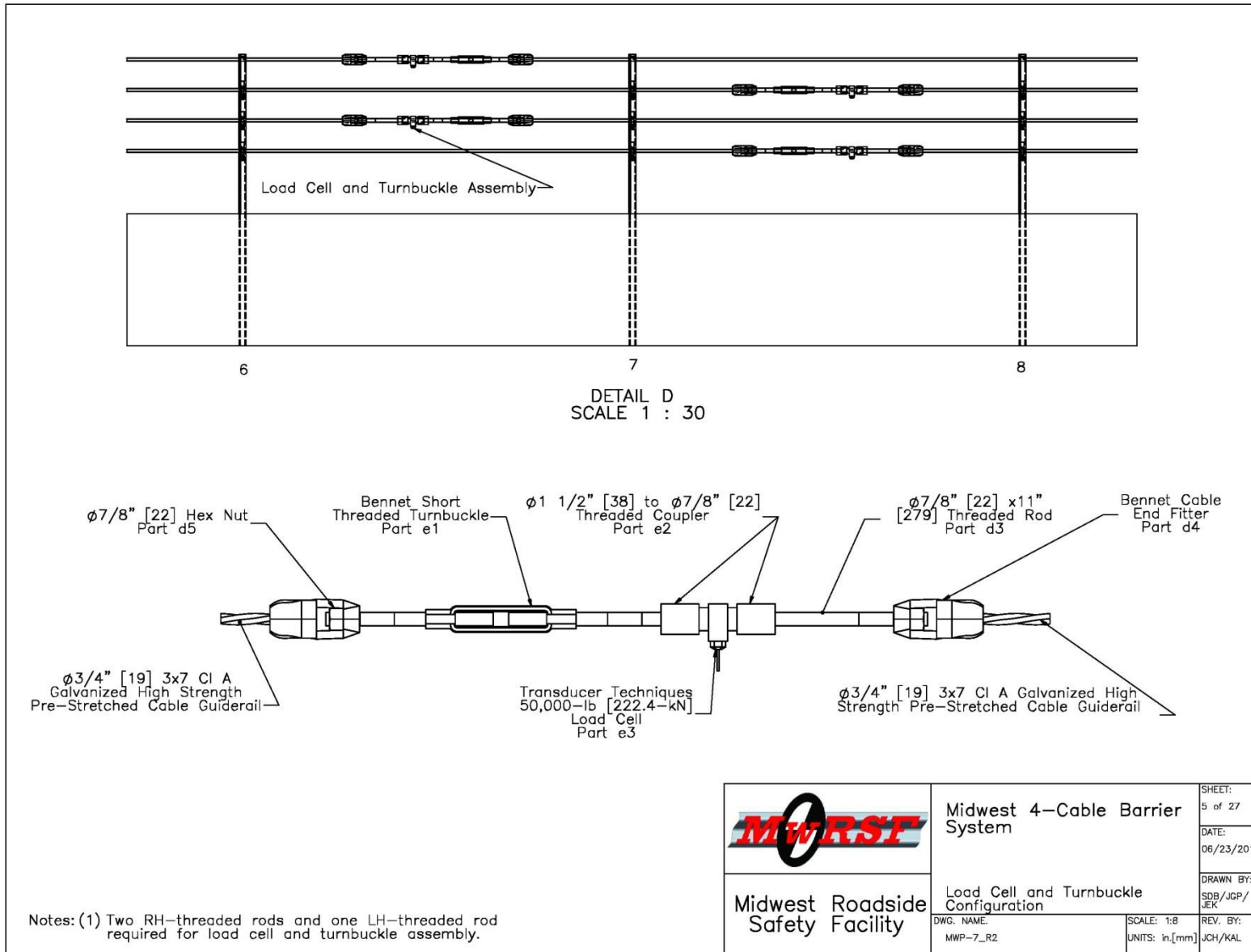


Figure 115. Load Cell and Turnbuckle Configuration, Test No. MWP-7

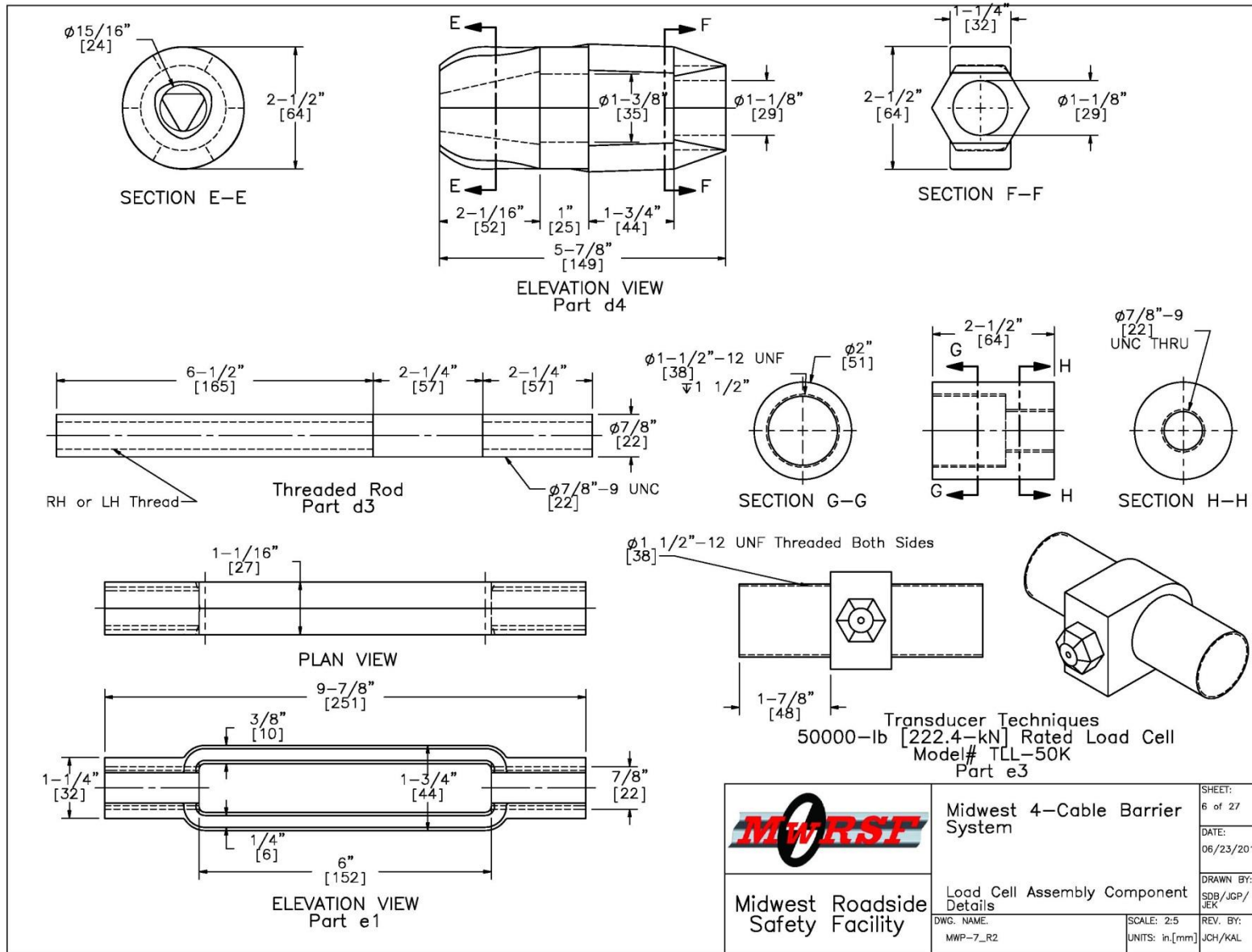


Figure 116. Load Cell Assembly Details, Test No. MWP-7

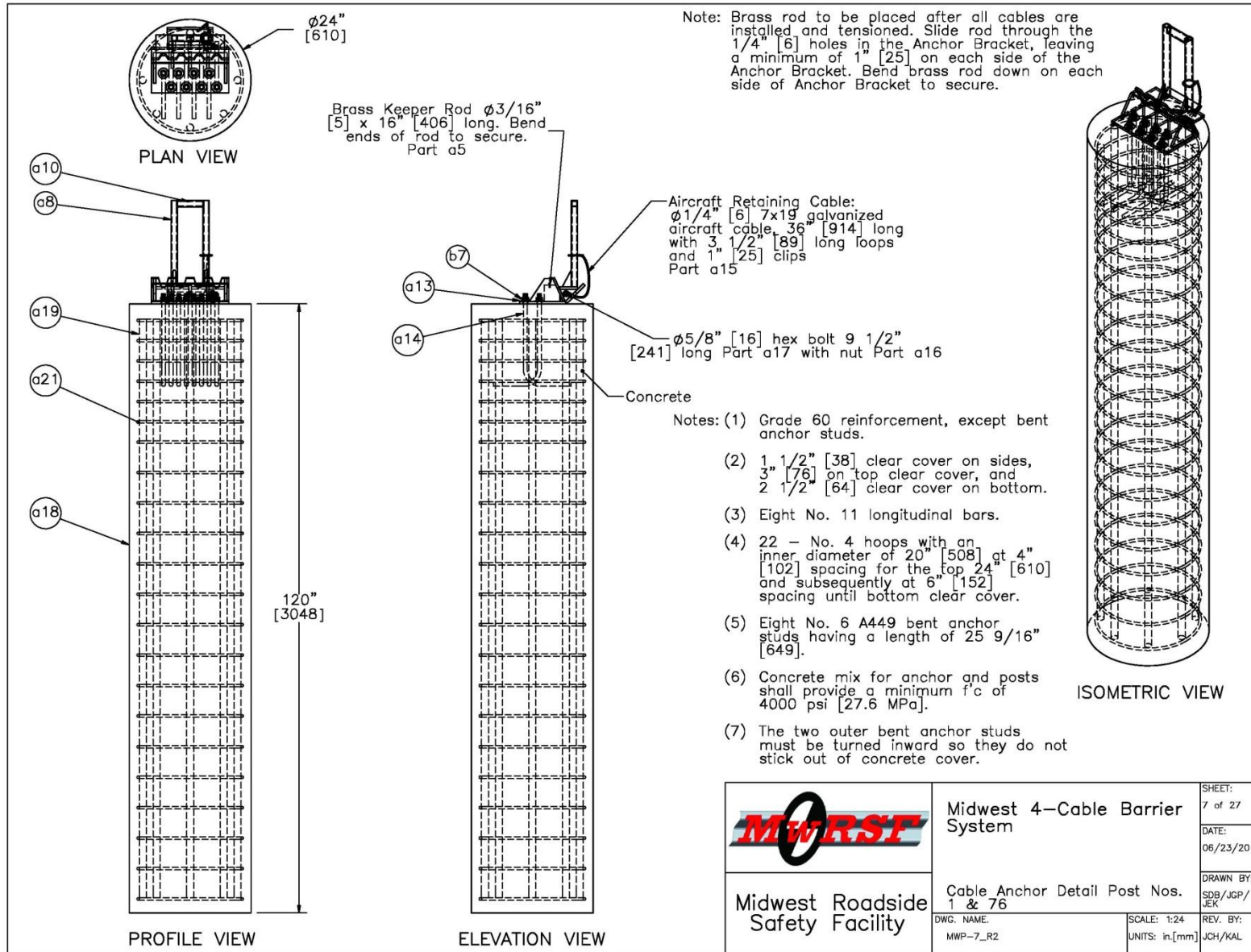


Figure 117. Cable Anchor Foundation, Post Nos. 1 and 76, Test No. MWP-7

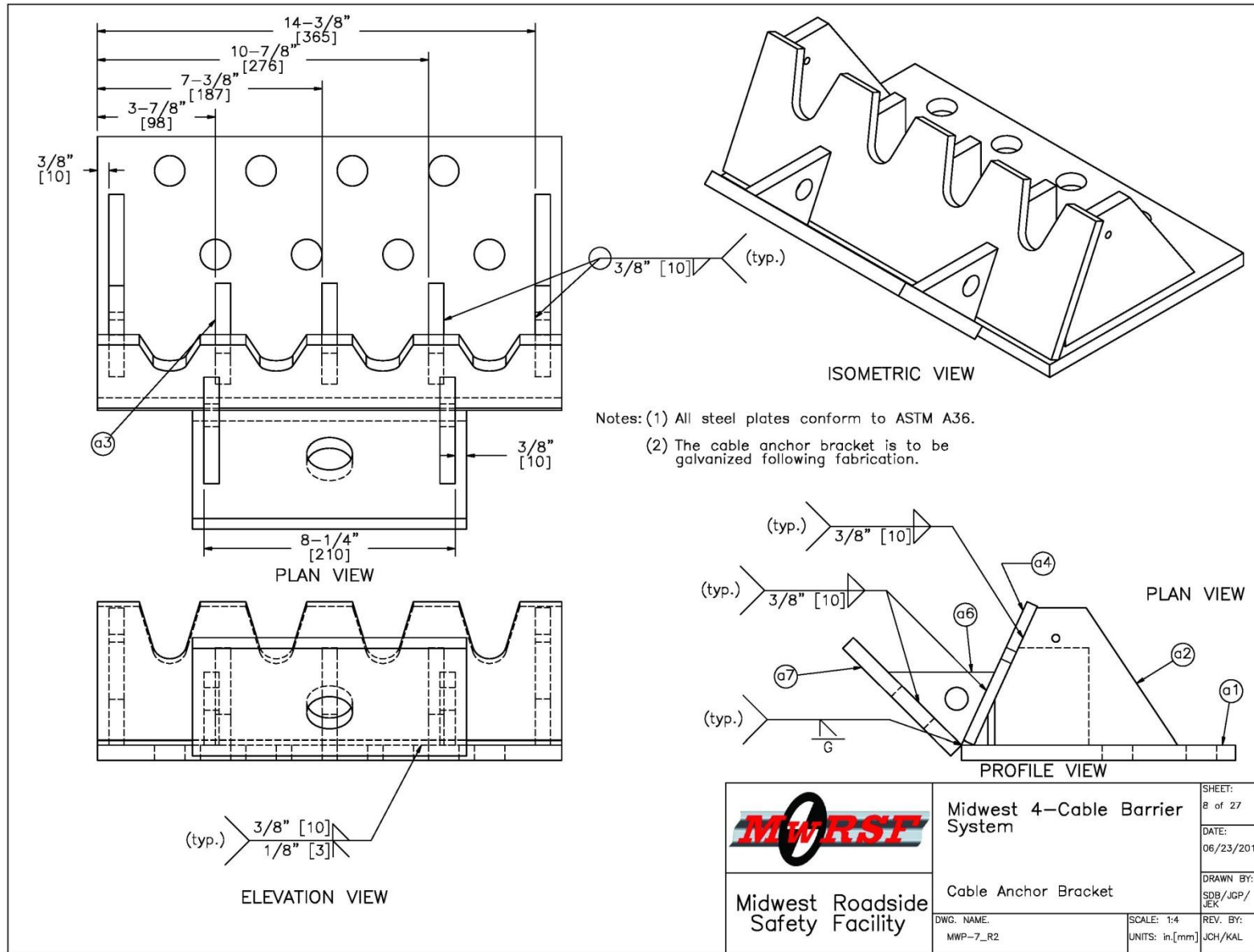
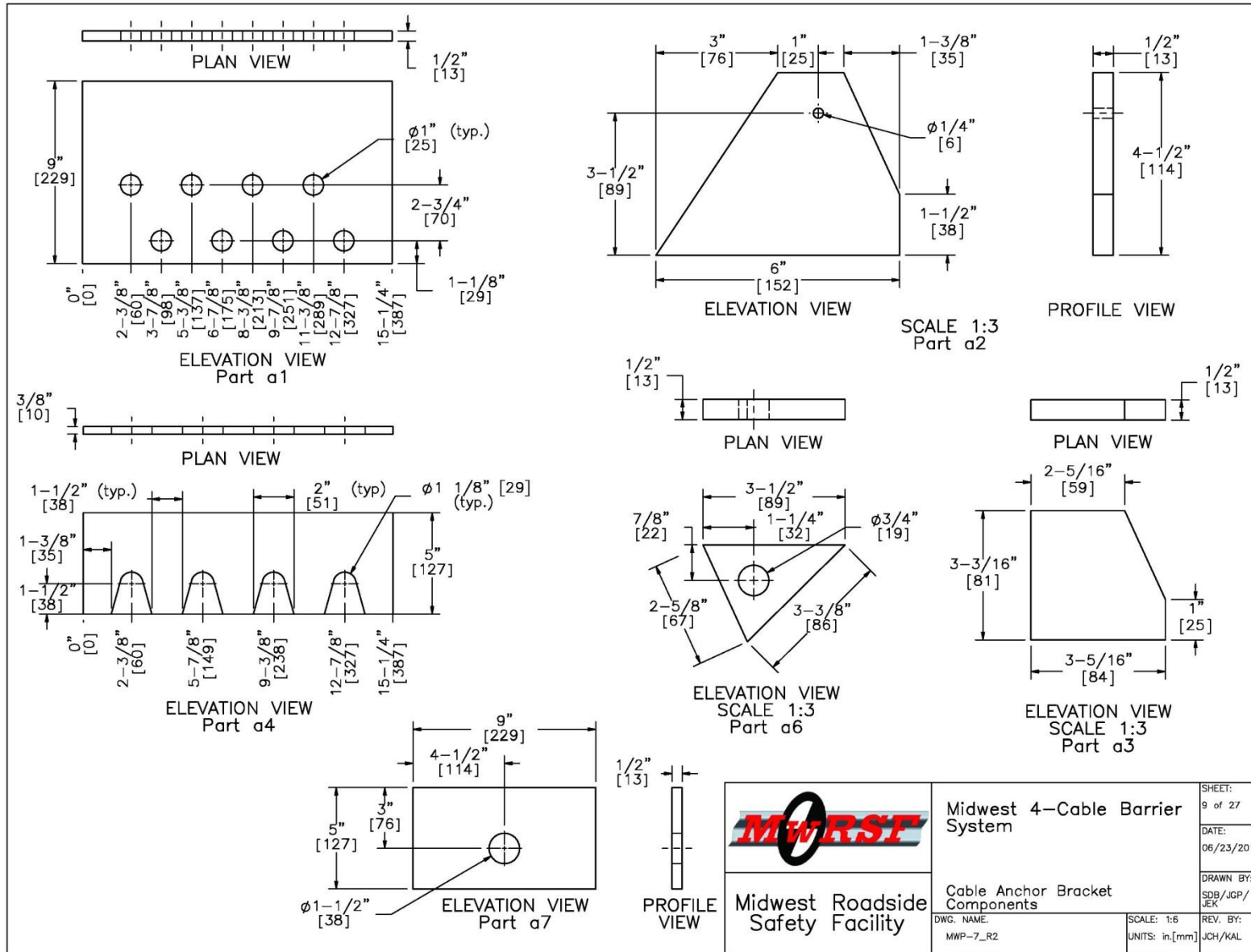


Figure 118. Cable Anchor Bracket, Test No. MWP-7



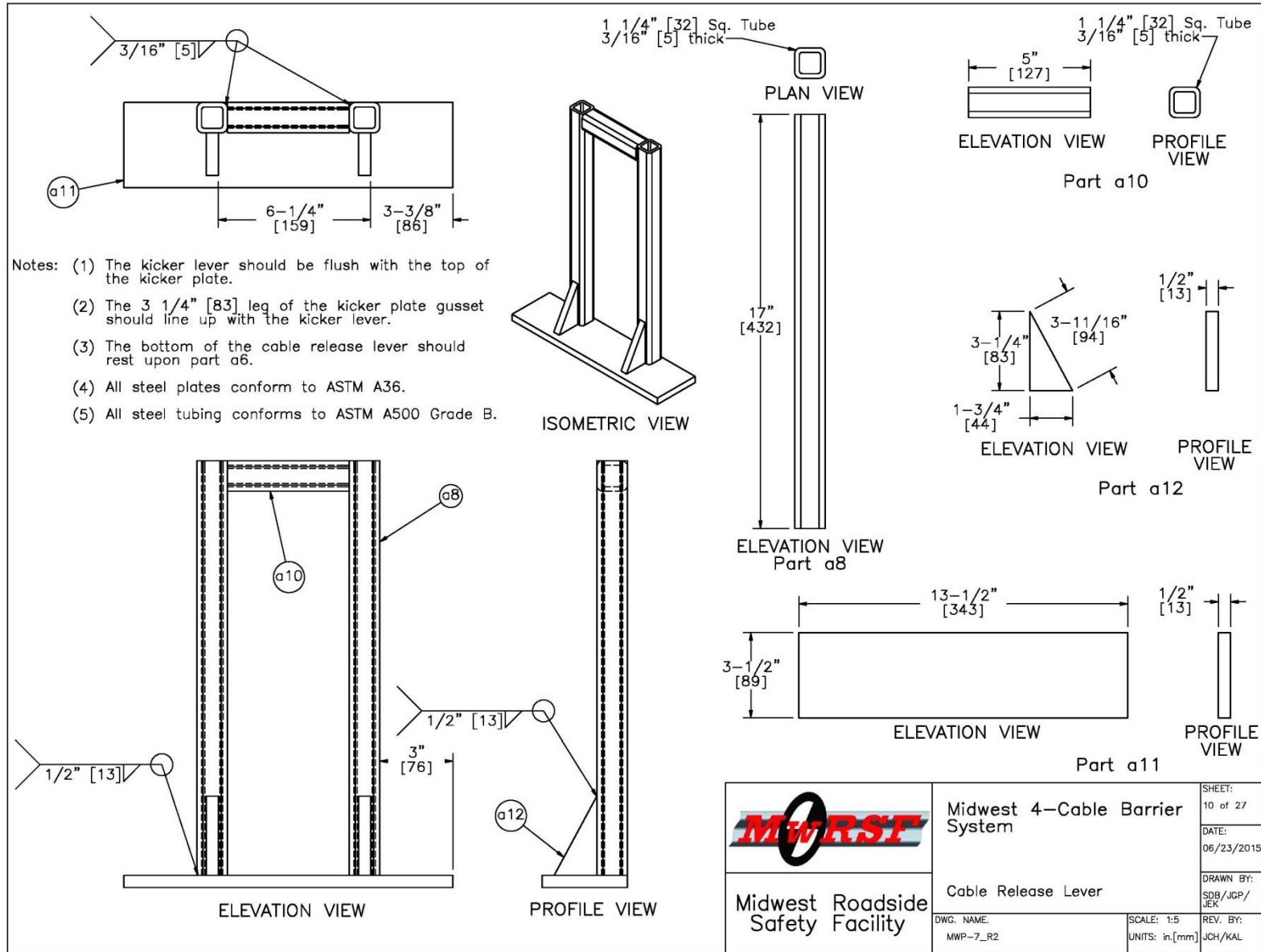


Figure 120. Cable Release Lever, Test No. MWP-7

	Midwest 4-Cable Barrier System	SHEET: 10 of 27 DATE: 06/23/2015
	Cable Release Lever	DRAWN BY: SDB/JGP/JEK REV. BY: JCH/KAL
Midwest Roadside Safety Facility	DWG. NAME: MWP-7_R2 SCALE: 1:5 UNITS: in,[mm]	REV. BY: JCH/KAL

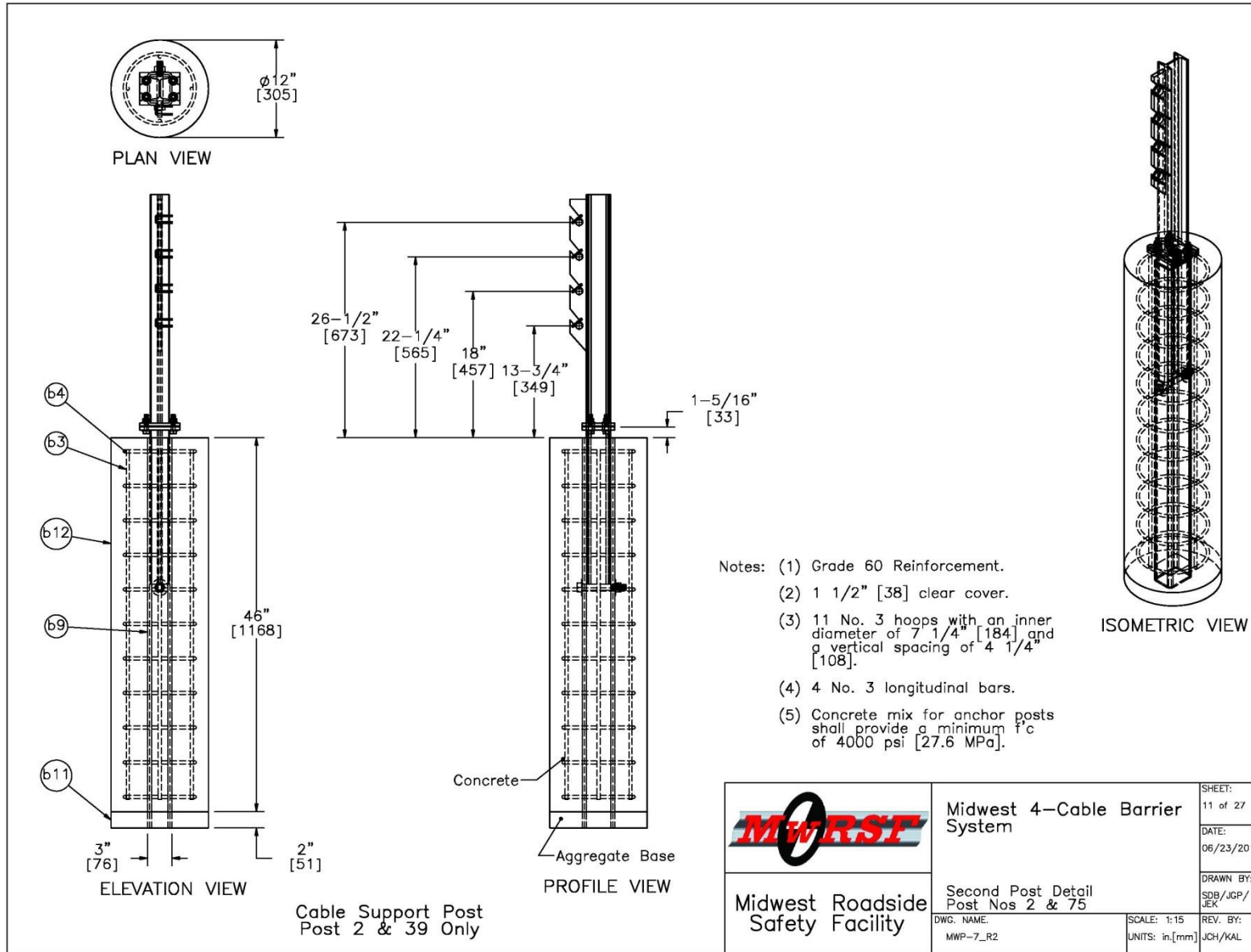


Figure 121. Second Post Details, Post Nos. 2 and 75, Test No. MWP-7

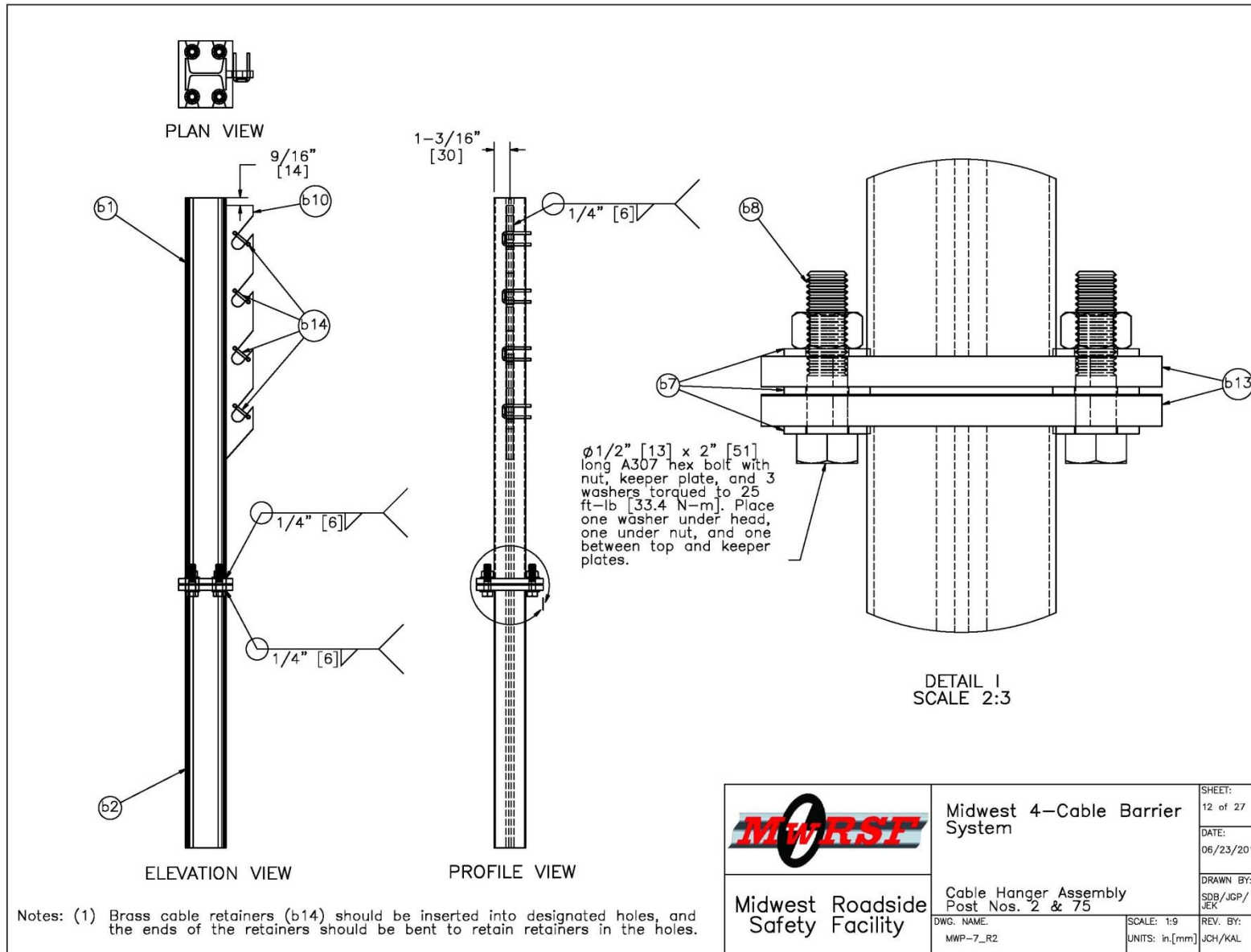


Figure 122. Cable Hanger Assembly, Post Nos. 2 and 75, Test No. MWP-7

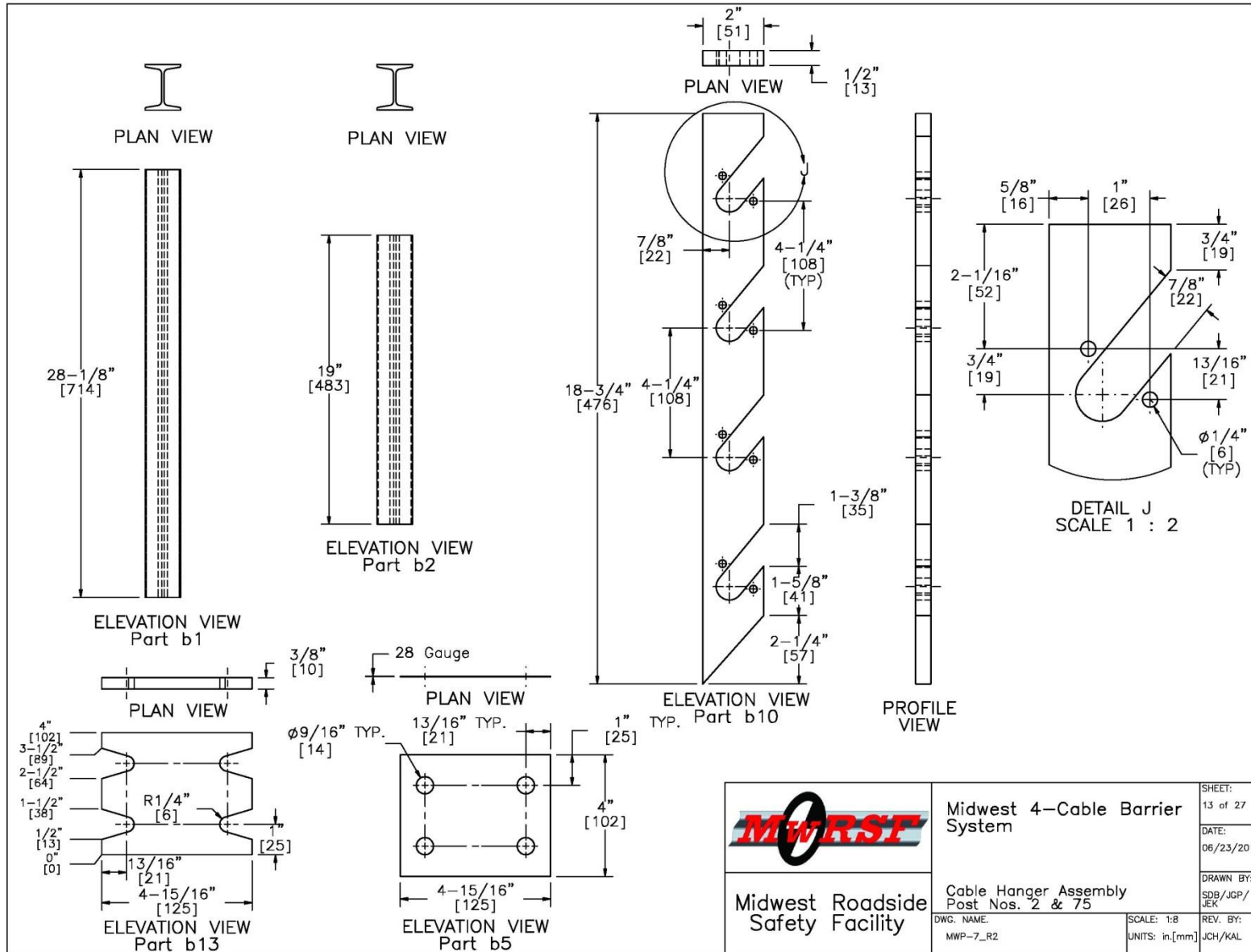


Figure 123. Cable Hanger Assembly, Post Nos. 2 and 75, Test No. MWP-7

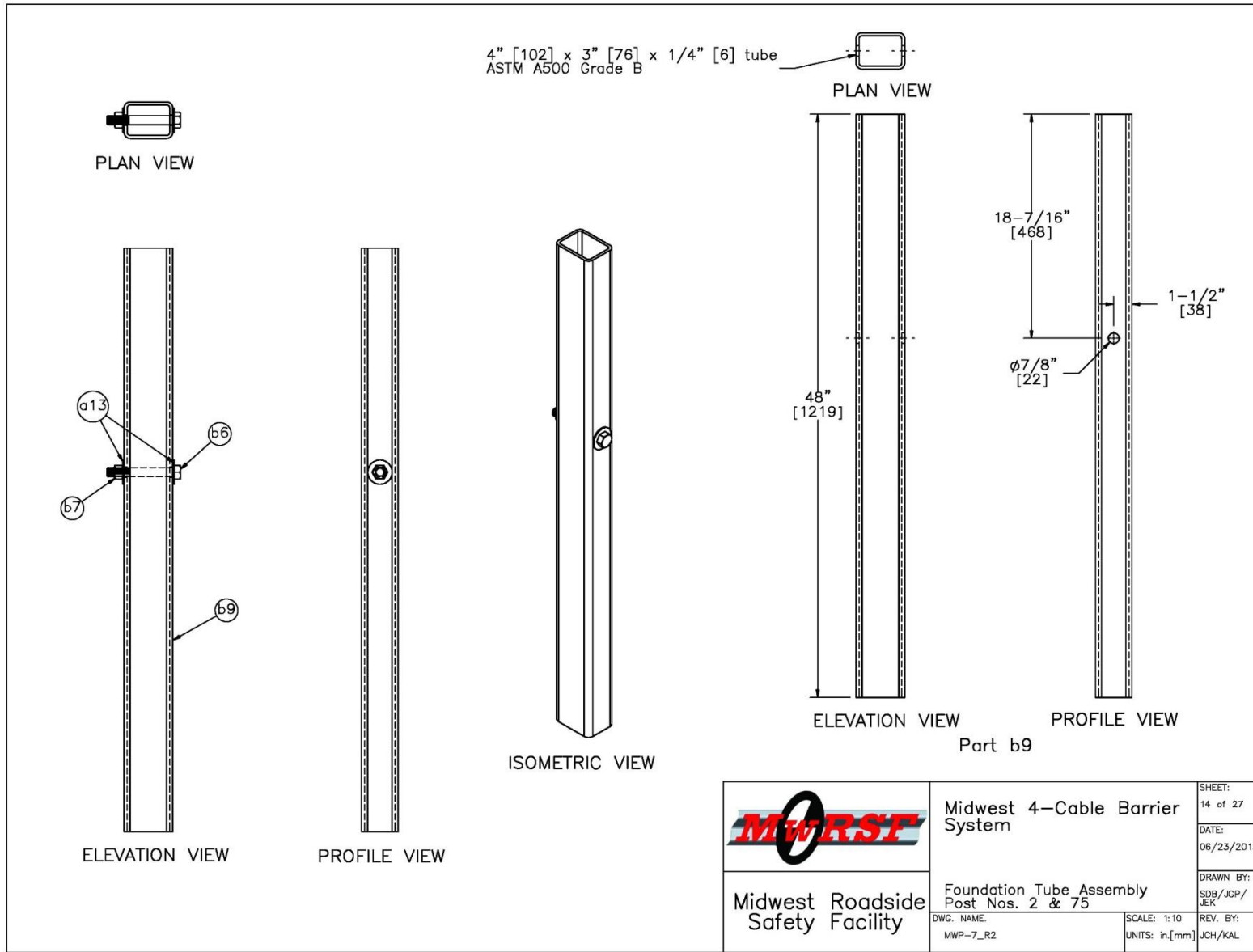
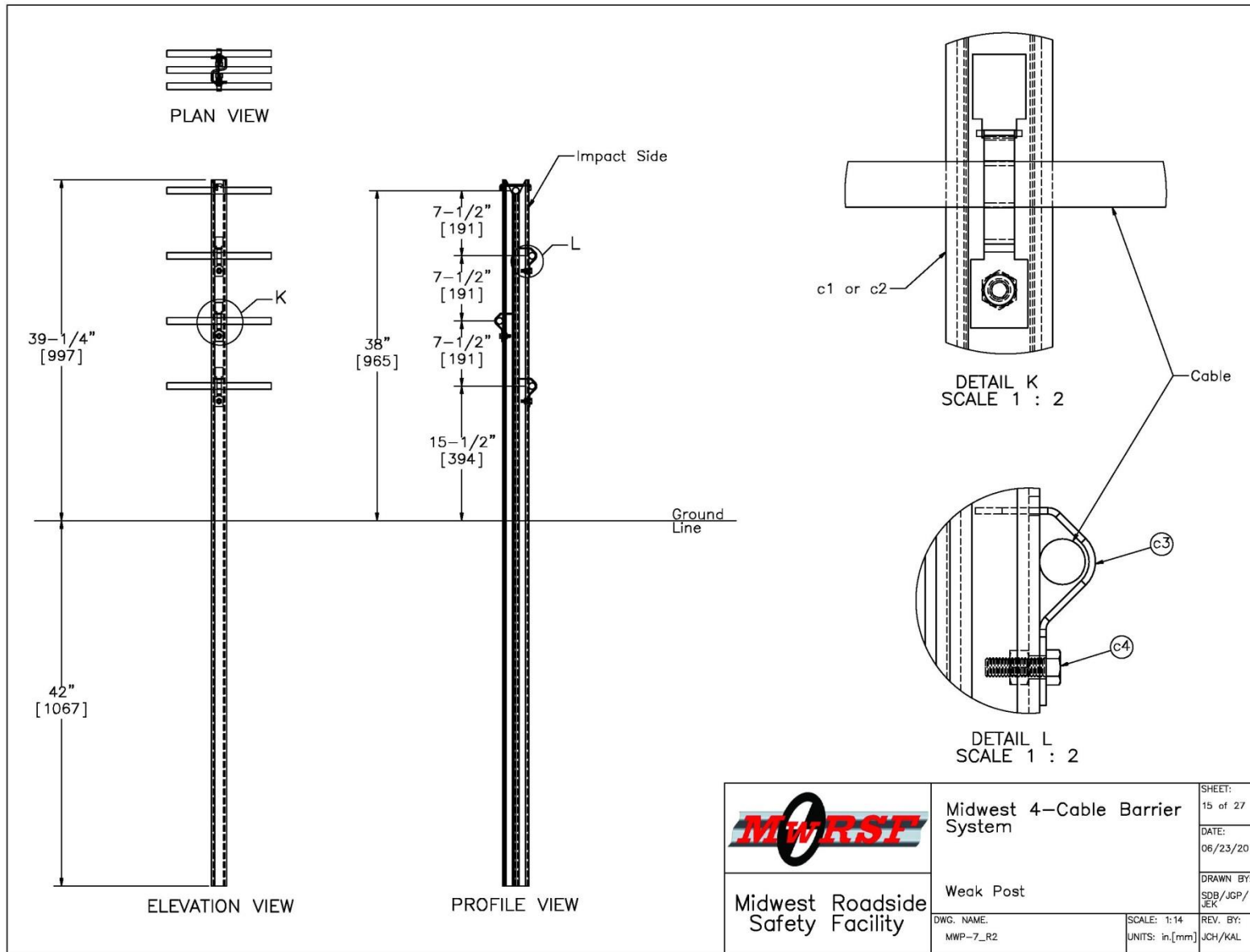


Figure 124. Foundation Tube Assembly, Post Nos. 2 and 75, Test No. MWP-7




	Midwest 4-Cable Barrier System		SHEET: 15 of 27
	Week Post		DATE: 06/23/2015
Midwest Roadside Safety Facility	DWG. NAME: MWP-7_R2	SCALE: 1:14 UNITS: in,[mm]	DRAWN BY: SDB/JGP/JEK REV. BY: JCH/KAL

Figure 125. MWP Z-Post Details, Test No. MWP-7

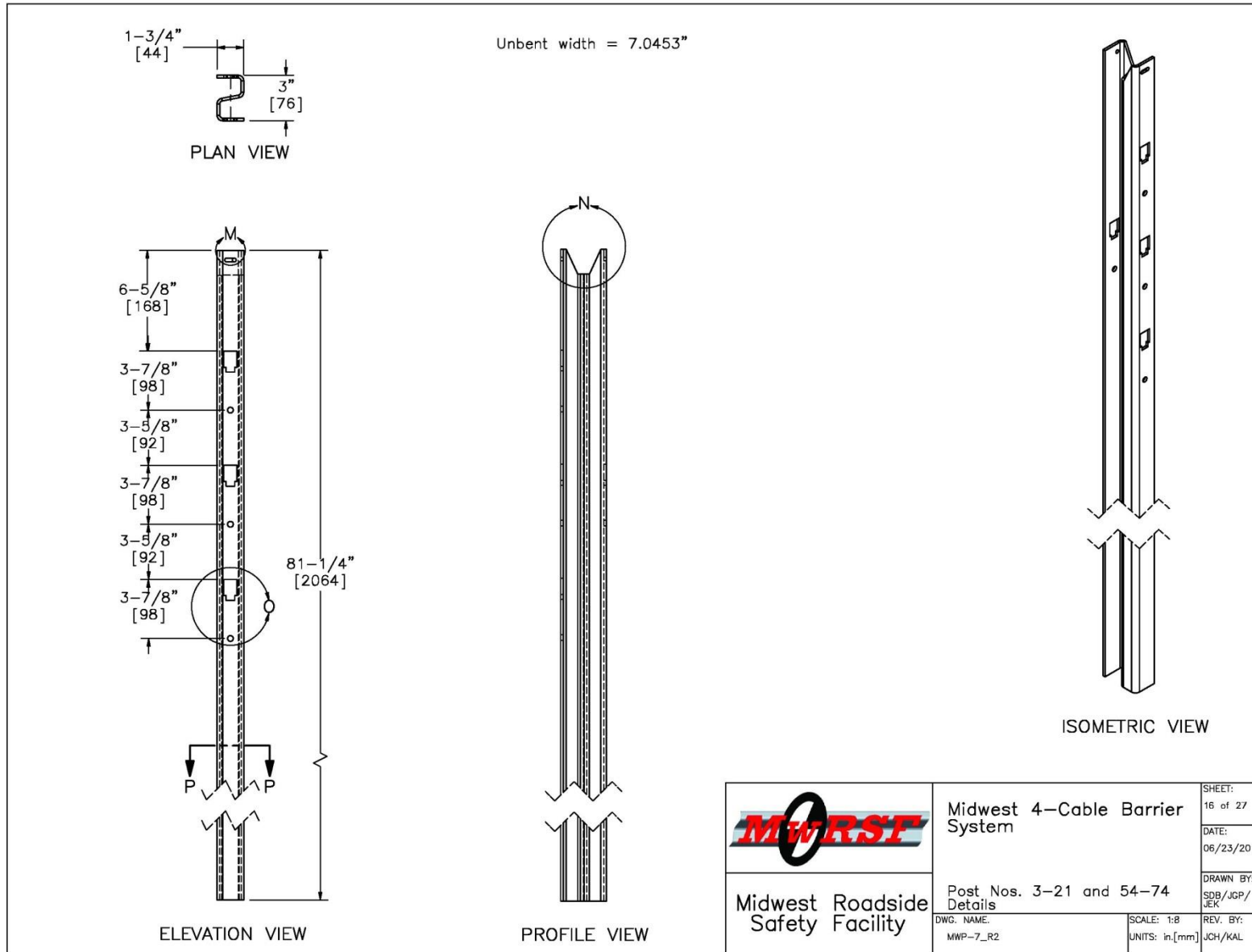


Figure 126. MWP Z-Post Details, Post Nos. 3 through 26 and 48 through 74, Test No. MWP-7

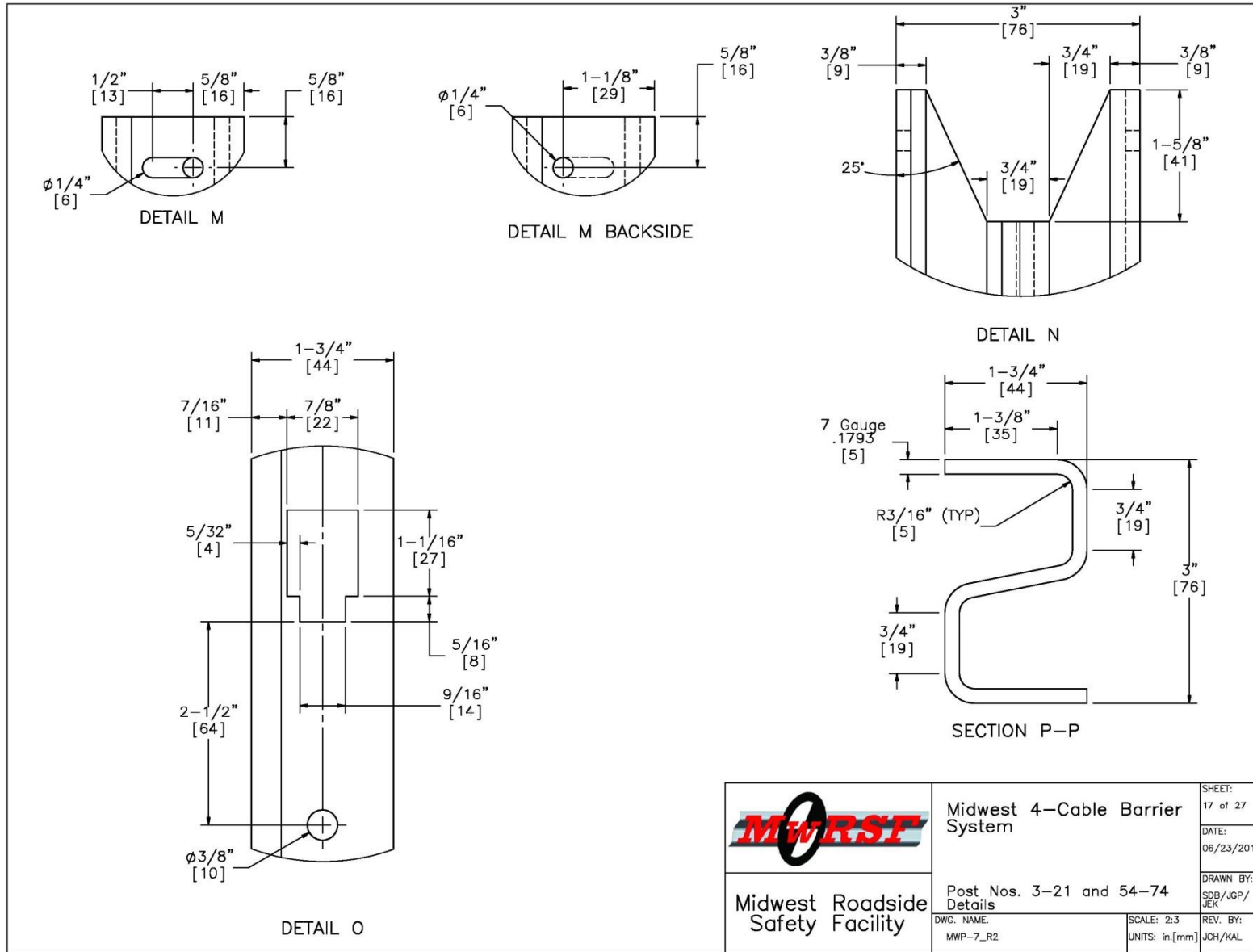


Figure 127. MWP Z-Post Details, Post Nos. 3 through 26 and 48 through 74, Test No. MWP-7

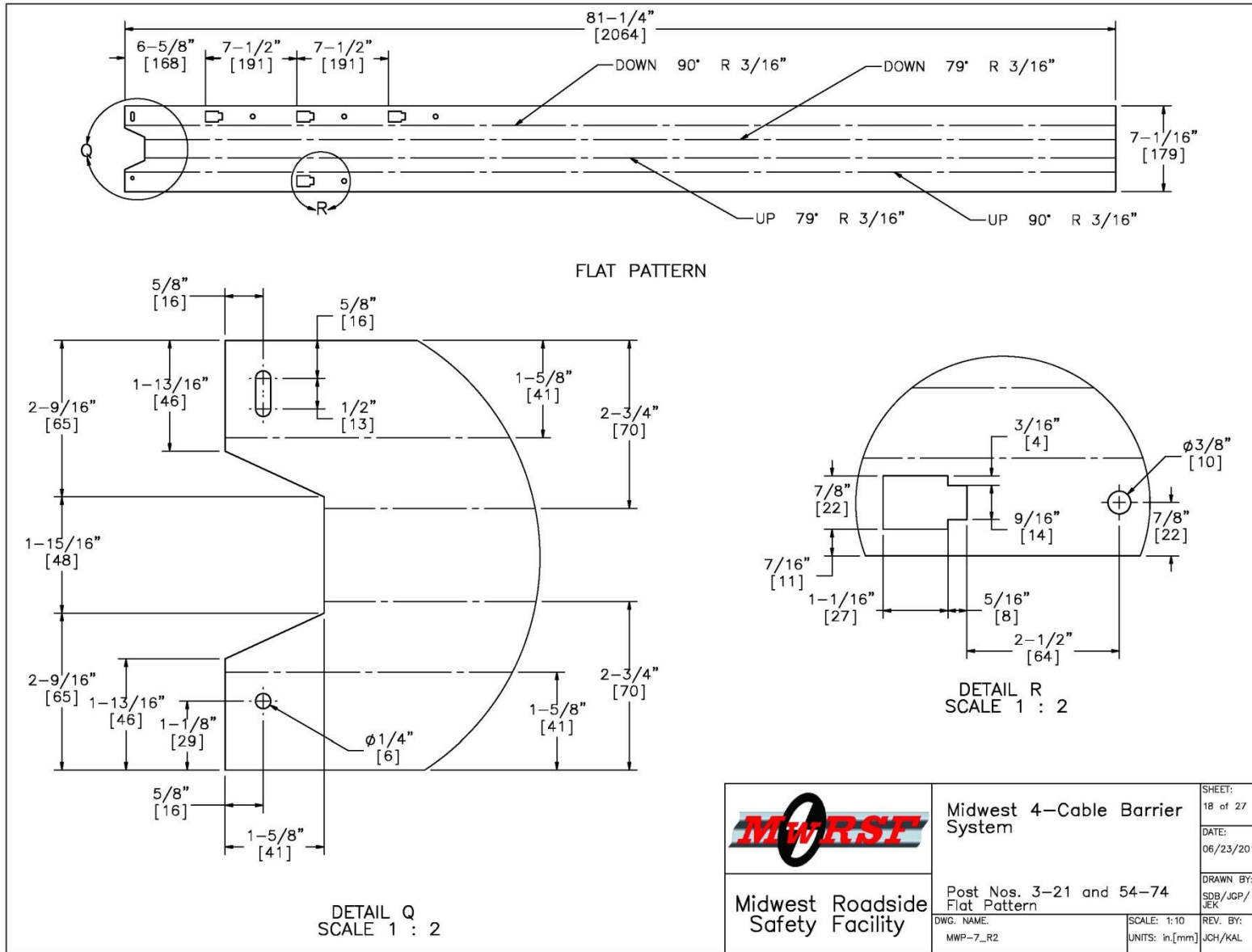


Figure 128. MWP Z-Post Details, Flat Pattern, Post Nos. 3 through 26 and 48 through 74, Test No. MWP-7

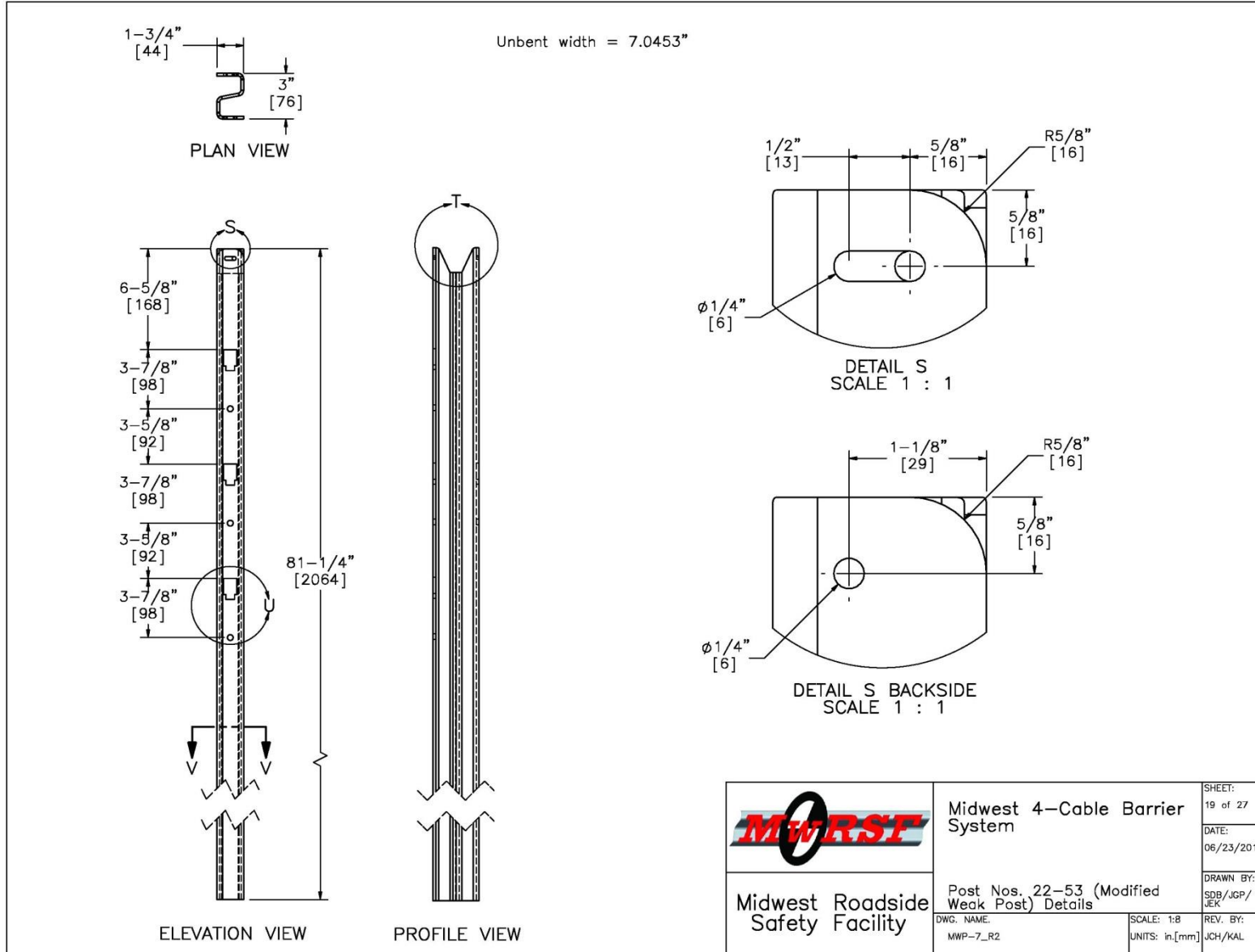


Figure 129. MWP Z-Post Details, Post Nos. 27 through 47, Test No. MWP-7

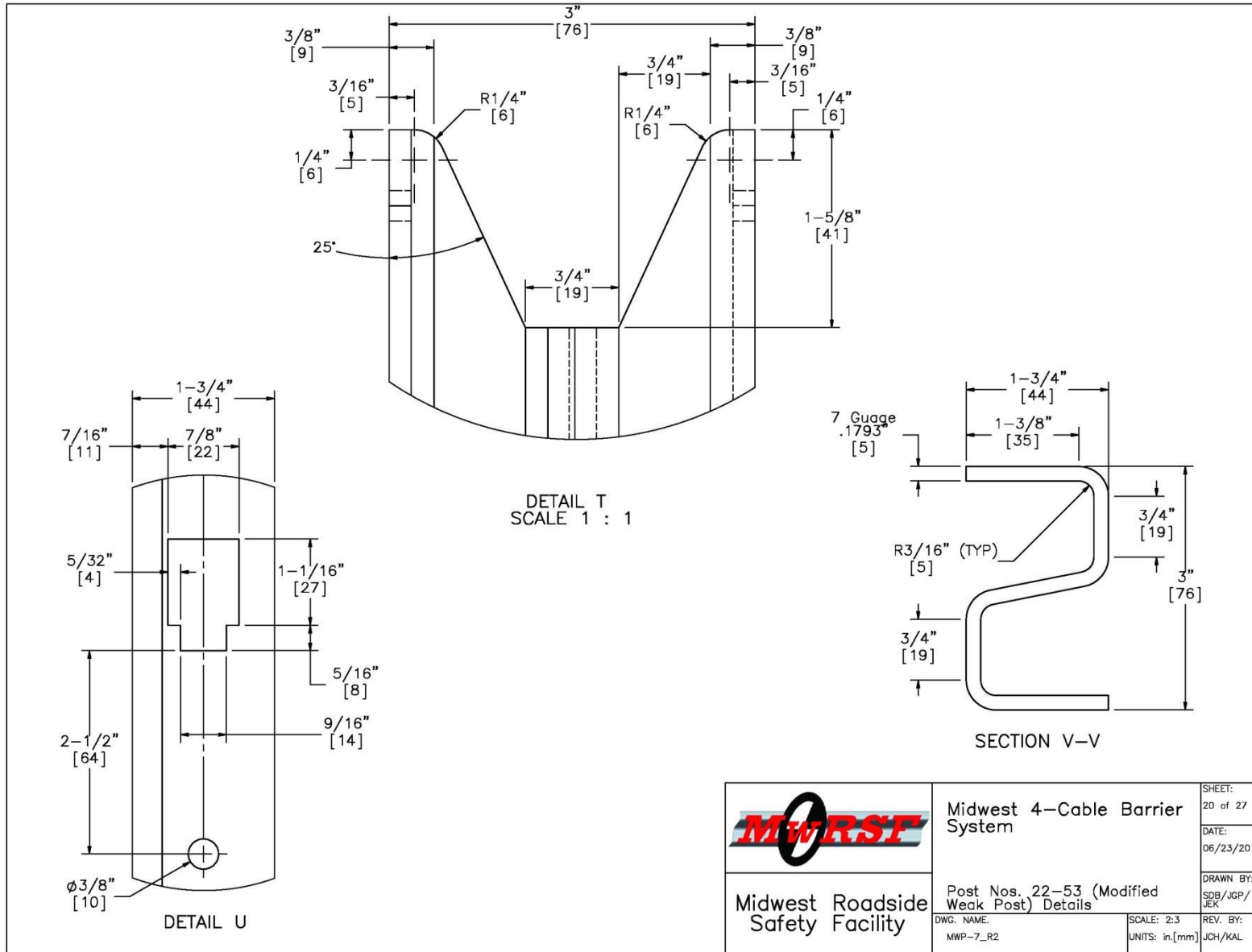


Figure 130. MWP Z-Post Details, Post Nos. 27 through 47, Test No. MWP-7

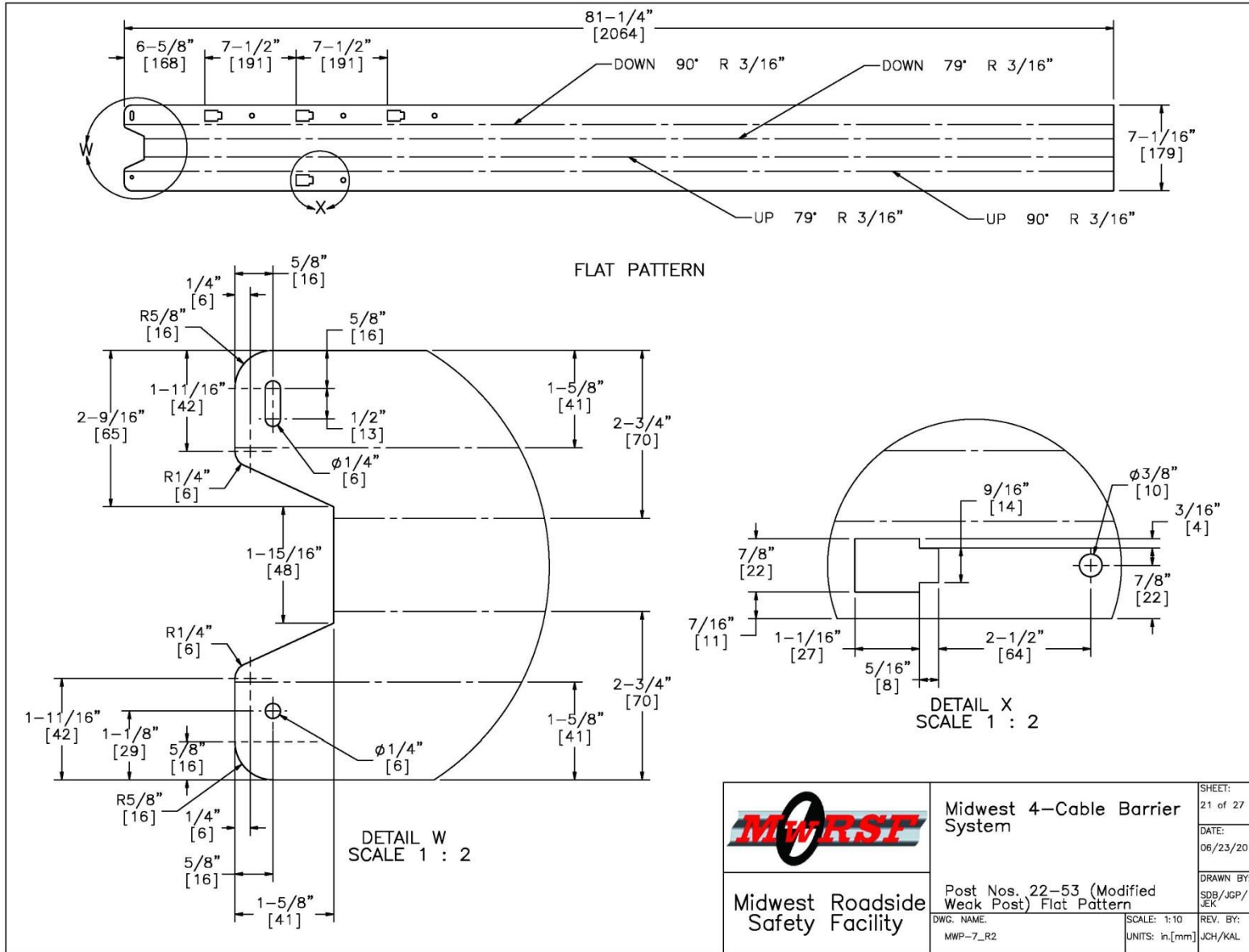


Figure 131. MWP Z-Post Details, Flat Pattern, Post Nos. 27 through 47, Test No. MWP-7

	Midwest 4-Cable Barrier System	SHEET: 21 of 27
	Midwest Roadside Safety Facility	DATE: 06/23/2015
DWG. NAME: MWP-7_R2	Post Nos. 22-53 (Modified Weak Post) Flat Pattern	DRAWN BY: SDB/JGP/JEK
UNITS: in,[mm]	SCALE: 1:10	REV. BY: JCH/KAL

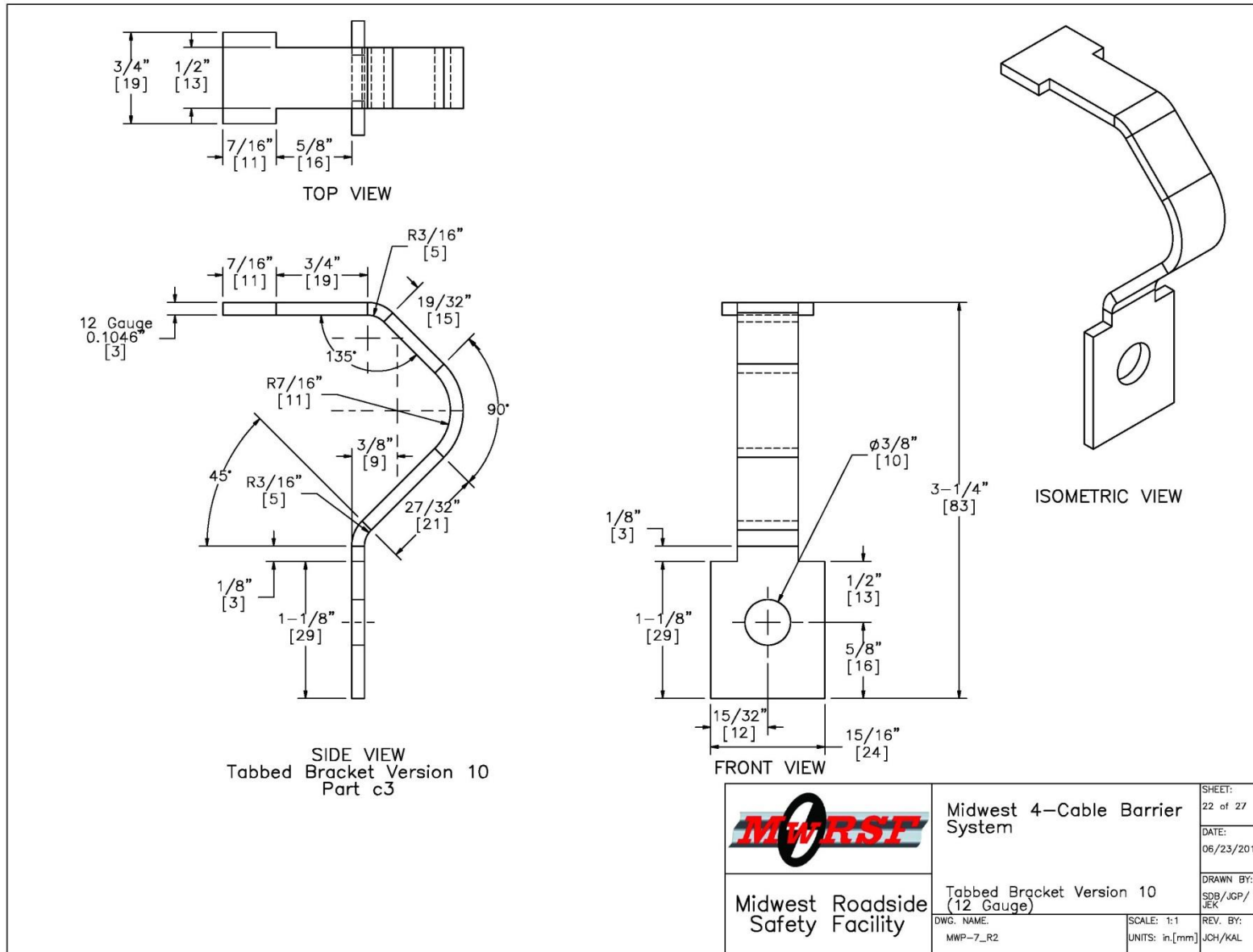


Figure 132. Tabbed Bracket Details, 12-Gauge, Test No. MWP-7

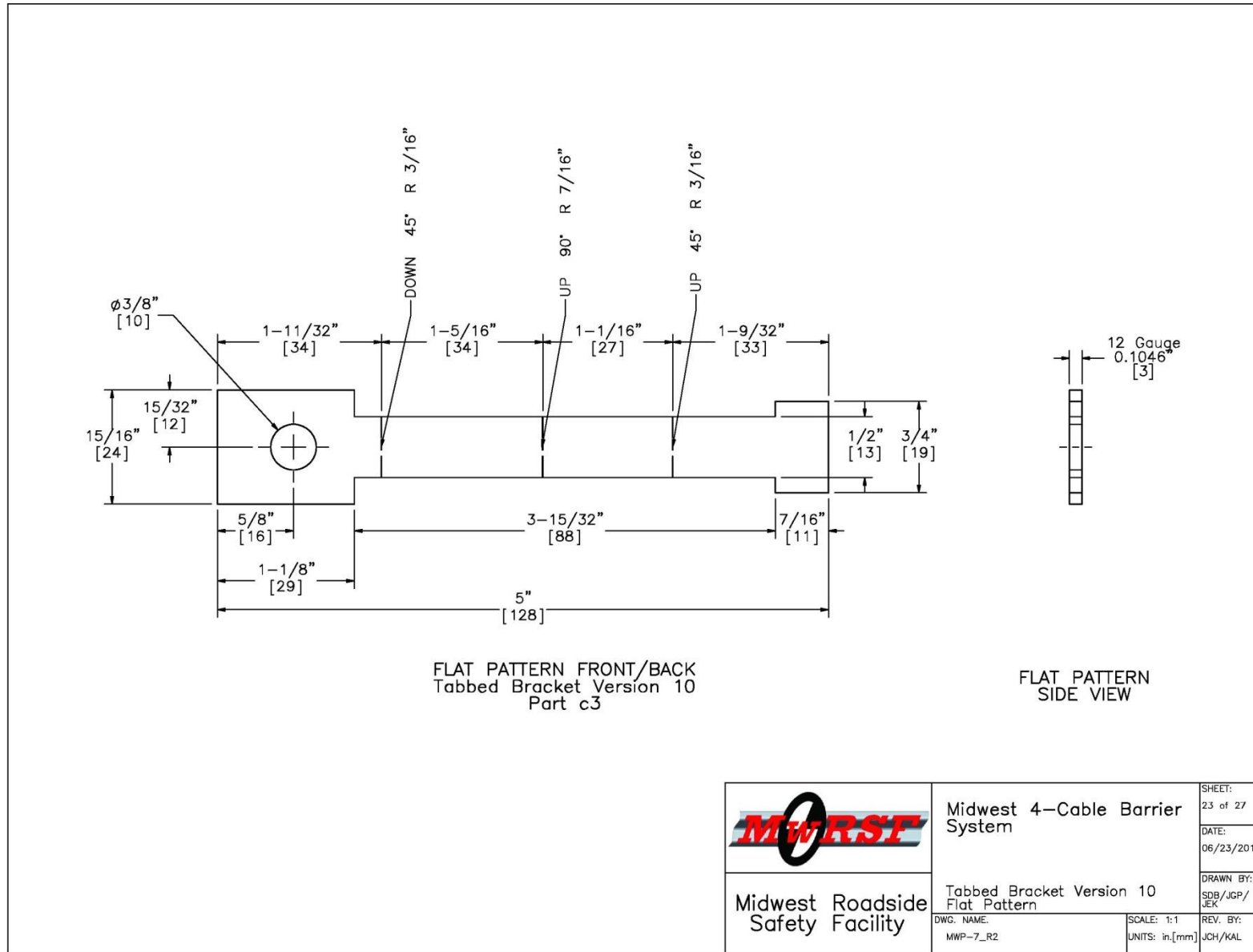


Figure 133. Tabbed Bracket Details, Flat Pattern, Test No. MWP-7

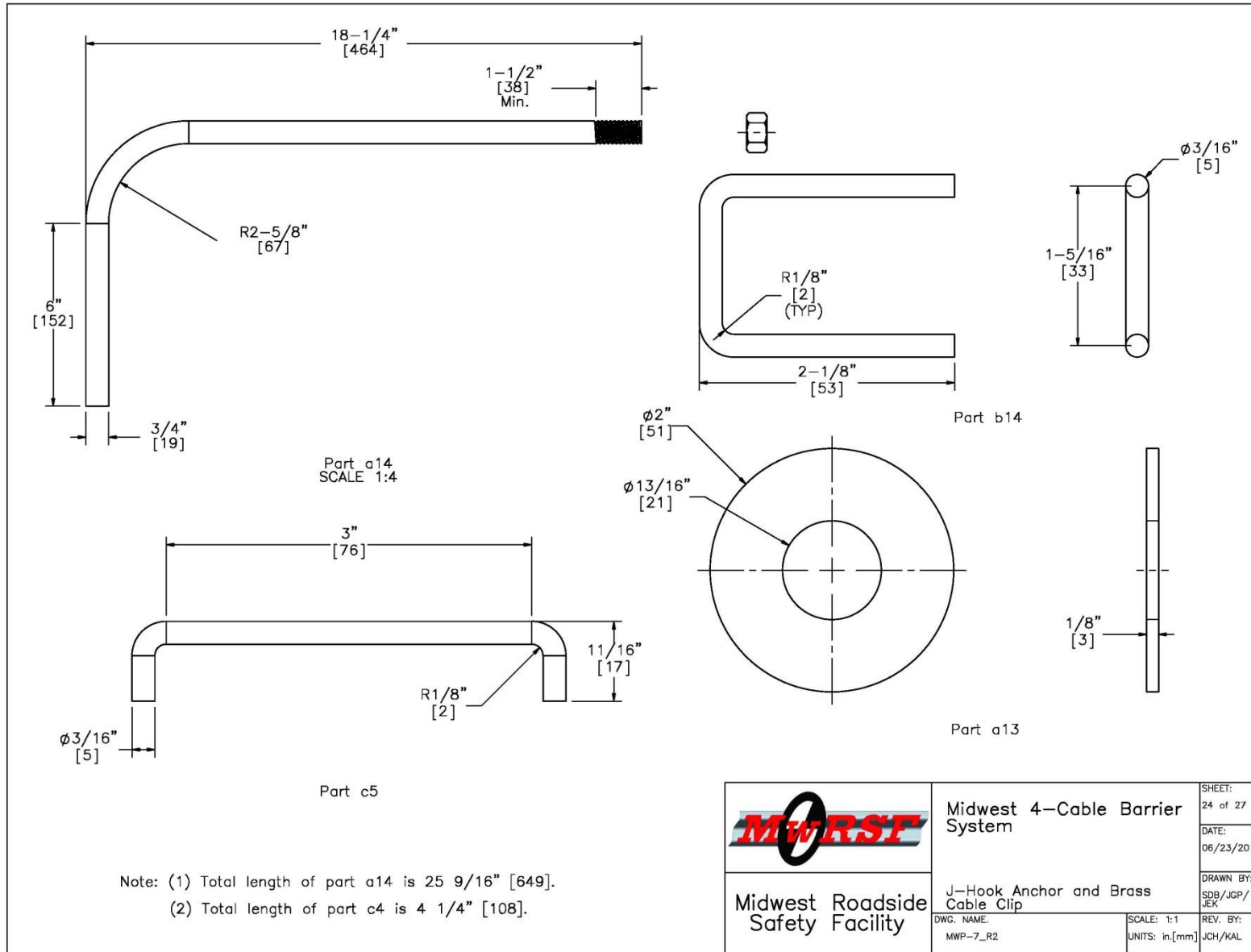


Figure 134. J-Hook Anchor and Brass Clips, Test No. MWP-7

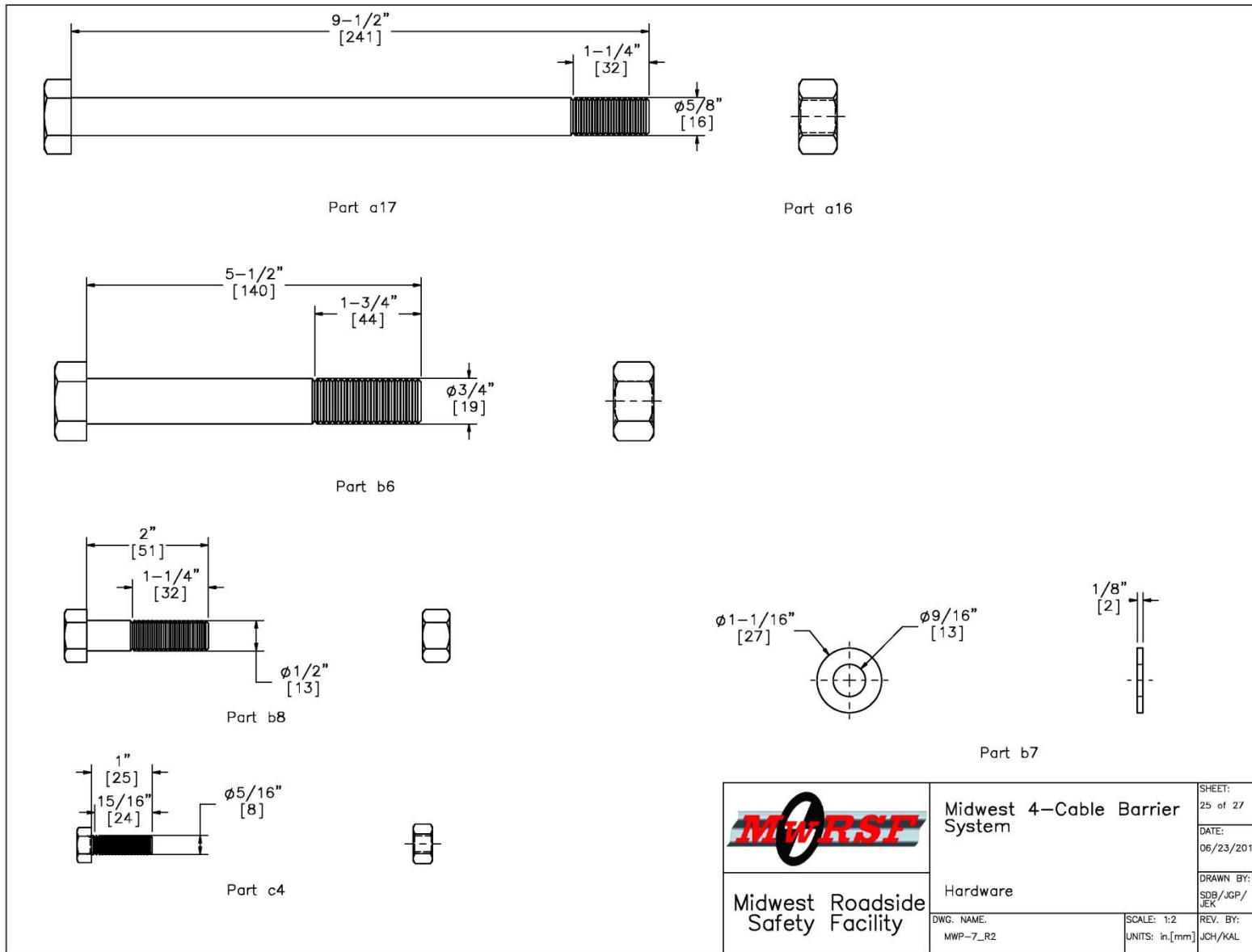


Figure 135. Hardware Details, Test No. MWP-7

Item No.	QTY.	Description	Material Specification
a1	2	Cable Anchor Base Plate	ASTM A36
a2	4	Exterior Cable Plate Gusset	ASTM A36
a3	6	Interior Cable Plate Gusset	ASTM A36
a4	2	Anchor Bracket Plate	ASTM A36
a5	2	3/16" [5] Dia. Brass Keeper Rod, 14" [356] long	Brass
a6	4	Release Gusset	A36 Steel
a7	2	Release Lever Plate	A36 Steel
a8	4	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Tube	ASTM A500 Gr. B
a9	8	CMB High Tension Anchor Plate Washer	ASTM A36
a10	2	1.25x1.25x0.1875" [32x32x5] TS CT Kicker Lever Connecting Tube	ASTM A 500 Gr. B
a11	2	3x10x0.5" [76x254x13] Kicker Plate	ASTM A36
a12	4	CT kicker - gusset	ASTM A36
a13	20	3/4" [19] Dia. Flat Washer	ASTM F844
a14	16	3/4" [19] Dia. UNC J-Hook Anchor and Hex Nut	J-Hook ASTM A449/Nut ASTM A563 DH
a15	2	1/4" [6] Dia. Aircraft Retaining Cable, 36" [914] long	7x19 Galv.
a16	2	5/8" [16] Dia. Heavy Hex Nut	ASTM A563C
a17	2	5/8" [16] Dia. UNC, 9 1/2" [241] Long Hex Bolt	ASTM A449 or SAE J429 Gr. 5
a18	2	24" [610] Dia. Concrete Anchor, 120" [3048] long	4,000 psi f'c
a19	16	#11 Straight Rebar, 114" [2896] long	Grade 60
a20	44	#4 Anchor Hoop Rebar with 21" [533] Dia.	Grade 60
b1	2	S3x5.7 [S76x8.5] Post by 28 1/8" [714]	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A
b2	2	S3x5.7 [S76x8.5] Post by 19" [483]	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A
b3	8	#3 Straight Rebar, 43" [1092] long	Grade 60
b4	22	7 1/4" [184] Dia. No. 3 Hoop Reinforcement	Grade 60
b5	2	2nd Post Keeper Plate, 28 Gauge	ASTM A36
b6	2	3/4" [19] Dia. UNC, 5 1/2" [140] Long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b7	24	1/2" [13] Dia. Washer with 1 1/16" [27] OD	ASTM F844
b8	8	1/2" [13] Dia. UNC, 2" [51] long Hex Bolt and Nut	Bolt ASTM A307 Gr. A/Nut ASTM A563A
b9	2	4x3x1/4" [102x76x6] Foundation Tube, 48" [1168] long	ASTM A500 Grade B
b10	2	2nd Post Cable Hanger	ASTM A36
b11	2	2nd Post Anchor Aggregate 12 in, Depth	-
b12	2	12" Dia. 2nd Post Concrete Anchor, 46" long	4,000 psi f'c
b13	4	2nd Post Base Plate	ASTM A36
b14	8	3/16" [5] Dia. 5 1/4" [133] Long Brass Rod	ASTM B16-00


 Midwest Roadside Safety Facility	Midwest 4-Cable Barrier System	SHEET: 26 of 27
	Bill of Materials	DATE: 06/23/2015
DWG. NAME: MWP-7_R2	SCALE: NONE UNITS: in.[mm]	DRAWN BY: SDB/JGP/ JEK
		REV. BY: JCH/KAL

Figure 136. Bill of Materials, Test No. MWP-7

Item No.	QTY.	Description	Material Spec
c1	40	3"x1-3/4"x7 Gauge [76x44x4.6], 81 1/4" [2064] Long Bent MWP Z-Section Post	Hot-Rolled ASTM A1011 HSLA Gr. 50
c2	32	3"x1-3/4"x7 Gauge [76x44x4.6], 81 1/4" [2064] Long Bent MWP Z-Section Post (Modified)	Hot-Rolled ASTM A1011 HSLA Gr. 50
c3	216	12 Gauge Tabbed Bracket - Version 10	Hot-Rolled ASTM A1011 HSLA Grade 50
c4	216	5/16" [8] Dia. UNC, 1" [25] Long Hex Cap Screw and Nut	Bolt SAE J429 Gr. 5 or ASTM A449/Nut ASTM A563 DH
c5	72	Straight Rod - ϕ 3/16" [5] Cable Clip	ASTM B16 Brass C36000 Half Hard (H02), ROUND. TS \geq 68.0 ksi, YS \geq 52.0 ksi
d1	1	3/4" [19] Dia. 3x7 Cable Guiderail	AASHTO M30-92(2000)/ASTM A741-98 Type 1 Class A coating except with Type 1 minimum breaking strength = 39 kips [173.5 kN]
d2	16	7/8" [22] Dia. Hex Nut	ASTM A563C
d3	28	Cable End Threaded Rod	ASTM A449
d4	24	Bennet Cable End Fitter	ASTM A47
d5	24	7/8" [22] Dia. Hex Nut	SAE J429 Gr. 5
e1	8	Bennet Short Threaded Turnbuckle	Not Specified
e2	8	Threaded Load Cell Coupler	N/A
e3	4	50,000-lb [222.4-kN] Load Cell	N/A


	Midwest 4-Cable Barrier System	SHEET: 27 of 27
	DATE: 06/23/2015	
Midwest Roadside Safety Facility	Bill of Materials	DRAWN BY: SDB/JGP/JEK
	DWG. NAME: MWP-7_R2	SCALE: NONE UNITS: in,[mm]
		REV. BY: JCH/KAL

Figure 137. Bill of Materials, Test No. MWP-7



Figure 138. Test Installation Photographs, Test No. MWP-7

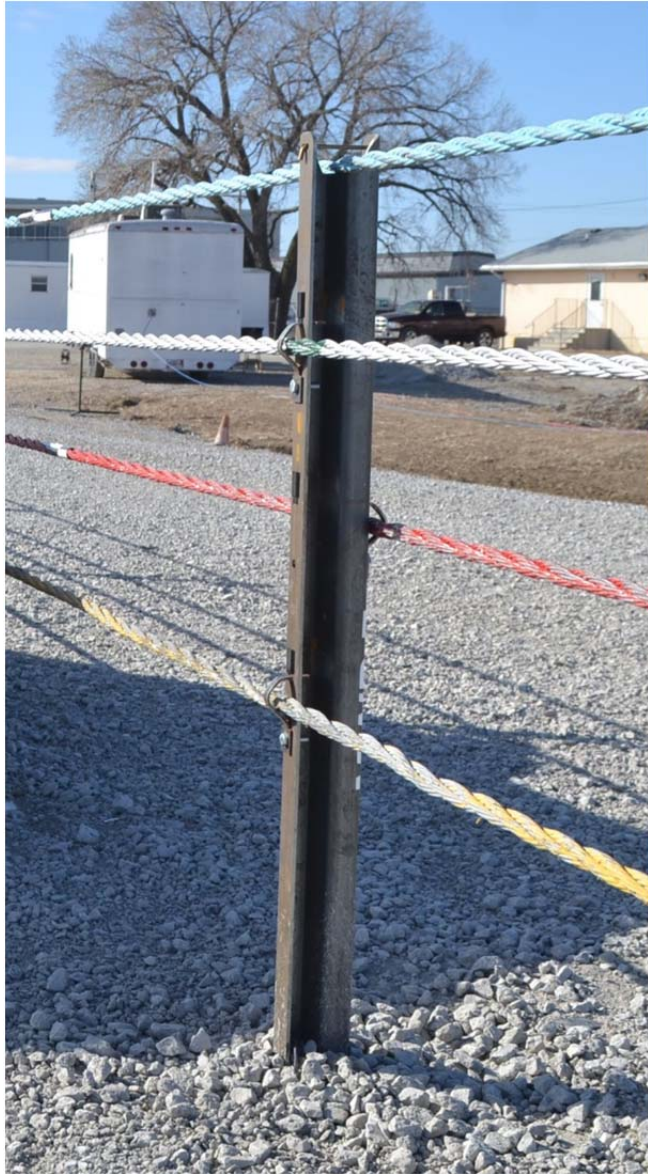


Figure 139. Test Installation Photographs, Test No. MWP-7

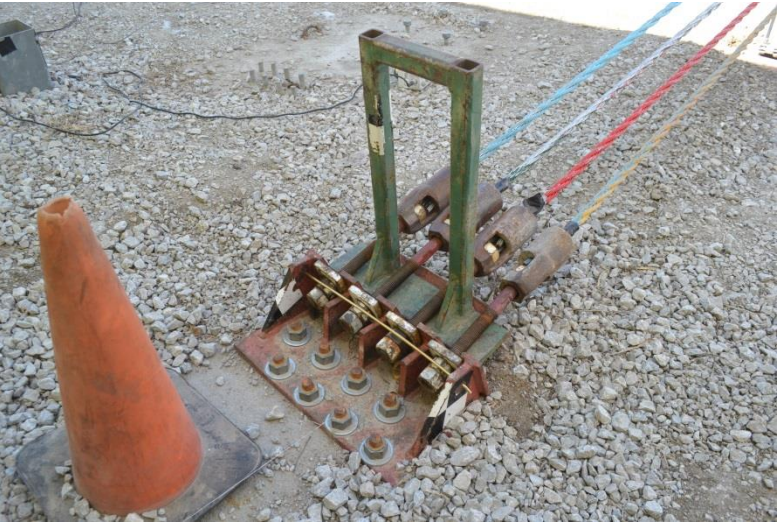
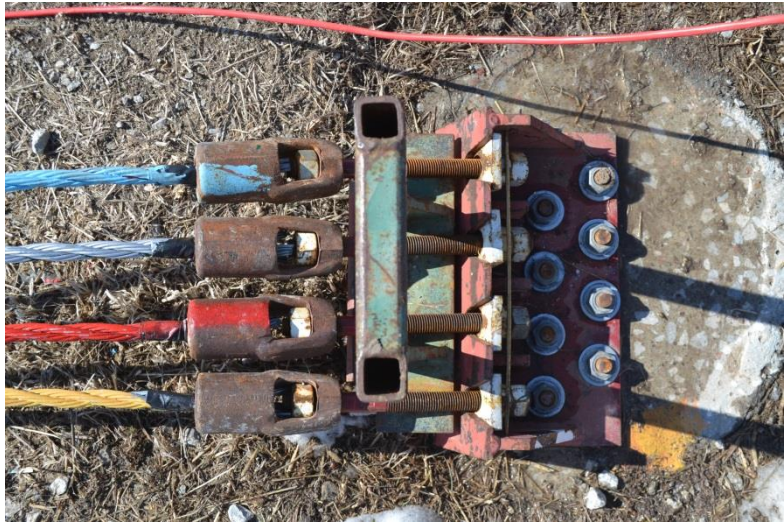


Figure 140. Test Installation Photographs, Test No. MWP-7



Figure 141. Test Installation Photographs, Test No. MWP-7

9 FULL SCALE CRASH TEST MWP-7

9.1 Static Soil Test

Before full-scale crash test no. MWP-7 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The soil for this test was partially frozen, making it difficult to get a full range of soil strength up to 15 in. of deflection. The winch utilized to load the post reached its capacity, prior to reaching 15 in. (381 mm) of displacement. The winch capacity is over 2.5 times the required strength. Note that weak posts used in cable barrier systems do not rotate in strong soil. Instead, weak posts yield at the ground line in both frozen and unfrozen strong soils configured with compacted crushed limestone. Thus, the frozen soil condition was considered acceptable for this cable barrier test. The static test results, as shown in Appendix C, demonstrated a soil resistance above the baseline test limits. Thus, the soil provided adequate strength, and full-scale crash testing was conducted.

9.2 Weather Conditions

Test no. MWP-7 was conducted on February 24, 2015 at approximately 2:30 p.m. The weather conditions, as per the National Oceanic and Atmospheric Administration (station 14939/LNK), were reported and are shown in Table 14.

Table 14. Weather Conditions, Test No. MWP-7

Temperature	49°F
Humidity	36%
Wind Speed	16 mph
Wind Direction	30° West of True North
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0 in.
Previous 7-Day Precipitation	0.01 in.

9.3 Test No. MWP-7

The 2,557-lb (1,160-kg) small car impacted the high-tension, four-cable median barrier at a speed of 63.9 mph (102.9 km/h) and at an angle of 25.7 degrees. A summary of the test results and sequential photographs are shown in Figure 142. Additional sequential photographs are shown in Figures 143 and 144. Documentary photographs of the crash test are shown in Figure 145.

9.4 Test Description

Initial vehicle impact was to occur at a midspan location, or 4 ft (1.2 m) upstream from post no. 32, as shown in Figure 146, which was selected according to MASH guidelines. The actual point of impact was approximately 9.2 in. (234 mm) upstream from the target impact point. A sequential description of the impact events is contained in Table 15. The vehicle came to rest 89 ft (27.1 m) downstream from the point of impact, or between post nos. 42 and 43. The vehicle trajectory and final position are shown in Figures 142 and 147.

Table 15. Sequential Description of Impact Events, Test No. MWP-7

TIME (sec)	EVENT
0.000	Vehicle left-front bumper contacted cable no. 1 between post nos. 31 and 32.
0.008	Vehicle left fender contacted cable no. 3 between post nos. 31 and 32.
0.010	Vehicle left-front bumper contacted cable no. 2 between post nos. 31 and 32.
0.014	Cable no. 3 detached from post no. 31.
0.016	Vehicle left fender began to deform.
0.020	Vehicle left headlight began to deform, and post no. 32 began to deflect downstream.
0.022	Cable no. 3 detached from post no. 32.
0.024	Post nos. 31 and 32 began to deflect backward.
0.032	Vehicle left side mirror contacted cable no. 4 and began to deform.
0.036	Vehicle front bumper contacted post no. 32, and post no. 33 began to deflect backward.
0.042	Post no. 30 began to deflect backward.
0.044	Vehicle left A-pillar contacted cable no. 3.
0.048	Vehicle left A-pillar began to deform, and cable no. 4 detached from post no. 32.
0.052	Cable no. 2 detached from post no. 32.

0.060	Cable no. 3 detached from post no. 33.
0.062	Post no. 34 began to deflect backward.
0.068	Post no. 29 began to deflect backward.
0.076	Vehicle overrode post no. 32.
0.078	Vehicle left A-pillar contacted cable no. 4.
0.080	Cable no. 2 detached from post no. 33.
0.084	Vehicle left-front tire overrode cable no. 1, and cable no. 3 detached from post no. 34.
0.086	Vehicle left side mirror detached, and post no. 35 began to deflect backward.
0.088	Vehicle left-front tire overrode cable no. 1.
0.098	Cable no. 4 detached from post no. 31.
0.102	Cable no. 3 detached from post no. 35.
0.108	Post no. 36 began to deflect backward.
0.112	Cable no. 3 detached from post no. 30
0.118	Vehicle front bumper contacted post no. 33, and cable no. 4 detached from post no. 33.
0.128	Vehicle left-front door contacted cable no. 2.
0.132	Vehicle left-front door began to deform, and cable no. 3 detached from post no. 29.
0.142	Cable no. 4 detached from post no. 34.
0.164	Vehicle left-rear tire overrode cable no. 1, and cable no. 2 detached from post no. 34.
0.166	Vehicle right fender began to deform, and cable no. 4 detached from post no. 35.
0.180	Cable no. 2 detached from post no. 35.
0.186	Post no. 37 began to deflect backward, and vehicle under-rode cable nos. 3 and 4.
0.188	Post no. 38 began to deflect backward.
0.204	Vehicle left-front tire became airborne.
0.232	Vehicle left headlight detached.
0.242	Cable no. 2 detached from post no. 31.
0.252	Vehicle left-front tire regained contact with ground.
0.274	Vehicle right-rear tire overrode cable no. 1.
0.350	Cable no. 3 detached from post no. 43.
0.424	Vehicle was parallel to system.
0.516	Vehicle was yawing toward barrier.
0.522	Cable no. 3 detached from post no. 44.
0.528	Cable no. 3 detached from post no. 45.
0.588	Vehicle right fender contacted post no. 37.
0.626	Vehicle right-front door contacted post no. 37.
0.660	Vehicle right headlight contacted post no. 38.
0.730	Vehicle right A-pillar contacted cable no. 4.
0.734	Vehicle right-front window, and right C-pillar contacted cable no. 4.
0.815	Vehicle bumper contacted post no. 39.
0.880	Vehicle began to yaw away from barrier.
0.926	Vehicle left-front tire became airborne.
0.960	Vehicle was wedged between cable no. 2 (impact side) and cable nos. 1 and 4 (non-impact side).
1.002	Vehicle bumper contacted post no. 40.

1.006	Vehicle left-front tire regained contact with ground.
1.152	Vehicle right-front tire deflated.
1.178	Vehicle began to yaw toward barrier.
1.202	Vehicle bumper contacted post no. 41.
1.220	Vehicle began to transverse back toward barrier.
1.340	Vehicle right B-pillar contacted cable no. 4 coupler, grinding through one layer of steel.
1.458	Vehicle bumper contacted post no. 42.
2.096	Vehicle front bumper contacted post no. 43.
2.258	Vehicle came to a rest with its bumper pressed against post no. 43.

9.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 148 through 158. Barrier damage consisted of bent posts, disengaged cables, and bent and fractured brackets. At its final resting position, the vehicle was still in contact with the cables. Cable no. 3 was beneath the vehicle, cable no. 2 was on the impact side of the vehicle, and cable nos. 1 and 4 were on the non-impacting side of the vehicle.

Cable no. 4 disengaged from post nos. 31 through 46 due to fracturing of the brass keeper rods. Cable no. 3 disengaged from post nos. 23 through 45. Cable no. 2 disengaged from post nos. 31 through 43. Cable no. 1 disengaged from post nos. 32, 33, as well as from post nos. 36 through 44. Seven of these cable brackets fractured at the neck, and two fractured at the tabs. The remainder of the brackets released the cables due to rotation of the bracket tab through the keyway. Negligible cable slip occurred at splice locations.

Post nos. 31 through 45 had varying degrees of plastic deformations in the form of bending and twisting, while other posts were only slightly displaced through the soil. Typically, posts were twisted to face downstream, and were bent laterally backward and/or longitudinally downstream, or a combination of both. In addition, post nos. 32, 33, as well as post nos. 37 through 42 had contact marks from the vehicle undercarriage overriding them. These same posts showed the greatest deflection.

The maximum dynamic barrier deflection was 97 in. (2,464 mm), and the working width of the system was 103.6 in. (2,631 mm), as determined from high-speed video analysis. Neither anchor was permanently displaced as a result of the impact loads imparted to it.

9.6 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 159 through 162. The maximum occupant compartment deformations are listed in Table 16 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH-established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

Table 16. Maximum Occupant Compartment Deformations by Location, Test No. MWP-7

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	0.3 (8)	≤9 (229)
Floor Pan & Transmission Tunnel	1.2 (30)	≤12 (305)
Side Front Panel (in Front of A-Pillar)	0.2 (5)	≤12 (305)
Side Door (Above Seat)	0.1 (3)	≤12 (305)
Side Door (Below Seat)	0.1 (3)	≤9 (229)
Roof	0.5 (13)	≤4 (102)

The majority of the vehicle damage was concentrated on the left-front corner, where the initial impact occurred, and on the right-front corner of the vehicle, where it impacted the system again as it crossed from behind the system to the front side of the system. The front bumper, left headlight, left side mirror, a 19 in. (483 mm) long portion of the left fender, right-front door handle and rear antennae were disengaged. The right headlight was partially disengaged and fractured. Both front tires and the right-rear tire had deflated. The suspension on the right-front wheel was also damaged.

The left fender had been crushed into the wheel well. The right fender had crushed, which caused some tearing. The right-front door was crushed and dented inward. The left fender and engine hood were separated by a gap of 4 in. (102 mm), and the right fender separated away from the hood by 6¼ in. (159 mm).

The cable to vehicle contacts left striation marks on the left-front fender, up the length of the left A-pillar, and across the roof. This contact caused minor gouging on the A-pillar and denting on the roof. The damage to the left A-pillar caused spider-web cracking adjacent to the left-front A-pillar, which extended across the entire windshield. The cables also left gouges and scrapes along the entire left side of the vehicle and on the left-front rim. There was a 23 x 4½-in. (584 x 114-mm) long tear in the left-front door at the height of cable no. 2. On the right side of the vehicle, there were gouges on both right side tire rims, along both right side doors, and on the right A-pillar. Scraping was found on the right B- and C-pillars, as well as on the right-front and rear bumpers. There was a 5-in. (127-mm) kink in the front bumper, 10 in. (254 mm) left of center. Dents were observed on the right-front corner of the hood, the right-front tire rim, the right-rear wheel well, as well as on the roof.

There were four tears in the floor pan of the vehicle. There was a 2¾-in. (70-mm) long tear in the right-front floor pan, an 8-in. (203-mm) long tear behind the left-front seat, a 3½-in. (89-mm) long tear behind the right-front seat, and a 1-in. (25-mm) long tear in the left-rear of the floor pan. This damage can be seen in Figures 161 and 162.

9.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 17. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 17. The results of the occupant

risk analysis, as determined from the accelerometer data, are also summarized in Figure 142. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix I.

Table 17. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MWP-7

Evaluation Criteria		Transducer		MASH Limits
		SLICE 1 (primary)	SLICE 2	
OIV ft/s (m/s)	Longitudinal	-15.45 (-4.71)	-15.65 (-4.77)	≤ 40 (12.2)
	Lateral	12.03 (3.67)	12.41 (3.78)	≤ 40 (12.2)
ORA g's	Longitudinal	-10.29	-9.72	≤ 20.49
	Lateral	6.78	7.13	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	5.31	4.05	≤ 75
	Pitch	4.14	2.89	≤ 75
	Yaw	33.72	33.12	not required
THIV ft/s (m/s)		18.90 (5.76)	18.93 (5.77)	not required
PHD g's		11.38	11.42	not required
ASI		0.49	0.49	not required

9.8 Load Cells and String Potentiometers

The pertinent data from the load cells and string potentiometer were extracted from the bulk signal and analyzed using each transducer's calibration factor. The maximum displacement of the upstream anchor was recorded as 0.06 in. (2 mm). A summary of the maximum cable loads can be found in Table 18. The recorded data and analyzed results are detailed in Appendix J. The exact moment of impact could not be determined from the transducer data, as impact may

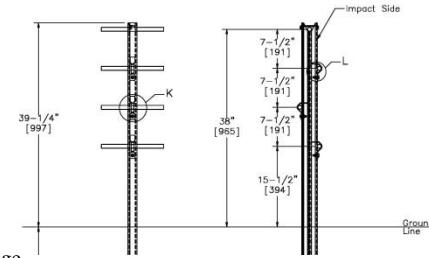
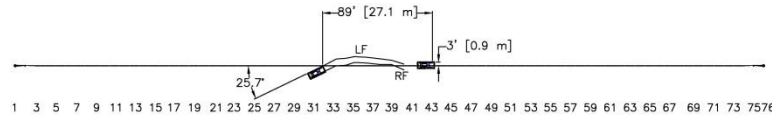
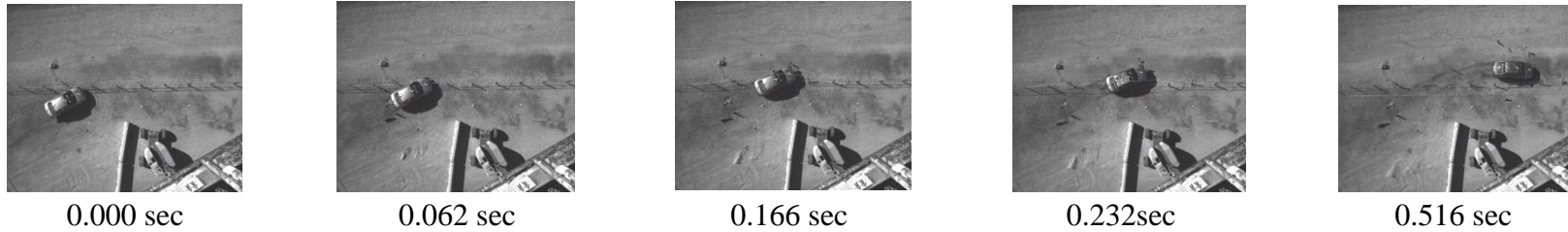
have occurred prior to observing a measurable signal in the electronic data. Thus, the extracted data curves should not be taken as a precise time after impact, but rather a general timeline between events within the data curve itself.

Table 18. Maximum Cable Loads, Test No. MWP-7

Cable Location	Sensor Location	Maximum Cable Load		Time (sec)
		kips	kN	
Combined Cable Load	Upstream of Impact	31.57	140.43	0.1234
Cable No. 4	Upstream of Impact	7.66	34.07	1.2421
Cable No. 3	Upstream of Impact	7.18	31.94	0.1429
Cable No. 2	Upstream of Impact	19.21	85.45	0.3614
Cable No. 1	Upstream of Impact	15.10	67.17	0.9403

9.9 Discussion

The analysis of the test results for test no. MWP-7 showed that the high-tension four-cable median barrier contained and redirected the 1100C vehicle, with controlled lateral displacements of the barrier. The test vehicle did not penetrate or ride over the barrier, and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix I, were deemed acceptable, because they did not adversely influence occupant risk safety criteria or cause rollover. After impact, the vehicle was captured and retained within the system, so there was no exit information. As the vehicle overrode the system posts, the posts tore the floorpan in multiple locations. The tears indicated that the top of these posts penetrated into the occupant compartment. Therefore, test no. MWP-7, conducted on the four-cable median barrier, was determined to be unacceptable according to the MASH safety performance criteria for test designation no. 3-10.



- Test AgencyMwRSF
- Test Number..... MWP-7
- Date02/24/2015
- MASH Test Designation3-10
- Test Article..... Four Cable Median Barrier
- Total Length 604 ft (184.1 m)
- Key Component - Cable
 - Size 3x7, 3/4-in. (19-mm) diameter
 - Cable Heights 15½, 23, 30½, 38 in. (394 mm, 584 mm, 775 mm, 965 mm)
- Key Component - MWP
 - Dimensions..... 3 x 1¼ x 81¼ in. (76 x 44 x 2,064 mm)
 - Spacing..... 8 ft (2.44 m)
- Soil TypeCompacted, coarse, crushed limestone
- Vehicle Make /Model.....2009 Kia Rio
 - Curb.....2,384 lb (1,081 kg)
 - Test Inertial.....2,392 lb (1,085 kg)
 - Gross Static.....2,557 lb (1,160 kg)
- Impact Conditions
 - Speed63.9 mph (102.9 km/h)
 - Angle 25.7 deg
 - Impact Location..... 4 ft - 9.2 in. (1.45 m) upstream of Post No. 32
- Impact Severity (IS)61.7 kip-ft (83.6 kJ) > 51 kip-ft (69.1 kJ)
- Exit Conditions
 - Speed NA
 - Angle NA
- Exit Box CriterionNA (Did not exit system)
- Vehicle Stability..... Satisfactory
- Vehicle Stopping Distance 89 ft (27.1 m)
- Vehicle Damage.....Moderate
 - VDS [8] 11-FL-5
 - CDC [9].....11-FDAK-6
 - Maximum Interior Deformation 3.46 in. (88 mm)

- Test Article Damage Moderate
- Maximum Test Article Deflections
 - Permanent Set24 in. (610 mm)
 - Dynamic.....97 in. (2,464 mm)
 - Working Width.....103.6 in. (2,631 mm)
- Transducer Data

Evaluation Criteria		Transducer		MASH Limit
		SLICE-1 (primary)	SLICE-2	
OIV ft/s (m/s)	Longitudinal	-15.45 (-4.71)	-15.65 (-4.77)	≤ 40 (12.2)
	Lateral	12.03 (3.67)	12.41 (3.78)	≤ 40 (12.2)
ORA g's	Longitudinal	-10.29	-9.72	≤ 20.49
	Lateral	6.78	7.13	≤ 20.49
MAX. ANGULAR DISPLACEMENT deg.	Roll	5.31	4.05	≤ 75
	Pitch	4.14	2.89	≤ 75
	Yaw	33.72	33.12	not required
THIV – ft/s (m/s)		18.90 (5.76)	18.93 (5.77)	not required
PHD – g's		11.38	11.42	not required
ASI		0.49	0.49	not required

Figure 142. Summary of Test Results and Sequential Photographs, Test No. MWP-7



0.000 sec



0.068 sec



0.204 sec



0.350 sec



0.522 sec



2.864 sec



0.000 sec



0.160 sec



0.326 sec



0.482 sec



0.880 sec



1.734 sec

Figure 143. Additional Sequential Photographs, Test No. MWP-7



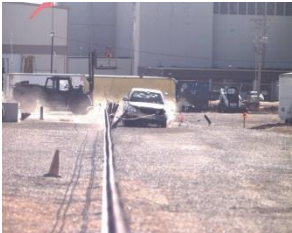
0.000 sec



0.118 sec



0.232 sec



0.424 sec



0.728 sec



1.152 sec



0.000 sec



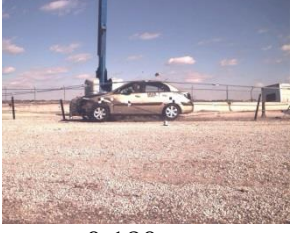
0.042 sec



0.084 sec



0.154 sec



0.180 sec



0.242 sec

Figure 144. Additional Sequential Photographs, Test No. MWP-7



Figure 145. Documentary Photographs, Test No. MWP-7



Figure 146. Impact Location, Test No. MWP-7



Figure 147. Vehicle Final Position and Trajectory Marks, Test No. MWP-7



Figure 148. System Damage, Test No. MWP-7



Figure 149. System Damage, End Anchorages, Test No. MWP-7



Figure 150. System Damage, Cable Brackets, Test No. MWP-7

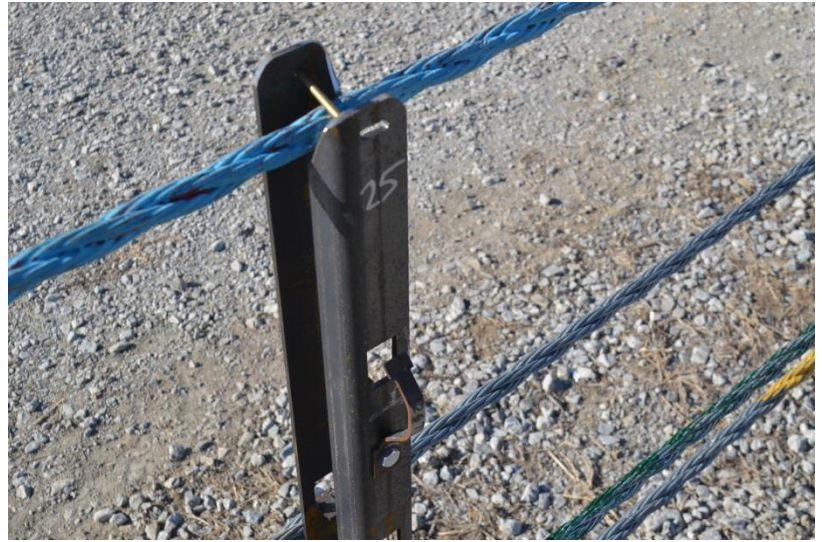
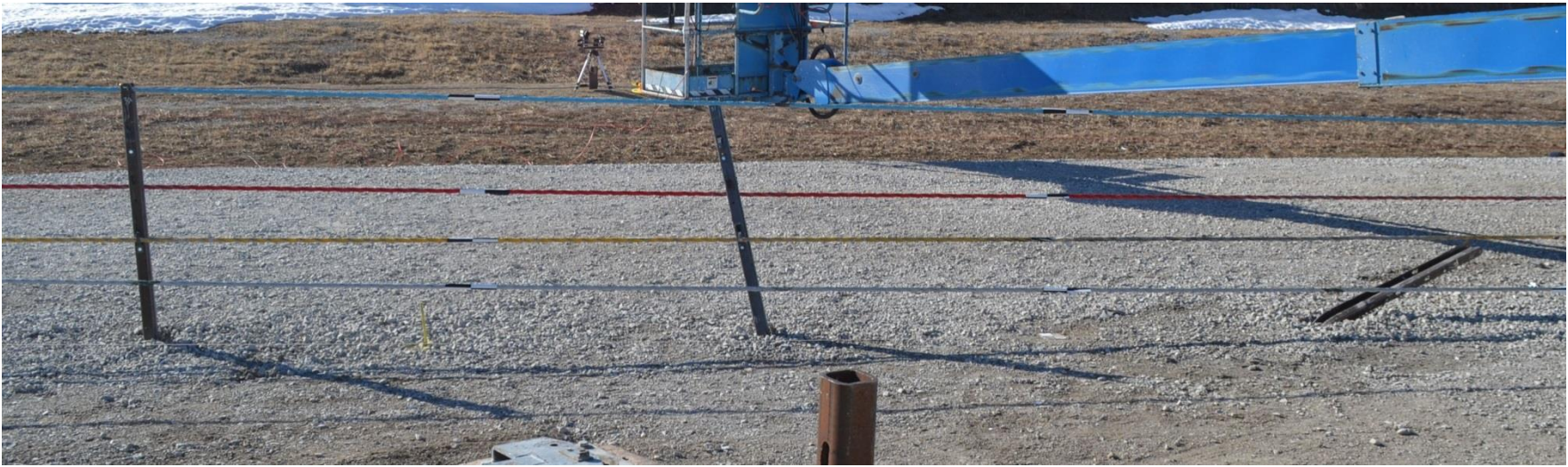


Figure 151. System Damage, Brass Rods, Test No. MWP-7



Post No. 30



Post No. 31



Post No. 32

Figure 152. System Damage, Post Nos. 30 through 32, Test No. MWP-7



Post No. 32



Post No. 33



Post No. 34

Figure 153. System Damage, Post Nos. 32 through 34, Test No. MWP-7



Post No. 34



Post No. 35



Post No. 36

Figure 154. System Damage, Post Nos. 34 through 36, Test No. MWP-7



Post No. 37



Post No. 38

Figure 155. System Damage, Post Nos. 37 through 38, Test No. MWP-7



Post No. 39



Post No. 40

Figure 156. System Damage, Post Nos. 39 through 40, Test No. MWP-7



Post No. 41



Post No. 43



Post No. 42



Post No. 43

Figure 157. System Damage, Post Nos. 41 through 43, Test No. MWP-7



Post No. 32



Post No. 39



Post No. 33



Post No. 42

Figure 158. Contact Marks, Post Nos. 33 through 39, Test No. MWP-7



Figure 159. Vehicle Damage, Test No. MWP-7



Figure 160. Vehicle Damage, Test No. MWP-7

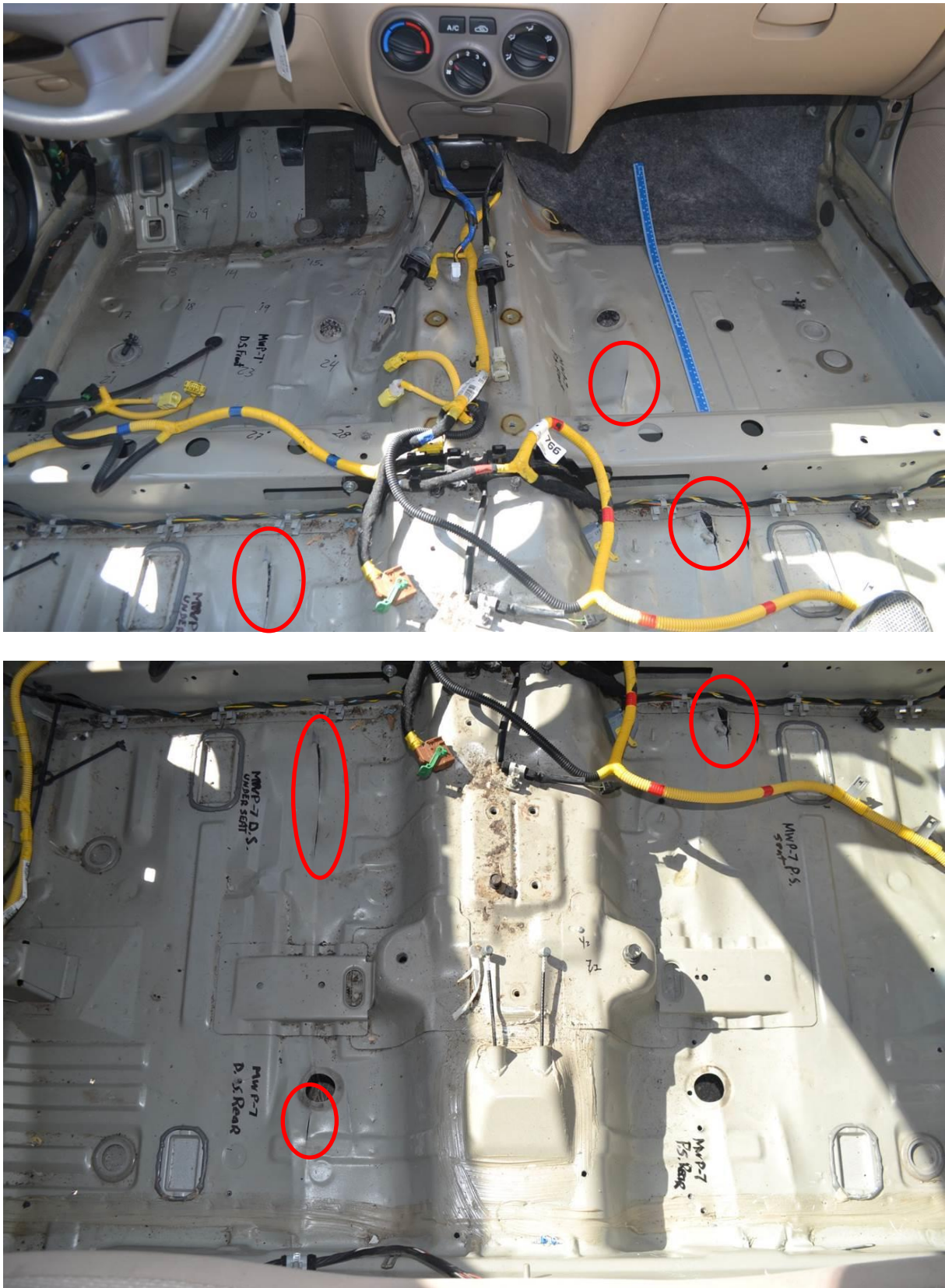


Figure 161. Occupant Compartment Damage, Test No. MWP-7
208

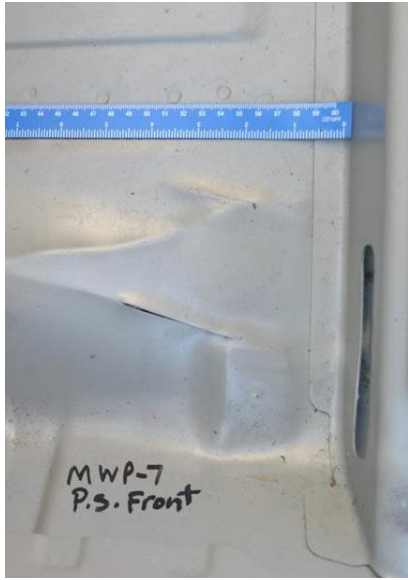
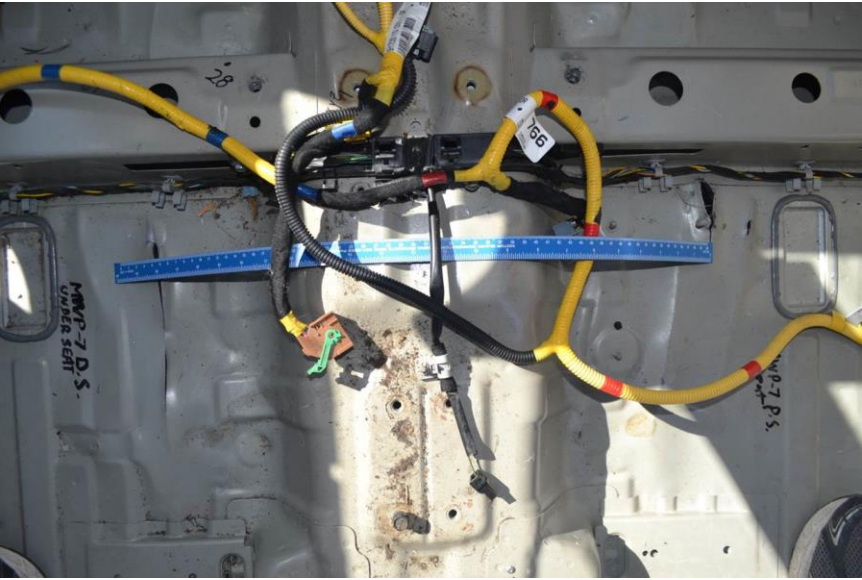


Figure 162. Occupant Compartment Damage, Test No. MWP-7

10 SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

The objective of this study was to continue to test and evaluate the prototype high-tension, four-cable median barrier system according to the MASH TL-3 safety criteria using the updated testing matrix for cable barrier systems installed within 6:1 median V-ditches. Three full-scale tests were conducted on the system and are reported herein.

Test no. MWP-4 was conducted in accordance with MASH test no. 3-11. The barrier was placed on level terrain and utilized a 10-ft (3.0-m) post spacing to establish the working width associated with a reduced post spacing. During the test, the 2270P pickup truck was initially captured and redirected by cable nos. 2 and 4. However, the vehicle eventually overrode cable no. 2 after the vehicle was parallel with the system. A working width of 16 ft - 9 in. (5.1 m) was observed during the test before the pickup came to rest in line with the barrier 144 ft - 10 in. (44.1 m) downstream from the point of impact. All occupant risk values were found to be within limits, and the occupant compartment deformations were also deemed acceptable. Subsequently, test no. MWP-4 was determined to satisfy the safety performance criteria for MASH test designation no. 3-11.

Test no. MWP-6, conducted in accordance with MASH test no. 3-10, involved a 1100C small car impacting the four-cable median barrier system with 8-ft (2.4-m) post spacing on level terrain. During the test, the small car was captured and redirected by cable no. 2. The A-pillar received only 0.12 in. (3 mm) of deformation, as the vehicle underrode cable nos. 3 and 4. The vehicle remained stable throughout the test, and the OIV and ORA values were below the MASH recommended limits. However, the occupant compartment was penetrated. When the top of posts were overridden, the floorpan was torn in two locations. Thus, test no. MWP-6 was determined to have failed the safety performance criteria corresponding to of MASH test designation no. 3-10.

To reduce the likelihood of occupant compartment penetration, the top corners of the MWP post were rounded. The outer corners were radiused $\frac{5}{8}$ in. (16 mm), and the inner bent corners were filleted $\frac{1}{4}$ in. (6 mm). Test no. MWP-7 was a repeat of MWP-6, but with the modified MWP post. During the test, the small car was captured and redirected by cable no. 2. The A-pillar received only 0.22 in. (6 mm) of deformation, as the vehicle under-rode cable nos. 3 and 4. The vehicle remained stable throughout the test, and the OIV and ORA values were below the MASH recommended limits. However, the floorpan was again torn due to contact with the tops of the MWP posts as the vehicle overrode them. Four separate tears occurred. Thus, test no. MWP-7 was determined to have failed the safety performance criteria corresponding to MASH test designation no. 3-10. The safety performance evaluation for each full-scale crash test is summarized in Table 19.

As a result of the unsuccessful 1100C crash tests, the prototype high-tension, four-cable, median barrier system will need to be further redesigned to prevent penetration of the occupant compartment observed in test nos. MWP-6 and MWP-7. Possible design changes may include, but are not limited to, alternative post spacings, reduction of weak-axis post strength at the ground line, further treatment of the post edges, and changes to post geometry. After the cable barrier system has been redesigned, it will need to be reevaluated according to MASH test designation no. 3-10 criteria before proceeding with remaining tests listed within the recommended testing matrix for cable barriers installed within median V-ditches. Depending on the nature of the design changes, it may be necessary to evaluate whether prior successful crash tests need to be rerun. The potential test designation nos. may be nos. 3-17 and 3-11 at a wide post spacings, and test no. 3-11 with a narrow post spacing.

Table 19. Summary of Safety Performance Evaluation – Test Nos. MWP-4, MWP-6, and MWP-7

Evaluation Factors	Evaluation Criteria	Test No. MWP-4	Test No. MWP-6	Test No. MWP-7		
Structural Adequacy	A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	S	S	S		
Occupant Risk	D. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	S	U	U		
	F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	S	S	S		
	H. Occupant Impact Velocity (OIV) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:	S	S	S		
	Occupant Impact Velocity Limits					
	Component				Preferred	Maximum
	Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)			
I. The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:	S	S	S			
Occupant Ridedown Acceleration Limits						
Component				Preferred	Maximum	
Longitudinal and Lateral	15.0 g's	20.49 g's				
Final Evaluation		PASS	FAIL	FAIL		

S – Satisfactory U – Unsatisfactory NA - Not Applicable

11 REFERENCES

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9. *Collision Deformation Classification – Recommended Practice J224 March 1980*, Handbook Volume 4, Society of Automotive Engineers (SAE), Warrendale, Pennsylvania, 1985.

12 APPENDICES

Appendix A. Material Specifications

Table A-1. Bill of Materials, Test No. MWP-4

Item No.	Description	Material Specification	Reference
a1	Cable Anchor Base Plate	ASTM A36	N/A
a2	Exterior Cable Plate Gusset	ASTM A36	N/A
a3	Interior Cable Plate Gusset	ASTM A36	N/A
a4	Anchor Bracket Plate	ASTM A36	N/A
a5	3/16 [5] Dia. Brass Keeper Rod 14" [356] long "	Brass	H# 05543-1
a6	Release Gusset	A36 Steel	N/A
a7	Release Lever Plate	A36 Steel	N/A
a8	1.25x1.25x0.1875 [32x32x5] TS CT Kicker Lever Tube "	ASTM A500 Gr. B	N/A
a9	CMB High Tension Anchor Plate Washer	ASTM A36	H# 64047117
a10	1.25x1.25x0.1875 [32x32x5] TS CT Kicker Lever Connecting Tube "	ASTM A 500 Gr. B	N/A
a11	3x10x0.5 [76x254x13] Kicker Plate "	ASTM A36	N/A
a12	CT kicker - gusset	ASTM A36	N/A
a13	3/4 [19] Dia. Flat Washer "	ASTM F844	PFC COC R# 14-0082
a14	3/4 [19] Dia. UNC J-Hook Anchor and Hex Nut "	J-Hook ASTM A449/Nut ASTM A563 DH	BOLT: H# 11618020 NUT: Item# DHHNO75CG Lot# 170277
a15	1/4 [6] Dia. Aircraft Retaining Cable 36" [914] long "	7x19 Galv.	N/A
a16	5/8 [16] Dia. Heavy Hex Nut "	ASTM A563C	R# 14-0343 COC
a17	5/8 [16] Dia. UNC 9 1/2" [241] Long Hex Bolt "	ASTM A449 or SAE J429 Gr. 5	R# 14-0343 COC
a18	24 [610] Dia. Concrete Anchor 120" [3048] long "	4,000 psi f'c	R# 14-0353 T# 4156617
a19	#11 Straight Rebar, 114 [2896] long "	Grade 60	H# 58196113
a20	#4 Anchor Hoop Rebar with 21 [533] Dia. "	Grade 60	H# 111485
b1	S3x5.7 [S76x8.5] Post by 28 1/8 [714] "	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A	R# 14-0476 H# 11935540
b2	S3x5.7 [S76x8.5] Post by 19 [483] "	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A	R# 14-0476 H# 11935540
b3	#3 Straight Rebar, 43 [1092] long "	Grade 60	H# JW12105480
b4	7 1/4 [184] Dia. No. 3 Hoop Reinforcement "	Grade 60	H# 537484
b5	2nd Post Keeper Plate, 28 Gauge	ASTM A36	N/A
b6	3/4 [19] Dia. UNC 5 1/2" [140] Long Hex Bolt and Nut "	Bolt ASTM A307 Gr. A/Nut ASTM A563A	Structural Bolt Distributor's Affidavit R# 14-0343
b7	1/2 [13] Dia. Washer with 1 1/16" [27] OD "	ASTM F844 (F436-SAE 1050 MOD4)	R#14-0106 H# A32336 BL# 195624
b8	1/2 [13] Dia. UNC 2" [51] long Hex Bolt and Nut "	Bolt ASTM A307 Gr. A/Nut ASTM A563A	Structural Bolt Distributor's Affidavit R# 14-0343
b9	4x3x1/4 [102x76x6] Foundation Tube 48" [1168] long "	ASTM A500 Grade B	H#B200931 / R# 13-0175
b10	2nd Post Cable Hanger	ASTM A36	R# 14-0476 H# A402276
b11	2nd Post Anchor Aggregate 12 in, Depth	-	-
b12	12 Dia. 2nd Post Concrete Anchor 46" long "	4,000 psi f'c	R# 14-0353 T# 4156617
b13	2nd Post Base Plate	ASTM A36	R# 14-0476 H# B314839
b14	3/16" [5] Dia. 5 1/4" [133] Long Brass Rod	ASTM B16-00	H# 05543-1
c1	3x1-3/4"x7 Gauge [76x44x4.6] 83" [2108] Long Bent Z-Section Post "	Hot-Rolled ASTM A1011 HSLA Gr. 50	H# 667827 Coil# 1131814950 R#14-0491 Green Paint
c2	12 Gauge Tabbed Bracket - Version 10	Hot-Rolled ASTM A1011 HSLA Grade 50	H# 832D32560
c3	5/16 [8] Dia. UNC 1" [25] Long Hex Cap Screw	Bolt SAE J429 Gr. 5 or ASTM A449	Lot# 3278740008 Order# 210072383

c3	5/16 Nut"	Nut ASTM A563 DH	Part# 1136304 H# 328711 AND H# 328481
c4	Straight Rod - 3/16 [5] Cable Clip "	ASTM B16 Brass C36000 Half Hard (HO2), ROUND. TS >=68.0 ksi, YS >= 52.0 ksi	H# 05543-1
d1	3/4 [19] Dia. High Strength Pre-Stretched Cable Guiderail "	3x7 Cl A Galv.	C1/C2 and C3, see next tab
d2	7/8 [22] Dia. Hex Nut "	ASTM A563C	R# 14-0325 H# M643354 White Paint
d3	Cable End Threaded Rod	ASTM A449	R# 14-0325 H# 133079 White Paint (left) Red Paint (right)
d4	Bennet Cable End Fitter	ASTM A47	H# 9Q4 AND OP5
x	Cable Wedges	ASTM A47	R# 14-0455 H# BR1
d5	7/8 [22] Dia. Square Nut "	SAE J429 Gr. 5	N/A
e1	Bennet Short Threaded Turnbuckle	Not Specified	COC
e2	Threaded Loadcell Coupler	N/A	N/A
e3	50,000-lb [222.4-kN] Load Cell	N/A	N/A

Table A-2. Bill of Materials, Test Nos. MWP-6 and MWP-7

Item No.	Description	Material Specification	Reference
a1	Cable Anchor Base Plate	ASTM A36	N/A
a2	Exterior Cable Plate Gusset	ASTM A36	N/A
a3	Interior Cable Plate Gusset	ASTM A36	N/A
a4	Anchor Bracket Plate	ASTM A36	N/A
a5	3/16 [5] Dia. Brass Keeper Rod 14" [356] long "	Brass	H# 05543-1
a6	Release Gusset	A36 Steel	N/A
a7	Release Lever Plate	A36 Steel	N/A
a8	1.25x1.25x0.1875 [32x32x5] TS CT Kicker Lever Tube "	ASTM A500 Gr. B	N/A
a9	CMB High Tension Anchor Plate Washer	ASTM A36	H# 64047117
a10	1.25x1.25x0.1875 [32x32x5] TS CT Kicker Lever Connecting Tube "	ASTM A 500 Gr. B	N/A
a11	3x10x0.5 [76x254x13] Kicker Plate "	ASTM A36	N/A
a12	CT kicker - gusset	ASTM A36	N/A
a13	3/4 [19] Dia. Flat Washer "	ASTM F844	PFC COC R# 14-0082
a14	3/4 [19] Dia. UNC J-Hook Anchor and Hex Nut "	J-Hook ASTM A449/Nut ASTM A563 DH	BOLT: H# 11618020 NUT: Item# DHHNO75CG Lot# 170277
a15	1/4 [6] Dia. Aircraft Retaining Cable 36" [914] long "	7x19 Galv.	N/A
a16	5/8 [16] Dia. Heavy Hex Nut "	ASTM A563C	R# 14-0343 COC
a17	5/8 [16] Dia. UNC 9 1/2" [241] Long Hex Bolt "	ASTM A449 or SAE J429 Gr. 5	R# 14-0343 COC
a18	24 [610] Dia. Concrete Anchor 120" [3048] long "	4,000 psi f'c	R# 14-0353 T# 4156617
a19	#11 Straight Rebar, 114 [2896] long "	Grade 60	H# 58196113
a20	#4 Anchor Hoop Rebar with 21 [533] Dia. "	Grade 60	H# 111485
b1	S3x5.7 [S76x8.5] Post by 28 1/8 [714] "	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A	R# 14-0476 H# 11935540
b2	S3x5.7 [S76x8.5] Post by 19 [483] "	ASTM A572 GR50-07, ASTM A709 GR50-09A, ASTM A992-06A	R# 14-0476 H# 11935540
b3	#3 Straight Rebar, 43 [1092] long "	Grade 60	H# JW12105480
b4	7 1/4 [184] Dia. No. 3 Hoop Reinforcement "	Grade 60	H# 537484
b5	2nd Post Keeper Plate, 28 Gauge	ASTM A36	N/A
b6	3/4 [19] Dia. UNC 5 1/2" [140] Long Hex Bolt and Nut "	Bolt ASTM A307 Gr. A/Nut ASTM A563A	Structural Bolt Distributor's Affidavit R# 14-0343
b7	1/2 [13] Dia. Washer with 1 1/16" [27] OD "	ASTM F844 (F436-SAE 1050 MOD4)	R#14-0106 H# A32336 BL# 195624
b8	1/2 [13] Dia. UNC 2" [51] long Hex Bolt and Nut "	Bolt ASTM A307 Gr. A/Nut ASTM A563A	Structural Bolt Distributor's Affidavit R# 14-0343
b9	4x3x1/4 [102x76x6] Foundation Tube 48" [1168] long "	ASTM A500 Grade B	H#B200931 / R# 13-0175
b10	2nd Post Cable Hanger	ASTM A36	R# 14-0476 H# A402276
b11	2nd Post Anchor Aggregate 12 in, Depth	-	-
b12	12 Dia. 2nd Post Concrete Anchor 46" long "	4,000 psi f'c	R# 14-0353 T# 4156617
b13	2nd Post Base Plate	ASTM A36	R# 14-0476 H# B314839
b14	3/16" [5] Dia. 5 1/4" [133] Long Brass Rod	ASTM B16-00	H# 05543-1
c1	3x1-3/4"x7 Gauge [76x44x4.6] 83" [2108] Long Bent Z-Section Post "	Hot-Rolled ASTM A1011 HSLA Gr. 50	H# 667827 Coil# 1131814950 R#14-0491 Green Paint
c2	12 Gauge Tabbed Bracket - Version 10	Hot-Rolled ASTM A1011 HSLA Grade 50	H# 832D32560
c3	5/16 [8] Dia. UNC 1" [25] Long Hex Cap Screw	Bolt SAE J429 Gr. 5 or ASTM A449	Lot# 3305380002 Order# 210072383 H# 311406798
c3	5/16 Nut"	Nut ASTM A563 DH	Part# 1136304 H# 328711 AND H# 328481 AND H# KV894

c4	Straight Rod - 3/16 [5] Cable Clip "	ASTM B16 Brass C36000 Half Hard (HO2), ROUND. TS >=68.0 ksi, YS >= 52.0 ksi	H# 05543-1
d1	3/4 [19] Dia. High Strength Pre-Stretched Cable Guiderail "	3x7 Cl A Galv.	C1/C2 and C3, H# 131499 see next tab
d2	7/8 [22] Dia. Hex Nut "	ASTMA563C	R# 14-0325 H# M643354 White Paint
d3	Cable End Threaded Rod	ASTMA449	R# 14-0325 H# 133079 White Paint (left) Red Paint (right)
d4	Bennet Cable End Fitter	ASTM A47	H# 9Q4 AND OP5
x	Cable Wedges	ASTM A47	R# 14-0455 H# BR1
d5	7/8 [22] Dia. Square Nut "	SAE J429 Gr. 5	N/A
e1	Bennet Short Threaded Turnbuckle	Not Specified	COC
e2	Threaded Loadcell Coupler	N/A	N/A
e3	50,000-lb [222.4-kN] Load Cell	N/A	N/A

P.O.# LI017752




TC Industries Test Center
3703 South Route 31
Crystal Lake, IL 60012-1412
Telephone (815) 459-2400 Fax (815) 459-3419

TEST REPORT

REPORT NO: 161620
DATE: APRIL 25, 2012
PAGE 1 OF 1

BILL TO: AMERICAN EAGLE STEEL
317 EAST 11TH STREET
CHICAGO HEIGHTS, IL 60411

SHIP TO: AMERICAN EAGLE STEEL
317 EAST 11TH STREET
CHICAGO HEIGHTS, IL 60411

DESC: 405 PCS .75"RD X 24'		HEAT: 57698C		GRADE: 1045		WT: 14601	
PO: 1414-TC1		MO: 0605680		CO: 1414		LOT: 80939	
SPEC: QUENCH, TEMPER, STRAIGHTEN PINK				ASTM-A449-10			
PROCESS:		FURN TEMP: 1600		FURN TIME hh.mm:		.45	
		TEMPER TEMP: 1075		TEMPER TIME hh.mm:		.45	
		STRESS TEMP:		STRESS TIME hh.mm:		QUENCH: WATER	
PARAMETER	UNITS	LIMITS		TEST RESULTS (See sampling plan on back)			
TENSILE	KSI	120.0	N/A	138.0			
YIELD .2%	KSI	92.0	N/A	124.0			
ELONG 2"	%	14.0	N/A	19.0			
RED AREA	%	35.0	N/A	55.0			
SURFACE HB	HBW	255	321	289	285	294	285
				285	285		285
4Cable Anchorage "J-Hook bolts" R#15-0281 Yellow Paint December 2015 SMT							
 ACCREDITED Testing Cert #1281-01							

TC INDUSTRIES and SUBCONTRACTED LABS (A2LA ACCREDITED)

Tensile, Standard TC	Rockwell	Micro Analysis*
Tensile, Full Size	Brinell TC	Decarb Measure
Charpy V Notch	Ultra Sonic*	Chemistry*
Microhardness, Knoop*	Bend Test*	
TC: TC Test Center	BE: Berg Eng.	EX: Exova
Cert #1281.01	Cert #L1157-1	Cert #104.02
2/28/13	2/4/14	6/30/12
		MSI: Metallurgical Ser.
		Cert #0510.01
		12/31/12

Time 12:26 DATE IN: 4/11/12 *not included in our scope of accreditation FC 4.12.16F 7/15/10

NOTES:

Phil Burgdorf
Test Center Tech II

There are no deviations from test methods unless noted. It should not be assumed that mechanical properties of raw material heat treated to a fastener standard will have the same properties of a finished fastener whose original material characteristics may have been significantly altered.
No mercury was used/added and no welding/weld repair was performed on this material while in the possession of TC Industries, Inc.
This original test report displays a raised "TC Industries Test Center" seal. This test report relates only to the items listed and shall not be reproduced, except in full, without the written permission of TC Industries Test Center.

Figure A-1. Cable End Threaded Rod, Test No. MWP-4

QUALITY CERTIFICATE

NINGBO JINDING FASTENING PIECE CO., LTD

XIJINGTANG JIULONGHU NINGBO CHINA TEL:+86-574-86530122 FAX: +86-574-86530858

Customer:	FASTENAL COMPANY PURCHASING--IMPORT	Date :	2014-05-04
Product:	HEX CAP SCREWS	Contract No:	13JDF499T
Class:	5	Invoice No:	00500225-1
Size:	5/16-18X1	Lot No:	3278740008
Marking:	JDF three radius	Order No.	210072383
Quantity:	60.000 mpcs	Part No.	110120325
		Production Date	2014-02-14

Dimensions Of SPEC:

Certificate No. :

Inspection Items	Standard	Result	Sample	Pass						
Visual Appearance	-----	OK	29	29						
Body Diameter	/	/	5	5						
Thread	Go	3A	OK	5						
	No Go	2A	OK	5						
Width Across Flats	0.500-0.489	0.493-0.495	15	15						
Width Across Corners	0.577-0.557	0.571-0.567	5	5						
Major Diameter	0.311-0.303	0.311-0.303	5	5						
Head Height	0.211-0.195	0.202-0.205	5	5						
Total Length	0.970-1.000	0.984-0.988	15	15						
Thread Length	min 0.861	0.865-0.869	15	15						
Key Engagement	/	/								
Head Diameter	/	/								
Mechanical Properties										
Characteristics	Standard	Result								
Surface Hardness [30N]	MAX 54	46-48	5	5						
Core Hardness [HRC]	25-34	28.6-30	5	5						
Wedge Strength [psi]	min 119880	139182-146003	3	3						
Yield Strength [psi]	min 91869	102028-108849	3	3						
Elongation [%]	min 14	15.8-17.3	3	3						
Reduction Of area [%]	min 35	41.6-48.8	3	3						
Proof Load [Ib]	4450	4450	3	3						
Impact test -20°C [Kv/J]	/	/								
Decarburization	N≥1/2H1 HV0.3	296.12 296.12 311.88	3	3						
HV2>=HV1-30, HV3<=HV1+30	G 0.0006max									
CHEMICAL COMPOSITION (%)										
Heat No	C	Si	Mn	P	S	Cr	Ni	Cu	Mo	B
35#	4200289BB	0.35	0.14	0.63	0.020	0.011				
Thickness [UM]		min 5				8.1-8.87			20	20
Surface Coating:	ZPCr3+(coating test method: X ray according to ASTM B568M 2007 standard test									
Thread Specification:	ASME B1.1 2003, UNIFIED INCH SCREW THREADS (UN AND UNR THREAD FORM)									
sampling dimension specification:	ASME B18.18.2 2009 inspection and quality assurance for high-volume machine assembly									
Dimension Specification:	ASME B18.2.1 2010, HEX CAP SCREWS									
sampling mechanical properties specification:	ASTM F1470 2009 Standard Guide for Fastener Sampling for Specified Mechanical									
Mechanical Properties:	SAE J429 2011, MECHANICAL AND MATERIAL REQUIREMENTS FOR EXTERNALLY THREADED FASTENERS									
Surface Defect:	ASTM F788M, SURFACE DISCONTINUITIES OF BOLTS, SCREWS, AND STUDS									
Plating Specification:	ASTM A974 2010, Electrodeposited Coatings On Threaded Fasteners									
Quality Control Supervisor							Quality Control Manager			



5/16" Grade 5 Bolts
MWP-4 Clip Hardware R#15-0093 August 2014 SMT

刘北平

Figure A-2. 5/16 in. (8 mm) Hex Cap Screws, Test No. MWP-4

SUPER CHENG INDUSTRIAL CO.,LTD.

NO. 18 BEN-GONG 2nd ROAD., BEN CHOU INDUSTRIAL PARK, KAOHSIUNG COUNTY 820, TAIWAN R.O.C.
TEL : 886-7-6225326-30(5 LINES) FAX : 886-7-6215377/6212335/6235829

CERTIFICATE OF INSPECTION

CERT.# : P58-13071707-1T ISSUED DATE : 2013/9/27 PAGE 1 OF 1

CLIENT : SUPER CHENG INDUSTRIAL CO., LTD.

ADDRESS : NO. 18 BEN-GONG 2nd ROAD., BEN CHOU INDUSTRIAL PARK, KAOHSIUNG COUNTY 820, TAIWAN R.O.C.

PURCHASER : FASTENAL COMPANY PURCHASING	PO # : 210068905
PART #1136304	QTY SHIPPED : 90,000 PCS

COMMODITY : GRADE 5 FIN HEX NUT

FINISH : TRIVALENT ZINC

SIZE : 5/16-18

LOT# : P58-13071707

SAMPLING PLAN : ANSI/ASME B18.18.2M-93

QTY : 807510 PCS


MATERIAL : SWRCH15A

HEAT NO. : 328711

MANUFACTURER : SUPER CHENG IND. CO., LTD.

MANU. DATE : 2013/8/20

DIMENSIONAL INSPECTION SPEC. : ANSI/ASME B18.2.2-10 SAMPLED BY : SHU HUI WANG

ITEM	SAMPLE SIZE	SPECIFIED		ACTUAL RESULT	JUDGMENT
APPEARANCE	100	ASTM F812-07		GOOD	OK
W.A.F.	32	0.500 ~ 0.489 in.		0.493 ~ 0.492 in.	OK
W.A.C.	8	0.577 ~ 0.557 in.		0.565 ~ 0.563 in.	OK
THICKNESS	8	0.273 ~ 0.258 in.		0.263 ~ 0.262 in.	OK
THREAD	32	ANSI/ASME B1.1		PASS	OK

MECHANICAL PROPERTIES SPEC. : SAE J995-12 SAMPLED BY : SHU HUI WANG

ITEM	SAMPLE SIZE	TEST METHOD	SPECIFIED	ACTUAL RESULT	JUDGMENT
HARDNESS	8	ASTM F606-11a	MAX HRC32	11.0 ~ 8.0 HRC	PASS
PROOF LOAD	4	ASTM F606-11a	MIN 6300LB	6449 ~ 6415 LB	PASS
PLATING THICKNESS	4	ASTM B568-98	MIN 0.0001 in	0.00013 ~ 0.00012 in	PASS

5/16" Grade 5 Nuts

MWP-4 Clip Hardware R#15-0093 August 2014 SMT

There are two separate Heat numbers for this purchase.

REMARK : 1、THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT WRITTEN APPROVAL OF THE LAB.

2、THIS INSPECTION CERTIFICATE IS FOR RESPONSIBILITY UNDER SAMPLE ONLY

3、ABOVE SAMPLES TESTED CONFORM TO THE FASTENER SPECIFICATION OR STANDARDS



LAB. DIRECTOR(SIGNATORY) : _____

表單編號 : LQC 10E Rev.0

Figure A-3. 5/16 in. (8 mm) Hex Cap Nuts, Test No. MWP-4



Certificate of Compliance

Sold To:

UNL BUILD SYSTEM MAINTENANCE

Purchase Order:

Job:

Invoice Date: 08/22/2014

THIS IS TO CERTIFY THAT WE HAVE SUPPLIED YOU WITH THE FOLLOWING PARTS.
THESE PARTS WERE PURCHASED TO THE FOLLOWING SPECIFICATIONS.

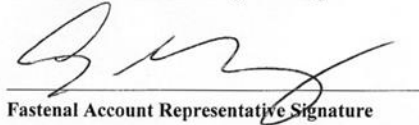
95 PCS 5/16"-18 x 1" Zinc Finish SAE J429 Grade 5 Hex Cap Screw SUPPLIED UNDER OUR TRACE NUMBER 210072383
AND UNDER PART NUMBER 110120325

100 PCS 5/16"-18 x 1" Zinc Finish SAE J429 Grade 5 Hex Cap Screw SUPPLIED UNDER OUR TRACE NUMBER 210072383
AND UNDER PART NUMBER 110120325

100 PCS 5/16"-18 Zinc Finish Grade 5 Finished Hex Nut SUPPLIED UNDER OUR TRACE NUMBER 210075139 AND
UNDER PART NUMBER 1136304

100 PCS 5/16"-18 Zinc Finish Grade 5 Finished Hex Nut SUPPLIED UNDER OUR TRACE NUMBER 210068905 AND
UNDER PART NUMBER 1136304

This is to certify that the above document is true
and accurate to the best of my knowledge.



Fastenal Account Representative Signature

Eric Fugleberg
Printed Name

8/22/14
Date

Please check current revision to avoid using obsolete copies.

This document was printed on 08/22/2014 and was current at that
time.

Fastenal Store Location/Address

3200 N. 20th Street
LINCOLN, NE 68521
Phone #: (402)476-7900
Fax #: (402)476-7958

Figure A-4. 5/16 in. (8 mm) Hex Cap Screws and Nuts, Test No. MWP-4

Concrete Industries 6300 Cornhusker Highway P. O. Box 29529 Lincoln, NE 68529 Phone: (402)434-1800 FAX: (402)434-1899 4CMB/MWP Anchorage Rebar Yellow Paint R#14-0349 SMT							JOB NUMBER 8000MISC.		RELEASE NUMBER DAVID-789		REQ. DELIVERY DATE		PAGE 1 of 1						
MATERIAL TYPE Rebar, Grade 60, Black							REFERENCE		DRAWING ID		DESCRIPTION STOCK								
Item	Qty	Size	Length	Mark	Shape	Lbs	A	B	C	D	E	F/R	G	H	J	K	O	BC	
1	32	11	9-06			1615												0	
						1615.													
2	88	4	7-00	A401	T3	411			5-06				1-06					1-09	1
						411.													
3	44	3	3-01	A301	T3	51			2-01				1-00					0-08	1
4	16	3	3-07			22													0
						73.													

Total Weight: 2,099 Lbs

Longest Length: 9-06

WEIGHT SUMMARY

TOTAL				STRAIGHT			LIGHT BENDING			HEAVY BENDING		
SIZE	ITEMS	PIECES	LBS	ITEMS	PIECES	LBS	ITEMS	PIECES	LBS	ITEMS	PIECES	LBS
Rebar, Grade 60, Black												
3	2	60	73	1	16	22	1	44	51	0	0	0
4	1	88	411	0	0	0	1	88	411	0	0	0
11	1	32	1615	1	32	1615	0	0	0	0	0	0
	4	180	2099	2	48	1637	2	132	462	0	0	0

Total Weight: 2,099 Lbs

Longest Length: 9-06

#3 COIL EVRAZ 111940 ✓
 #3 Gerdau 59054886 ✓
 #4 COIL EVRAZ 112001 ✓
 #11 Gerdau 11677949 ✓

Figure A-5. Rebar in Concrete Anchor, Test Nos. MWP-4, MWP-6 and MWP-7



ROCKY MOUNTAIN STEEL
A DIVISION OF EVRAZ INC. NA

P.O. Box 316
Pueblo, CO 81002 USA

MATERIAL TEST REPORT

Date Printed: 03-DEC-13

Date Shipped: 03-DEC-13	Product: DEF #3 (3/8")	Specification: ASTM A-706/A-615
FWIP: 52815363	Customer: CONCRETE INDUSTRIES INC	Cust. PO: 104048

Heat Number	CHEMICAL ANALYSIS															
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al	V	B	Cb	Sn	N	Ti
111940	.26	1.27	.013	.030	.25	.31	.11	.10	.032	.002	.042			.013	.0147	

Heat Number	Sample No.	MECHANICAL PROPERTIES					
		Yield (Psi)	Ultimate (Psi)	Elongation (%)	Reduction (%)	Bend	Wt/ft
111940	01	0.2% offset	76276	106690	14.8	ok	0.371
111940	02	70502	105120	14.3	ok	0.371	

0.0035 EUL

All melting and manufacturing processes of the material subject to this test certificate occurred in the United States of America.

ERMS also certifies this material to be free from Mercury contamination.

This material has been produced and tested in accordance with the requirements of the applicable specifications. We hereby certify that the above test results represent those contained in the records of the Company.

Quality Assurance Department

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Figure A-6. Steel Rebar within Concrete Anchors, Test Nos. MWP-4, MWP-6 and MWP-7



EVRAZ

ROCKY MOUNTAIN STEEL
A DIVISION OF EVRAZ INC. NA

P.O. Box 316
Pueblo, CO 81002 USA

MATERIAL TEST REPORT

Date Printed: 24-FEB-14

Date Shipped: 24-FEB-14	Product: DEF #4 (1/2")	Specification: ASTM A-706/A-615
FWIP: 52815364	Customer: CONCRETE INDUSTRIES INC	Cust. PO: 105158

Heat Number	CHEMICAL ANALYSIS															
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al	V	B	Cb	Sn	N	Ti
112001	0.27	1.21	0.019	0.027	0.28	0.41	0.12	0.22	0.042	0.002	0.041			0.013	0.010	
Carbon Equivalent = 0.505																

Heat Number	Sample No.	MECHANICAL PROPERTIES						Bend	Wt/ft
		Yield (Psi)	Ultimate (Psi)	Elongation (%)	Reduction (%)				
112001	01	0.2% offset (MPa)	69333 478.0	105470 727.2	14.0		ok	0.669	
	02	0.0035 EUL (MPa)	66533 458.7	108940 751.1	15.5		ok	0.674	

All melting and manufacturing processes of the material subject to this test certificate occurred in the United States of America. ERMS also certifies this material to be free from Mercury contamination.

This material has been produced and tested in accordance with the requirements of the applicable specifications. We hereby certify that the above test results represent those contained in the records of the Company.

Quality Assurance Department

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Figure A-7. Steel Rebar within Concrete Anchors, Test Nos. MWP-4, MWP-6 and MWP-7

Certified Report Of Chemical Analysis And Mechanical Tests

Arcelor

ArcelorMittal
 Indiana Harbor West
 3001 Dickey Road
 East Chicago, IN 46312



Date Shipped: 5/26/2009
 Sales Order: 423794001 Customer PO: P90323BL0024
 Sold To: STATE STEEL SUPPLY CO
 214 COURT STREET P.O. BOX 3224 SIOUX CITY IA
 Ship To: STATE STEEL SUPPLY CO(RAIL)
 214 COURT STREET - RAIL SIOUX CITY IA
 Product Description: ASTM A1011 GRD 80XP Hot Band Prime ASTM A1011 GRD 50XF 0.1250 Min x 80.2500 In

Heat Chemistry %

Heat	C	Mn	P	S	Si	Cu	B	Cr	V	Ti	Cb	Al	N	Ni	Mo	Ca	SN
88471	0.06	0.87	0.008	0.007	0.025	0.01	0.000	0.02	0.001	0.017	0.018	0.039	0.0059	0	0.01	0.004	0.002

Heat Physicals

Yield PSI	Yield MPa	UTS PSI	UTS MPa	Elongation %	Direction
54200	374	65200	449	32.2	L
56300	388	66500	458	31.3	L

Shipment Tags Represented By Preceding Heat Results

Tag #	Load	Gauge	Width	Length
06582707	01325949	0.125	60.25	Coil

Handwritten: 11

All tests were performed by ArcelorMittal - Indiana Harbor, unless specified, in accordance with the following: chemical analysis per ASTM E415 and E1019; mechanical test per ASTM E8 and E946, JIS Z2241, Z253 and Z254, EN 10002-1; Rockwell hardness per ASTM E18; coating weight per ASTM A754, A90, and A425. All tests are performed to the current version of the standard, unless otherwise noted. All tensile testing performed with gauge length of 2 inches. These results relate only to the items tested. Information about measurement uncertainty, when applicable, is available upon request. ArcelorMittal - Indiana is A2LA certified. Charpy testing is performed by ArcelorMittal - Burns Harbor, an A2LA certified facility.

We hereby certify the above is correct as contained in the records of the corporation.
 ArcelorMittal, Indiana Harbor West - Quality Assurance Department Peter D. Carey

Figure A-8. Cable Clips Chemical Report, Test Nos. MWP-4, MWP-6 and MWP-7

ESSAR Steel Algoma Inc. 105 West Street, Sault Ste. Marie, Ontario Canada P6A 7B4

CUSTOMER PURCHASE ORDER NUMBER P90728BL002	ENTRY DATE 2009/07/31	SHIP DATE 2009/09/08	TALLY NUMBER 140719	SHIPPER'S NO. 03-5628	CARRIER GTW	PAGE -187955
CHANGE TO CUSTOMER NAME AND ADDRESS STATE STEEL SUPPLY CO. 214 COURT STREET SIOUX CITY IOWA 51102 P.O. BOX 3224			SHIP TO CUSTOMER NAME AND ADDRESS STATE STEEL SUPPLY CO. 214 COURT STREET SIOUX CITY, IOWA 51102 IOWA			MILL TEST REP ESSAR STEEL ALGOMA INC. CERTIFIED THAT THE MATERIAL DESCRIBED WAS MADE AND ACCORDANCE WITH THE RUL SPECIFICATION SHOWN. ALL ARE RETAINED IN ACCORDANCE COMPANY'S STANDARD RECORD PRACTICES. J. JOHNSTON MANAGER METALLURGY THIS MILL TEST REPORT MAY BE REPRODUCED EXCEPT IN FULL WRITTEN APPROVAL OF ESSAR ALGOMA INC. IF YOU RECEIVE DOCUMENT AND ARE NOT THE RECEIVER, PLEASE CALL (78) COLLECT FOR INSTRUCTIONS OF DISPOSAL OF DOCUMENT.
CUSTOMER SPECIFICATION HOT ROLLED STEEL SHEET - HSLA - ASTM A1011 GR 50 HSLAS-F (07) - DQ - TEMPER ROLLED - RESTRICTED GAUGE 1/2 TOLERANCE - HSLA MODERATE FORMING SEMI-CRIT SURFACE STD SHPE						
SUPPLEMENTARY INSTRUCTIONS TEST CERT 1: BOB LANSWORTH 712-277-3306 TEST CERT 2: PLATE TE ST COUPON:						
TEST REPORTS REQUIRED RESALE			2000115860 WS 2009/09/18 12:32			



MEETS EN 10204 3.1
 HEATS INDICATED WITH (+) MADE IN CANADA WITH DOMESTIC AND NORTH AMERICAN MATERIALS
 * * * * * PRODUCT SHIPPED * * * * *
 CUSTOMER ITEM 00002 OUR ITEM 001 DIMENSIONS .112 MIN X 60.25 X COIL

COIL NUMBER	HEAT	NO. PIECES	WEIGHT	COIL NUMBER	HEAT	NO. PIECES	WEIGHT
63526011	6946J-01	1	40600	63526012	6946J-51	1	40740

* * * * * MECHANICAL PROPERTIES * * * * *

TENSILE TESTS:

HEAT	SAMPLE	GAUGE	COND	METH	DIR	YIELD TENSILE	% ELONG	LAB
6946J	DSFC	.1120	AR	.2	L	KSI	KSI	ALG
						55.5	68.0	32(2")

* * * * * CHEMICAL PROPERTIES * * * * *

HEAT	(WT %)	C	MN	P	S	SI	CR	NI	CU	MO	AL	CB	V	B
6946J +		.06	.46	.007	.003	.02	.02	.02	.05	.00	.021	.006	.031	.00280
		.001		.0096										

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****WARNING**** THE TEST RESULTS AND VALUES REPORTED HEREIN INDICATE ONLY THAT (1) THE PARTICULAR STEEL FOR WHICH THIS CERTIFICATE IS ISSUED MEETS THE MINIMUM SPECIFIED YIELD STRENGTH AND (2) THE CHEMICAL ANALYSIS AND PHYSICAL PROPERTIES OF SUCH STEEL ARE IN CONFORMANCE WITH THE REQUIREMENTS OF THE SPECIFICATION INDICATED. THE RESULTS OR VALUES REPORTED HEREIN CAN NOT BE USED TO QUALIFY THE STEEL FOR ANY SPECIFICATION OTHER

Figure A-9. Cable Clips Chemical Report, Test Nos. MWP-4, MWP-6 and MWP-7



MUELLER BRASS CO.

Control No: 705583

LOCATIONS:

2199 LAPEER AVENUE
PORT HURON, MICHIGAN 48060

302 ASHFIELD STREET
BELDING, MICHIGAN 48809

Certified Test Report

Sold: 00061067

Ship: 00059225

To: COPPER & BRASS SALES
ATTENTION: ACCOUNTS PAYABLE
P.O. BOX #5116
SOUTHFIELD, MI 48086-5116

To: COPPER & BRASS SALES-
8001 THYSSENKRUPP PARKWAY
NORTHWOOD, OH 43619

Cust PO: 5400146354

MBCo SO: 352441 Ln 70 Cert Lvl: 2

Cust Part: CURD00527

Part Nbr: 0250RD601200XX1 FC

Type: ROD Size: RND 0.250

Qty Shpd: 3,085 UM: Lbs

Cust Spec: ASTM B16/16M-10

BOL: 50471286 Shpd: 06/05/12

Mechanical Properties

Lot Number: 1375756		Temper: H020 1/2 H		CDA Alloy: C36000	
Yield Strength ()	Tensile Strength ()	Elongation % in 2 Inches		Hardness RB	

Chemical Analysis (%)

	Cu	Pb	Fe	Zn				
ASTM B16/16M-10	60.0-63.0	2.5-3.0	0.35 Max	REM				
Lot Number: 1375756	61.6	2.7	0.13	REM.				

OTHER EACH MAX: .50

We hereby certify to the chemical and mechanical properties reported herewith and to the fact that they were determined in conformance with the specification noted above or any exceptions to this specification we have granted. We also hereby certify that the material furnished on this order is free from mercury contamination and that no mercury bearing equipment was used in the manufacture of these items.

Melted and Manufactured in USA

ISO9001:2008 registered QMS

Produced in Compliance with:
EN10204 3.1
EU Directives:
2002/95/EC (RoHS Compliant)
2000/53/EC

By: *Stephanie Goodell* 06/05/12

Stephanie Goodell
Metallurgist

From: Copper and Brass Sales

Cust: ONLINE METALS

Del: 2401949744

Part: 1257

PO: 76155

Wgt: 86.000 LB

Date: 07/09/2012

Figure A-10. Straight Brass Rod Cable Clip, Test Nos. MWP-4, MWP-6 and MWP-7



Test Certificate

Document: 01024973

Norfolk Iron & Metal Co.

3001 North Victory Road
Norfolk, NE 68701
PH: (402) 371-1810

Product Description
Thickness: .1800 Heat: 083707 Supplier: THYSSENKRUPP STEEL USA
Specification(s): A1011 HSLAS-F GR50-12

Chemistry Data

C	MN	P	S	SI	AL	CB	V	CU	CR
.059	.417	.0189	.0026	.017	.0469	.02	.0001	.005	.022
NI	MO	SN	TI	N	B	ZR			
.012	.0001	.00	.001	.004	.0002	.00			

Mechanical Data

	Yield (PSI)	Tensile (PSI)	Elongation	Reduction Of Area	Sample Taken From
1	59716	68741	37.50 2"	71.9100	Head
2	59522	68267	40.40 2"	76.1700	Center

Produced From Coil

Melted and Manufactured In: Not Provided

The Mechanical Data for the product described above reflect the results of tests made by us in accordance with applicable ASTM or ASME standards and our testing procedures, and we certify that the information included in this Test Certificate with respect to such Mechanical Data is accurate to the best of our knowledge.

The Chemistry Data shown above was reported to us by THYSSENKRUPP STEEL USA and have been included in this Test Certificate solely for your information.

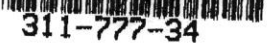
Figure A-11. Z-Post Chemical Report, Test Nos. MWP-4, MWP-6 and MWP-7

2-05 14:13

FROM-

T-094 P.02/03 F-176

LAKE ERIE SCREW CORPORATION



311-777-34

TEST REPORT

13001 ATHENS AVENUE
CLEVELAND, OHIO 44107
T 216 521 1800
F 216 228 4520

$\frac{5}{16}$ -18 X 1" X 2 1/4 Round Bend U Bolt

3281 WEST COUNTY ROAD 215
FRANKFORT, INDIANA 4604 0900
T 765 654 0477
F 765 654 0857

SAE J429 Grade 5 ORDER INFORMATION



Date: 03/15/01

Cust PO: 194802

Certification#: LE23743300300500233137

Lot Nbr: 00233137

Quantity: 534 Pieces

KANEBRIDGE CORPORATION
153 BAUER DRIVE
OAKLAND NJ 07436-3150

PART INFORMATION

Part Number: 31112CH5L
Description: NC5 5/16-18 X 7
Finish: ZINC 0.00015" MIN.

Headmarking: LE 3 RADIALS
HEX CAP SCREW

RAW MATERIAL ANALYSIS

Steel Heat Nbr: CR137970	Steel Supplier: CHARTER STEEL	Steel Grade: LESC 4037M (1), LE 1.1
C 0.37	Mn 0.80	P 0.01
S 0.012	Si 0.29	Cr 0.32
Mo 0.18	Cu 0.07	Ni 0.06
Al 0.041		

MECHANICAL PROPERTIES

10 ⁴ Wedge	Tensile Strength Psi	Proof Load Test Lbs	Elong	Superficial R30N	Core Rc
High	139000			51.0	30.0
Low	136000			48.0	25.0
Avg	137600			49.6	28.0

CERTIFICATION TEST RESULTS INCLUDE THOSE REPORTED BY THE FOLLOWING ACCREDITED LABORATORIES:
LAKE ERIE SCREW- LAKEWOOD LAB
CHARTER STEEL

Applicable Standards, Specifications, and Sampling Schemes:
ANSI B18.2.1
SAE J429 Grade 5, ASTM F606, E8, E18, F1470, ASME B18.18.7M

The listed standards, specifications, and sampling schemes are of the revision in effect on the date of manufacture unless noted otherwise.

DEVIATIONS FROM TEST METHODS
None

This lot has been found to conform to the requirements of the above standards and specifications.

Certification Mailed to Bill-to address

We certify that the product named by Lake Erie Screw Corporation was manufactured, sampled, tested, and inspected in accordance with the standards and specifications listed above and with the Lake Erie Screw Corporation Quality Manual in effect as in the case of rework. The above data accurately represents values provided by Lake Erie Screw Corporation's suppliers and are not intended to be used for any other purpose. The above data accurately represents values provided by Lake Erie Screw Corporation's suppliers and are not intended to be used for any other purpose. The above data accurately represents values provided by Lake Erie Screw Corporation's suppliers and are not intended to be used for any other purpose.

Lake Erie Screw Corporation

Jerry Mink
Jerry Mink
Quality Manager

Figure A-12. $\frac{5}{16}$ in. (8 mm) Round U bolt, Test Nos. MWP-4, MWP-6 and MWP-7

SUPERIOR WASHER AND GASKET CORP.
170 Adams Avenue
Hauppauge, New York 11788
Phone: (631) 273-8282
Fax: (631) 273-8088
E-Mail: swg@superiorwasher.com
Web: superiorwasher.com
(In the East)

SUPERIOR WASHER AND GASKET CORP.
662 Bryant Blvd.
Rock Hill, South Carolina 29732
Phone: (803) 366-3250
Fax: (803) 366-3511
E-Mail: swg@superiorwasher.com
Web: superiorwasher.com
(In the South)

ACCURATE MANUFACTURE GROUP

P.O. BOX 7232 - DEPT. 168

INDIANAPOLIS, IN 46206

Customer Purchase Order Number 9454		Superior Order Number 504612-1	Superior Lot Number 504612 - 1	Tracer No. SC31483 -3 /21153114
Date 04-02-13	Production Card 175383	Part Number WASB12NZ		Quantity 15,000
Drawing P/N S-1/2TYBNZ A		Dual Cert No.		

We hereby certify that all materials and processes conform to the required drawing specifications and that the parts have been manufactured in the U.S.A.
All parts are manufactured in a Mercury-free environment

Material

1008 LOW CARBON STEEL No. 5

ZINC TRIVALENT CHROMIUM

Chemical Analysis

C	CARBON	.0700
Mn	MANGANESE	.3300
P	PHOSPHORUS	.0080
S	SULPHUR	.0070
Si	SILICON	.0100
Cr	CHROMIUM	.0200
Ni	NICKEL	.0100
Mo	MOLYBDENUM	.0100
Cu	COPPER	.0200
Fe	IRON	
Ti	TITANIUM	
Co	COBALT	
N	NITROGEN	
Cb	COLUMBIUM	
Al	ALUMINUM	.0430
Sn	TIN	
Mg	MAGNESIUM	
Zn	ZINC	
Pb	LEAD	
Va	VANADIUM	

Mechanical Properties

Yield	
Tensile	
Elongation	
Hardness	B 49.0
Heat	4179170
Magnetic	
Permeability	
Bend Test	

SUPERIOR WASHER & GASKET CORP.

By *Richard Anderson, Jr.*
Richard Anderson, Jr.
Quality Control Manager

Figure A-13. 1/2 in. (13 mm) Washers, Test Nos. MWP-4, MWP-6 and MWP-7



811 ATLANTIC STREET, NORTH KANSAS CITY, MO 64116 1-816-474-5210 TOLL FREE 1-800-892-TUBE

STEEL VENTURES, LLC dba EXLTUBE

CERTIFIED TEST REPORT

Customer: SPS - Tulsa 1050 Fort Gibson Road Catoosa OK 74015	Size: 03.00X04.00	Spec No: ASTM A500-07	Date: 03/15/2010
	Gauge: 1/4	Grade: B,C	Customer Order No: 4500135793
			B/L No: 81474184

Heat No	Yield	Tensile	Elongation
A52867	P.S.I. 58,900	P.S.I. 62,300	% 2 inch 23.50

Heat No	C.	MN.	P.	S.	SI.
A52867	0.060	0.440	0.012	0.005	0.030

We hereby certify that the above material was manufactured in the U.S.A and that all test results shown in this report are correct as contained in the records of our company. All testing and manufacturing is in accordance to A.S.T.M. parameters encompassed within the scope of the specifications denoted in the specification and grade tiles above.

STEEL VENTURES, LLC dba EXLTUBE

Steve Frerichs
Quality Assurance Manager

Figure A-14. 3x4 Tube Post, Test Nos. MWP-4, MWP-6 and MWP-7

PURCHASE REQUISITION

- INSTRUCTIONS**
 1. PLEASE PRINT OR TYPE
 2. SEND COMPLETED REQUISITION TO PURCHASING
 EITHER BY MAIL OR FAX. DO NOT SEND TO THE
 VENDOR.
 3. GL BUDGET ACCOUNT CODES ARE FOUND IN THE
 CHART OF ACCOUNTS, AVAILABLE FROM
 ACCOUNTING.
 4. PROVIDE VENDOR FAX NUMBER TO EXPEDITE ORDER:

PO NUMBER Sending Bill
 REQ. TRACKING NUMBER 10-0153

SUGGESTED VENDOR
 NAME, COMPANY Design & Fabrication
 STREET ADDRESS 9930 N134th Street

REQUIRED DELIVERY DATE (MONTH/DAY/YEAR) _____ CITY, STATE, ZIP Waverly, NE 68462

FOR PURCHASING ONLY:
 VENDOR # _____ ORDER TYPE _____ PURCHASING GRP/BUYER _____
 PLANT _____ STORAGE LOCATION _____ MATERIAL GROUP _____ Q _____
 FOB _____ TERMS _____ INVOICE MATCHING _____

SHORT TEXT/DESCRIPTION	QUANTITY	UNIT PRICE	TOTAL PRICE	GL ACCOUNT CODE	COST CENTER/ WBS ELEMENT
Fabrication +					4-Cable Median
Material for post 2 HTCB Upper + lower	6	52.50	315.-		↓

TODAY'S DATE 6/10/2010
 DEPARTMENT NAME Midwest Roadside Safety Facility CAMPUS ZIP _____
 REQUESTOR'S NAME Curt Meyer PHONE # 312-7677 FAX # _____ PAGER # _____

APPROVAL SIGNATURE(S) _____
 DELIVERY INSTRUCTIONS: BUILDING ABBR: ROOM NUMBER: INDIVIDUAL'S NAME: CAMPUS CODE OR DELIVERY CODE:

Figure A-15. Upper and Lower HTCB Posts, Test Nos. MWP-4, MWP-6 and MWP-7

MATERIAL CERTIFICATION REPORT

SIOUX CITY FOUNDRY
 P. O. BOX 3067
 SIOUX CITY, IA 51102-3067

SIOUX CITY FOUNDRY
 801 DIVISION
 SIOUX CITY, IA

TESTED IN ACCORDANCE WITH ASTM A6

INVOICE NO. PRODUCT PLATS
 HEAT NO. 69852 96 Pcs
 Length 20'0"

DATE 12/21/09
 Cust S-2050 -0000
 GRADE A3652950 -
 SIZE F 4 X 3/8 X 5.106

PO:120098W

CHEMICAL ANALYSIS		MECHANICAL PROPERTIES	TEST 1		TEST 2		TEST 3	
			IMPERIAL	METRIC	IMPERIAL	METRIC	IMPERIAL	METRIC
C	.16	YIELD STRENGTH	55,300 PSI	381 MPa	55,600 PSI	383 MPa	PSI	MPa
Mn	.84	TENSILE STRENGTH	78,500 PSI	541 MPa	79,300 PSI	547 MPa	PSI	MPa
P	.009	ELONGATION	29.0 %	29.0 %	26.0 %	26.0 %	%	%
S	.033	GAUGE LENGTH	8 in	203 mm	8 in	203 mm	in	mm
Si	.18	BEND TEST DIAMETER	d	d	d	d	d	d
Cu	.15	BEND TEST RESULTS						
Ni	.12	SPECIMEN AREA	sq in	sq mm	sq in	sq mm	sq in	sq mm
Cr	.10	REDUCTION OF AREA	%	%	%	%	%	%
Mo	.027	IMPACT STRENGTH	ft-lbs	J	ft-lbs	J	ft-lbs	J
Cl	.012							
V	.000							
B								
Al								
Sn	.005							
N								
Ti								
CI								
CE	.34							

IMPACT STRENGTH	IMPERIAL	METRIC	INTERNAL CLEANLINESS		GRAIN SIZE HARDNESS
AVERAGE	ft-lbs	J	SEVERITY		
TEST TEMP	F	C	FREQUENCY		
ORIENTATION			RATING		REDUCTION RATIO

Customer Grade & Specs: A36 AS29 GRADE 50
 44W, CSA50W, A70936
 ASME SA36

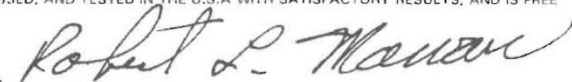
I HEREBY CERTIFY THAT THE MATERIAL TEST RESULTS PRESENTED HERE ARE FROM THE REPORTED HEAT AND ARE CORRECT. ALL TESTS WERE PERFORMED IN ACCORDANCE TO THE SPECIFICATIONS REPORTED ABOVE. ALL STEEL IS ELECTRIC FURNACE MELTED, MANUFACTURED, PROCESSED, AND TESTED IN THE U.S.A WITH SATISFACTORY RESULTS, AND IS FREE OF MERCURY CONTAMINATION IN THE PROCESS.

NOTARIZED UPON REQUEST

SWORN TO AND SUBSCRIBED BEFORE ME ON _____ DAY OF _____, 20____

IN JOHNSON COUNTY, TENNESSEE BY _____

COMMISSION EXPIRATION: _____

SIGNED 
 ROBERT L. MOWAN, QUALITY ASSURANCE MANAGER

DIRECT ANY QUESTIONS OR NECESSARY CLARIFICATIONS CONCERNING THIS REPORT TO THE SALES DEPARTMENT.

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Figure A-16. Post Baseplate, Test Nos. MWP-4, MWP-6 and MWP-7

MATERIAL CERTIFICATION REPORT

SIOUX CITY FOUNDRY
 P. O. BOX 3067
 SIOUX CITY, IA 51102-3067

SIOUX CITY FOUNDRY
 801 DIVISION
 SIOUX CITY, IA

TESTED IN ACCORDANCE WITH ASTM A6

INVOICE NO. PRODUCT PLATS
 HEAT NO. 66387 144 Pcs
 Length 20'0"

DATE 12/16/09 PO:120098W
 Cust S-2050 -0000
 GRADE A3644W
 SIZE F 2 X 1/2 X 3.404

CHEMICAL ANALYSIS	MECHANICAL PROPERTIES	TEST 1		TEST 2		TEST 3	
		IMPERIAL	METRIC	IMPERIAL	METRIC	IMPERIAL	METRIC
C .17	YIELD STRENGTH	51,600 PSI	356 MPa	52,000 PSI	359 MPa	PSI	MPa
Mn .88	TENSILE STRENGTH	74,500 PSI	514 MPa	74,400 PSI	513 MPa	PSI	MPa
P .022	ELONGATION	25.0 %	25.0 %	25.0 %	25.0 %	%	%
S .04	GAUGE LENGTH	8 in	203 mm	8 in	203 mm	in	mm
Si .17	BEND TEST DIAMETER	d	d	d	d	d	d
Co .32	BEND TEST RESULTS						
Ni .16	SPECIMEN AREA	sq in	sq mm	sq in	sq mm	sq in	sq mm
Cr .17	REDUCTION OF AREA	%	%	%	%	%	%
Mo .029	IMPACT STRENGTH	ft-lbs	J	ft-lbs	J	ft-lbs	J
Cb .000							
V .000							
B							
A							
Sr							
N							
E							

IMPACT STRENGTH	IMPERIAL	METRIC	INTERNAL CLEANLINESS		GRAIN SIZE HARDNESS
AVERAGE	ft-lbs	J	SEVERITY		
TEST TEMP	F	C	FREQUENCY		
ORIENTATION			RATING		

Customer Grade & Specs: ASTM A36 CSA G40.20/G40.21-98 GR 44W

I HEREBY CERTIFY THAT THE MATERIAL TEST RESULTS PRESENTED HERE ARE FROM THE REPORTED HEAT AND ARE CORRECT. ALL TESTS WERE PERFORMED IN ACCORDANCE TO THE SPECIFICATIONS REPORTED ABOVE. ALL STEEL IS ELECTRIC FURNACE MELTED, MANUFACTURED, PROCESSED, AND TESTED IN THE U.S.A WITH SATISFACTORY RESULTS, AND IS FREE OF MERCURY CONTAMINATION IN THE PROCESS.

NOTARIZED UPON REQUEST:
 SWORN TO AND SUBSCRIBED BEFORE ME ON _____ DAY OF _____, 20____
 IN ROANE COUNTY, TENNESSEE BY _____
 COMMISSION EXPIRATION: _____

SIGNED Robert L. Mowan
 ROBERT L. MOWAN, QUALITY ASSURANCE MANAGER

DIRECT ANY QUESTIONS OR NECESSARY CLARIFICATIONS CONCERNING THIS REPORT TO THE SALES DEPARTMENT.

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Figure A-17. Cable Retainer Post, Test Nos. MWP-4, MWP-6 and MWP-7



CONCRETE INDUSTRIES, INC.
 6300 Cornhusker Highway, Lincoln, NE 68529-0529
 402-434-1800 Fax: 402-434-1899
 www.ConcreteIndustries.com

Customer Receipt

Driver: _____
 Truck #: _____
 Ordered By: CALL

Bill To:
 91123 UNIVERSITY OF NEBRASKA
 MIDWEST RDSIDE SAFETY FACILITY
 W328.1 NEBRASKA HALL
 PO BOX 880529
 LINCOLN NE 68588-0529

Ship To:
 UNIVERSITY OF NEBRASKA
 MIDWEST RDSIDE SAFETY FACILITY
 W328.1 NEBRASKA HALL
 PO BOX 880529
 LINCOLN NE 68588-0529

Ship From:
 CONCRETE INDUSTRIES
 6300 CORNHUSKER HWY
 LINCOLN NE 68507

ATTN: KEN KRENK

Delivery Directions:

--	--

09:01 Order Number: SP 1195733 0 Delivery Date: 05/11/10 Customer PO Number:

Line	Item Description	Picked	Ordered	Back Order	Units	Unit Price	Discount	Extension
1	#11 STOCK REBAR GRADE 60 R1160		1,700.00		LB			
2	#11 REBAR FABRICATED / CUT 11FAB 32 PCS #11 X 10'-0 STR		1,700.00		LB	GERDAU	M652	732
3	#3 STOCK REBAR GRADE 60 R360		104.00		LB			
4	#3 REBAR FABRICATED / CUT 3FAB 16 PCS #3 X 4'-0 STR		104.00		LB	GERDAU	22526	780
5	#4 STOCK REBAR GRADE 60 R460		104.00		LB			
6	#4 REBAR FABRICATED / CUT 4FAB		104.00		LB	EVRAZ	5340	73
7	LIGHT BENDING CHARGE LBCHG 24 PCS #4 X 6'-6 BENT		104.00		LB			
8	24" FORM TUBE 67508 1 PCS 24" DIAMETER X 4'-0" FORM TUBE		4.00		FT			
9	12" FORM TUBE 67503 1 PCS 12" DIAMETER X 4'-0" FORM TUBE		4.00		FT			
10	#4 STOCK REBAR GRADE 60 20'-0" R46020		35.00		EA	GERDAU	1186	1680

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Received by _____

Print Name/Company _____

Returns: No returns w/o invoice. No returns on unusable material, seconds, architectural, decorative, all special order materials, and fractional units. All returnable materials subject to 50% restocking charge. No returns accepted after 30 days from date of purchase.

Terms: All invoices must be paid within 30 days of invoice. Past due accounts will be charged an interest rate of 1.33% per month which is 16% per year.

Tax Code:
 Total Weight: 2,404.80
 Total Cubic:

Sub Total:
 Sales Tax:
 Total Amount:
 Down Payment:
 Balance Due:

Document: 0 0 Print Date: 05/10/10 Print Time: 11:45 Page: 1 kathys

Figure A-18. Rebar for Anchorage, Test Nos. MWP-4, MWP-6 and MWP-7



ST PAUL STEEL MILL
1678 RED ROCK ROAD
ST PAUL MN 55119 USA
(651) 731-5600

Chemical and Physical Test Report
MADE IN UNITED STATES

M-075139

SHIP TO NEBCO, INC. STEEL DIVISION HAVELOCK, NE 68521	INVOICE TO CONCRETE INDUSTRIES INC ACCOUNTS PAYABLE PO BOX 29529 LINCOLN, NE 68529-0529	SHIP DATE 10/09/09 CUST. ACCOUNT NO 60052172
---	--	---

PRODUCED IN: ST PAUL

SHAPE + SIZE	GRADE	SPECIFICATION												SALES ORDER	CUST P.O. NUMBER
X36MM REBAR (#11)	420 (60)	A615/A615M-09 GR 60/420 A6/A6M-08a												9193731-01	79682-01
HEAT I.D.	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Sn				
M692732	.44	1.22	.013	.029	.22	.26	.11	.14	.034	.004	.014				
Mechanical Test:		Yield 64400 PSI, 444.02 MPA Load 100 KIPS Tensile: 110300 PSI, 760.49 MPA %El: 15.6/8in, 15.6/203.2mm Bend: OK													
Customer Requirements		SOURCE: GA-STP CASTING: STRAND CAST													

This material, including the billets, was produced and manufactured in the United States of America

Bhaskar Yalamanchili
Quality Director
Gerdau Ameristeel

THE ABOVE FIGURES ARE CERTIFIED EXTRACTS FROM THE ORIGINAL CHEMICAL AND PHYSICAL TEST RECORDS AS CONTAINED IN THE PERMANENT RECORDS OF COMPANY.

Metallurgical Services Manager
ST PAUL STEEL MILL

Seller warrants that all material furnished shall comply with specifications subject to standard published manufacturing variations. NO OTHER WARRANTIES, EXPRESSED OR IMPLIED, ARE MADE BY THE SELLER, AND SPECIFICALLY EXCLUDED ARE WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR PURPOSE. In no event shall seller be liable for indirect, consequential or punitive damages arising out of or related to the materials furnished by seller. Any claim for damages for materials that do not conform to specifications must be made from buyer to seller immediately after delivery of same in order to allow the seller the opportunity to inspect the material in question.

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Figure A-19. #11 Rebar for Anchorage, Test Nos. MWP-4, MWP-6 and MWP-7

7286072 P



ROCKY MOUNTAIN STEEL
A DIVISION OF EVRAZ INC. NA

P.O. Box 316
Pueblo, CO 81002 USA

MATERIAL TEST REPORT

Date Printed: 07-MAY-10

Date Shipped: 07-MAY-10	Product: DEF 13mm #4	Specification: ASTM-A-615M08b GR 420/ASTM-A-706M08a
FWIP: 52815348	Customer: CONCRETE INDUSTRIES INC	Cust. PO: 82444

Heat Number	CHEMICAL ANALYSIS															
	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al	V	B	Cb	Sn	N	Ti
534073	0.27	1.26	0.013	0.009	0.24	0.27	0.08	0.13	0.019	0.003	0.038	0.0005	0.000	0.013	0.0083	0.002
Carbon Equivalent = 0.500																

Heat Number	Sample No.	MECHANICAL PROPERTIES					Bend	Wt/r
		Yield (Psi)	Ultimate (Psi)	Elongation (%)	Reduction (%)			
534073	01	67005	98190	15.4		ok	0.663	
		(MPa) 462.0	677.0					
534073	02	67313	96890	16.1		ok	0.665	
		(MPa) 464.1	668.0					

All melting and manufacturing processes of the material subject to this test certificate occurred in the United States of America.
ERMS also certifies this material to be free from Mercury contamination.

This material has been produced and tested in accordance with the requirements of the applicable specifications. We hereby certify that the above test results represent those contained in the records of the Company.

Quality Assurance Department

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Figure A-20. #4 Rebar for Anchorage, Test Nos. MWP-4, MWP-6 and MWP-7

May 17, 2016
MwRSF Report No. TRP-03-327-16

Bill To:
 CONCRETE INDUSTRIES, INC.
 P.O. BOX 29529
 LINCOLN
 68529

Ship To: 1
 CONCRETE INDUSTRIES, INC.
 6300 CORNHUSKER HIGHWAY
 LINCOLN NE
 US

Order Date: 02/19/2010
 PO No: 81224
 Mill Order No: 3703679
 Load No: 1293276
 Manifest No: 1993673

CERTIFIED MATERIAL TEST REPORT
GERDAU AMERISTEEL
 Midlothian Mill
 300 Ward Road
 Midlothian, TX 76065
 (972) 775-8241

SPECIFICATIONS		SIZE # 3 REBAR/10 MM / 10 MM	GRADE 60/420	LENGTH 40 FT / 12.192 M	PRODUCT REBAR							
ASTM A615/A615M-09												
HEAT NO: 22526780		<u>CHEMICAL ANALYSIS</u>										
C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Sn	V	Al	Nb
.46	.86	.016	.038	.25	.34	.11	.14	.020	.014	.002	.004	.005
<u>Yield Strength</u>		<u>Tensile Strength</u>		<u>Specimen Area</u>		<u>Elongation</u>		<u>Bend Test</u>		<u>ROA</u>		
KSI	MPa	KSI	MPa	Sq In	Sq cm	%	Gage Length	Dia. Result				
67.0	461.9	106.3	732.9	0.110	0.71	15.3	8 In 200 mm	3.5 PASS				

All manufacturing processes of this product, including electric arc MELTING and continuous CASTING, occurred in the U.S.A. CMTR complies with EN 10204 3.1

"I hereby certify that the contents of this report are correct and accurate. All tests and operations performed by this material manufacturer or its sub-contractors, when applicable, are in compliance with the requirements of the material specifications and applicable purchaser designated requirements."

Signed: Tom L. Harrington Date: Mar. 01, 2010 Signed: _____ Date: _____
 Tom L. Harrington: Quality Assurance Manager Notary Public (if applicable) Page: 1 of 1

Figure A-21. #3 Rebar for Anchorage, Test Nos. MWP-4, MWP-6 and MWP-7

26Apr12 9:26 TEST CERTIFICATE No: MAR 877775

INDEPENDENCE TUBE CORPORATION P/O No 4500179833
6226 W. 74TH STREET Rel
CHICAGO, IL 60638 S/O No MAR 212696-001
Tel: 708-496-0380 Fax: 708-563-1950 B/L No MAR 123862-004 Shp 23Apr12
Inv No Inv

Sold To: (5017) Ship To: (1)
STEEL & PIPE SUPPLY STEEL & PIPE SUPPLY
401 NEW CENTURY PARKWAY 401 NEW CENTURY PKWY
KANSAS CITY WHSE. NEW CENTURY, KS 66031
NEW CENTURY, KS 66031

Tel: 913-768-4333 Fax: 913 768-6683

CERTIFICATE of ANALYSIS and TESTS Cert. No: MAR 877775
19Apr12

Part No
TUBING A500 GRADE B(C)
4" X 3" X 1/4" X 40' Pcs Wgt
20 8,408

Heat Number Tag No Pcs Wgt
E200931 621072 20 8,408
YLD=69070/TEN=81790/ELG=23.9

Heat Number *** Chemical Analysis ***
E200931 C=0.2000 Mn=0.4500 P=0.0120 S=0.0020 Si=0.0300 Al=0.0330
Cu=0.1200 Cr=0.0400 Mo=0.0100 V=0.0010 Ni=0.0400

WE PROUDLY MANUFACTURE ALL OF OUR HSS IN THE USA.
INDEPENDENCE TUBE PRODUCT IS MANUFACTURED, TESTED,
AND INSPECTED IN ACCORDANCE WITH ASTM STANDARDS.

CURRENT STANDARDS:
.....A500/A500M-10a
.....A513-07
.....A252-98 (2002)

Figure A-22. Foundation Tubes, Test Nos. MWP-4, MWP-6 and MWP-7

AUG/23/2012/THU 02:08 PM TSA MANUFACTURING

FAX No. 4028953297

P. 001/001

P.O. # 145117

PO# 30078 SO# 89068

Item: 3/4-10 X 18 1/4 J HOOK ANCHOR			
Material Specification: ASTM A449			
LOT#:	11618020		
Heat Number:	11618020		
Tensile Strength PSI:	131800 PSI	Yield Strength PSI:	121800 PSI
Elongation:	20	Reduction of Area:	58
Hardness:	27 HRC	Proof Load:	NA
Macro Etch:	NA	Tempering Temp.:	1340 F

Carbon (C):	0.44	Chromium (CR):	NA
Manganese (MN):	0.71	Molybdenum (MO):	NA
Phosphorus (P):	0.013	Copper (CU):	NA
Sulfur (S):	0.034	Nitrogen (N):	NA
Silicon (SI):	0.19	Nickel (NI):	NA
Cobalt (CO):	NA	Aluminum (AL):	NA
Vanadium (V):	NA	Tin (SN):	NA
Tungsten (W):	NA	Titanium (TI):	NA
Columbium/Niobium (NB/CB):	NA	Boron (B):	NA
Calcium (CA):	NA		

We hereby certify that the material was manufactured, sampled, tested and inspected per the most recent revision of the or material specification. The foregoing data was furnished to us by our supplier or resulting from a test performed in a recognized laboratory and is on file in the records of the corporation.
Name: Kayla Patterson Date: 08.13.12

Figure A-23. J-Hook Anchor Bolts, Test Nos. MWP-4, MWP-6 and MWP-7

Certificate of Quality
BEKAERT CORPORATION Van Buren, Arkansas

1881 BEKAERT DRIVE
VAN BUREN, AR 72956
TEL(479)474-5211 FAX(479)474-9075
TELEX 537439

DATE: 06/03/2010

Customer	Midwest Roadside Safety Facili	Customer Order No	sample	
Our Order No	4060145416 0010	Qty	3	Carriers
Product	3/4" 3X7 CL A GALV GUIDERAIL SHORTS			
Customer Part No		Customer Spec No	ASTM A 741	
MFG SMP No	AST3043SE10S			

Tested g#	Diameter in	Lay Length (in.)	Breaking Load lbf	Adherence Appearance of Wires	Steel Ductility
609409	0.79	6	46525	Pass	Pass
609459	0.75	7	46548	Pass	Pass
609513	0.75	7.3	49219	Pass	Pass

Material was melted and made in the U.S.A.
The undersigned certifies that the results are actual results and conform to the specification indicated
contained in the records of this Corporation.


Process Control Manager

Notary Public Commission Expires

Figure A-24. Bekaert Wire Rope, Test Nos. MWP-4, MWP-6 and MWP-7

Appendix B. Vehicle Center of Gravity Determination

Test: MWP-4 Vehicle: Ram 1500 QC

Vehicle CG Determination

VEHICLE	Equipment	Weight (lb)	Vert CG (in.)	Vert M (lb-in.)
+	Unbalasted Truck (Curb)	5084	28.07845	142750.9
+	Brake receivers/wires	6	54	324
+	Brake Frame	7	27	189
+	Brake Cylinder (Nitrogen)	22	27	594
+	Strobe/Brake Battery	6	31	186
+	Hub	27	15	405
+	CG Plate (EDRs)	25	28	700
-	Battery	-31	38	-1178
-	Oil	-9	23	-207
-	Interior	-83	30	-2490
-	Fuel	-154	22	-3388
-	Coolant	-14	35	-490
-	Washer fluid	-6	37	-222
BALLAST	Water	87	22	1914
	Misc.			0
	Misc.			0
				139087.9

Estimated Total Weight (lb)	4967
Vertical CG Location (in.)	28.00239

wheel base (in.)	140.25		
MASH Targets	Targets	Test Inertial	Difference
Test Inertial Weight (lb)	5000 ± 110	4967	-33.0
Long CG (in.)	63 ± 4	60.60	-2.40477
Lat CG (in.)	NA	0.26549	NA
Vert CG (in.) ≥	28	28.00	0.00239

Note: Long. CG is measured from front axle of test vehicle
Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

CURB WEIGHT (lb)		
	Left	Right
Front	1486	1395
Rear	1079	1124
FRONT	2881 lb	
REAR	2203 lb	
TOTAL	5084 lb	

TEST INERTIAL WEIGHT (lb)		
(from scales)		
	Left	Right
Front	1430	1391
Rear	1034	1112
FRONT	2821 lb	
REAR	2146 lb	
TOTAL	4967 lb	

Figure B-1. Vehicle Mass Distribution, Test No. MWP-4

Test: MWP-6

Vehicle: Rio

Vehicle CG Determination

VEHICLE	Equipment	Weight (lb)
+	Unbalasted Car (curb)	2295
+	Brake receivers/wires	5
+	Brake Frame	7
+	Brake Cylinder	22
+	Strobe Battery	5
+	Hub	27
+	CG Plate (EDRs)	15
+	DTS	0
-	Battery	-31
-	Oil	-7
-	Interior	-29
-	Fuel	0
-	Coolant	-7
-	Washer fluid	-5
BALLAST	Water	108
	Misc.	
	Misc.	
Estimated Total Weight		2405 lb

wheel base 98.5 in.

MASH targets		Test Inertial	Difference
Test Inertial Wt (lb)	2420 (+/-)55	2405	-15.0
Long CG (in.)	39 (+/-)4	38.95	-0.05052
Lateral CG (in.)	N/A	0.106653	NA

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

CURB WEIGHT (lb)		
	Left	Right
Front	777	692
Rear	390	436
FRONT	1469 lb	
REAR	826 lb	
TOTAL	2295 lb	

Dummy = 166lbs.

TEST INERTIAL WEIGHT (lb)		
(from scales)	Left	Right
Front	724	730
Rear	474	477
FRONT	1454 lb	
REAR	951 lb	
TOTAL	2405 lb	

Figure B-2. Vehicle Mass Distribution, Test No. MWP-6

Test: MWP-7

Vehicle: Rio

Vehicle CG Determination

VEHICLE	Equipment	Weight (lb)
+	Unbalasted Car (curb)	2384
+	Brake receivers/wires	6
+	Brake Frame	7
+	Brake Cylinder	22
+	Strobe Battery	5
+	Hub	22
+	CG Plate (EDRs)	13
+		0
-	Battery	-31
-	Oil	-6
-	Interior	-33
-	Fuel	0
-	Coolant	-8
-	Washer fluid	-4
BALLAST	Water	
	Misc. Battery	12
	Misc.	
Estimated Total Weight		2389 lb

wheel base 98.125 in.

MASH targets		Test Inertial	Difference
Test Inertial Wt (lb)	2420 (+/-)55	2392	-28.0
Long CG (in.)	39 (+/-)4	37.49	-1.50575
Lateral CG (in.)	N/A	0.357441	NA

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

CURB WEIGHT (lb)		
	Left	Right
Front	770	744
Rear	427	443
FRONT	1514 lb	
REAR	870 lb	
TOTAL	2384 lb	

TEST INERTIAL WEIGHT (lb)		
(from scales)		
	Left	Right
Front	723	755
Rear	458	456
FRONT	1478 lb	
REAR	914 lb	
TOTAL	2392 lb	

Figure B-3. Vehicle Mass Distribution, Test No. MWP-7

Appendix C. Static Soil Tests

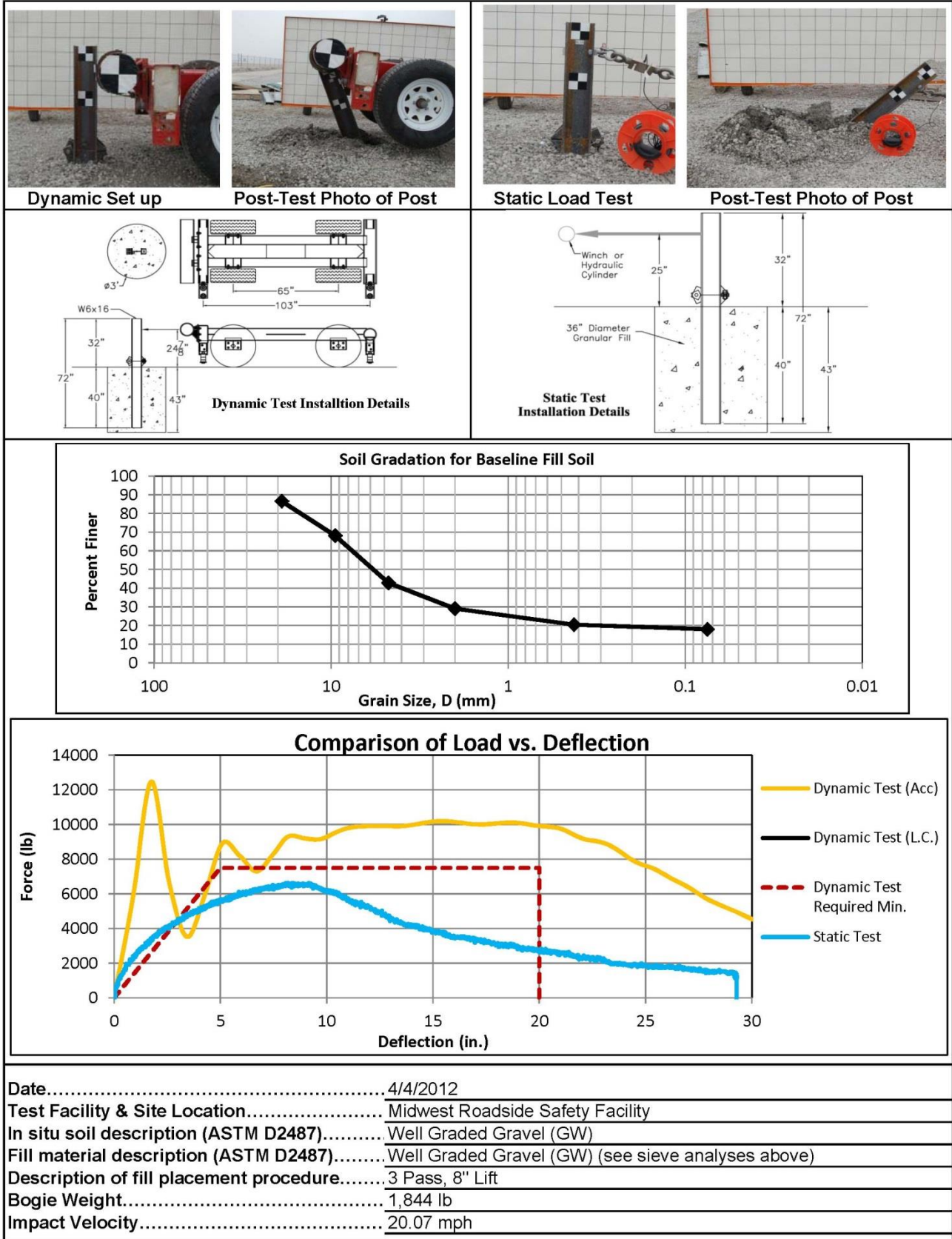


Figure C-1. Soil Strength, Initial Calibration Test, Test Nos. MWP-4, MWP-6, and MWP-7

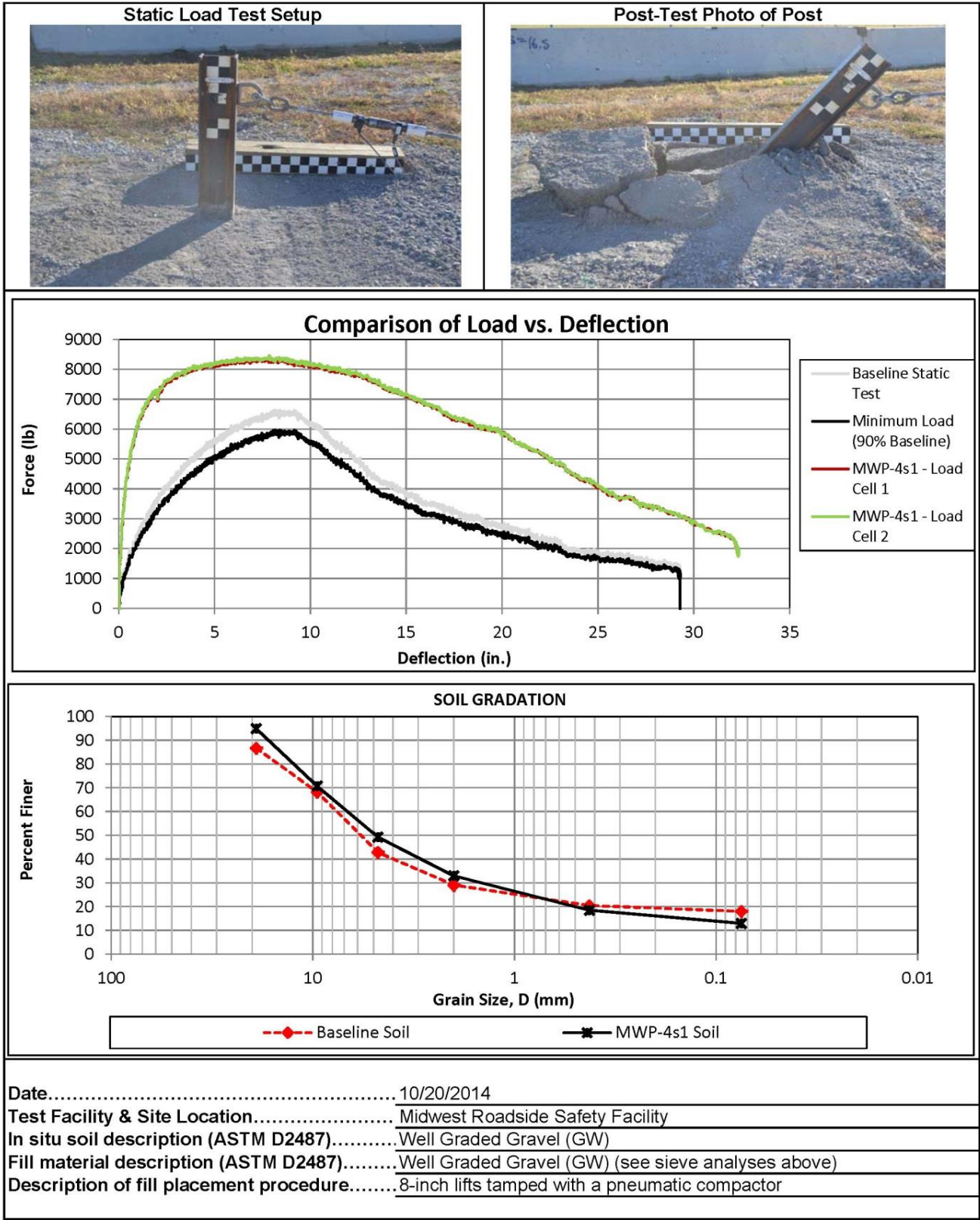
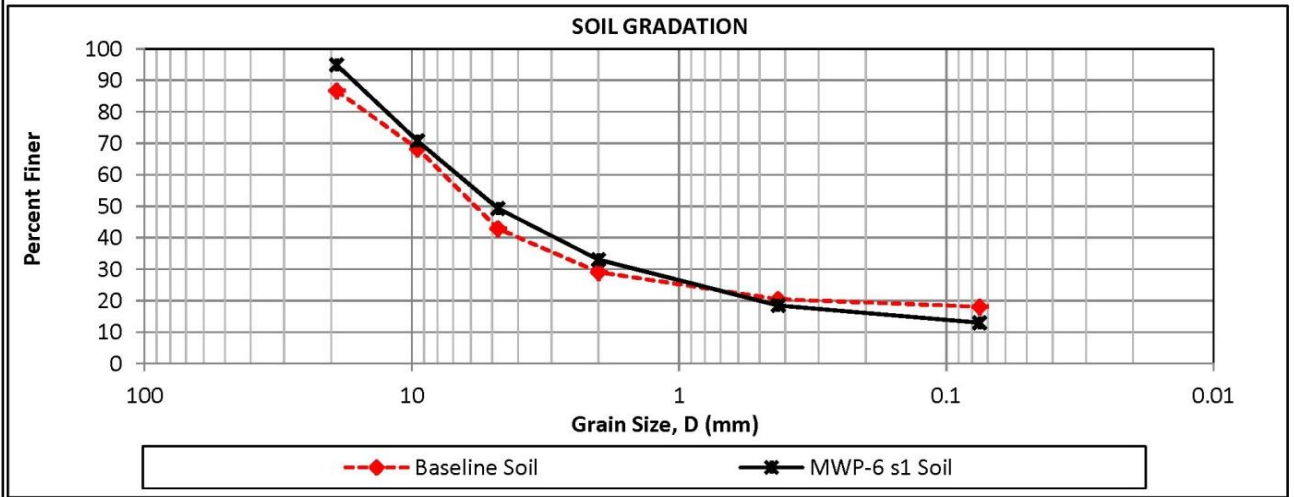
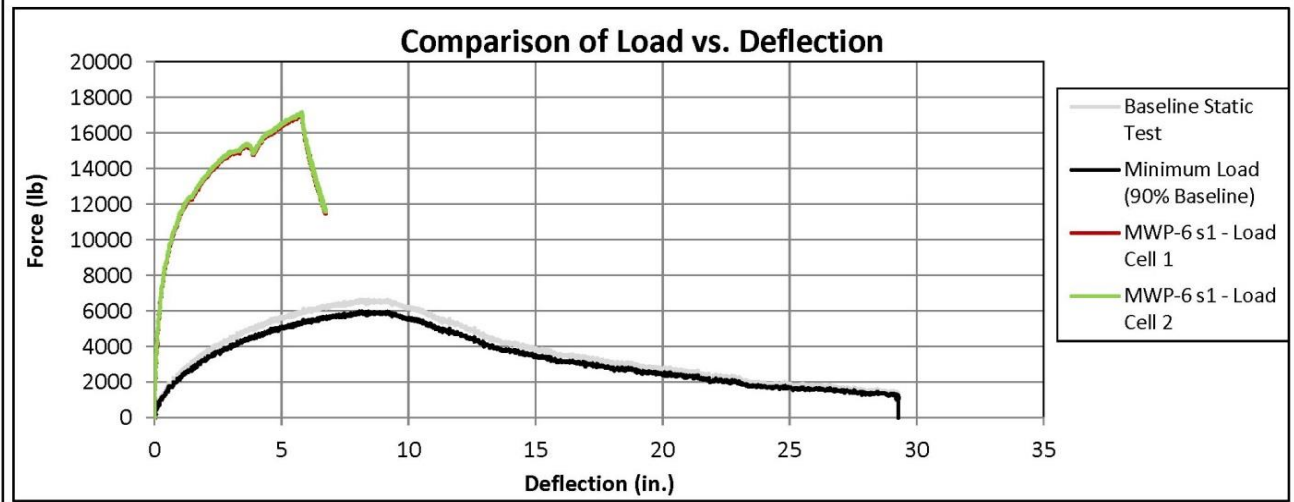
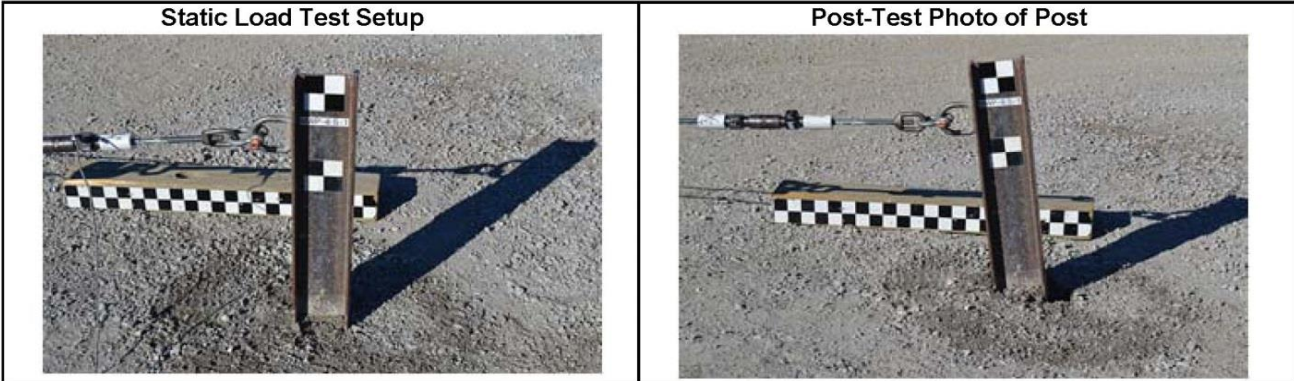
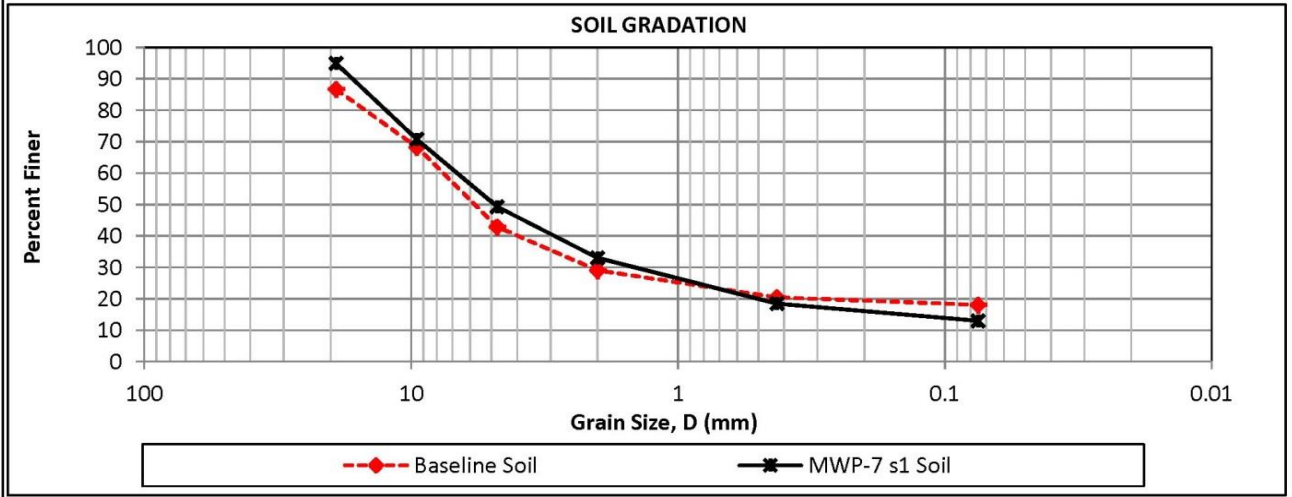
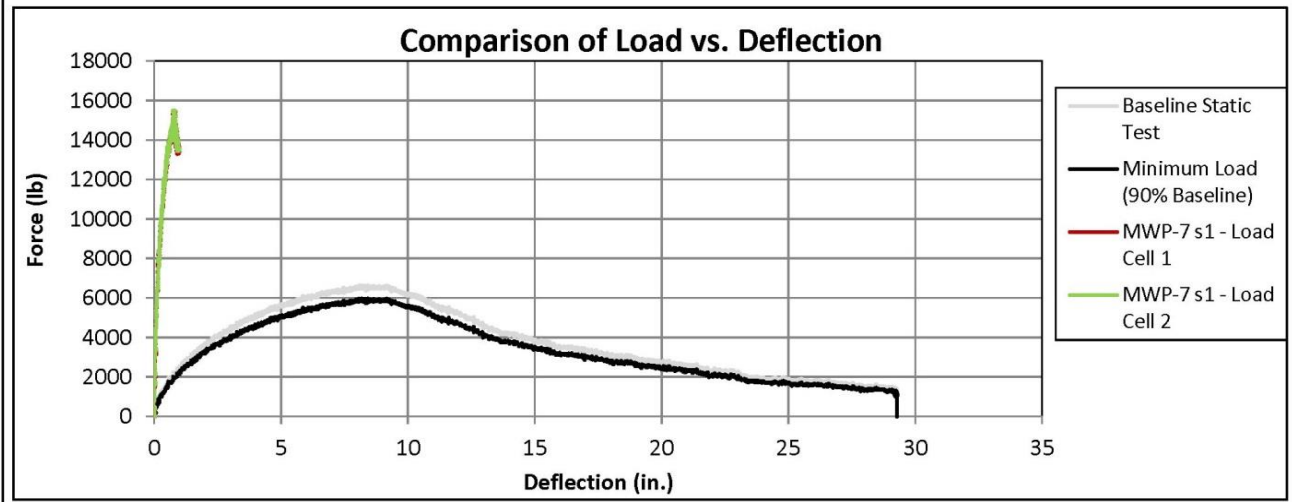
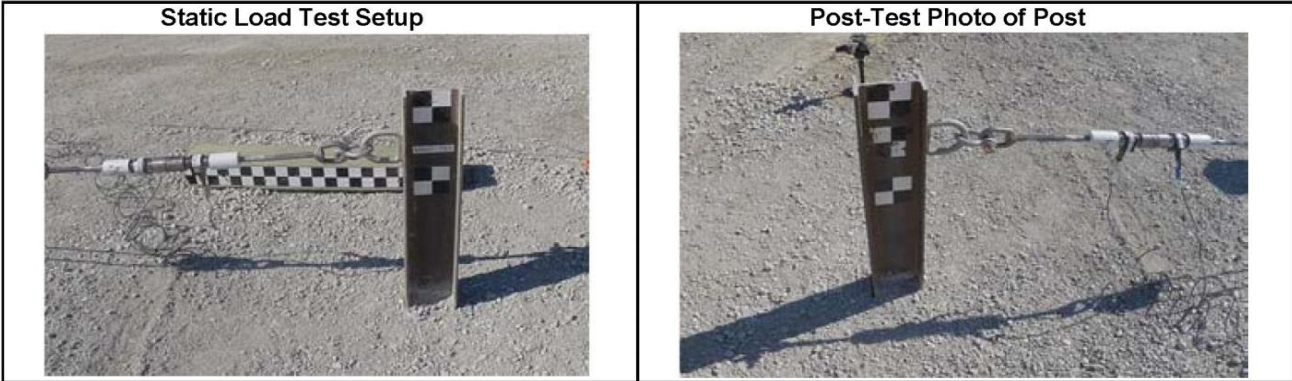


Figure C-2. Static Soil Test, Test No. MWP-4



Date.....	1/15/2015
Test Facility & Site Location.....	Midwest Roadside Safety Facility
In situ soil description (ASTM D2487).....	Well Graded Gravel (GW)
Fill material description (ASTM D2487).....	Well Graded Gravel (GW) (see sieve analyses above)
Description of fill placement procedure.....	8-inch lifts tamped with a pneumatic compactor

Figure C-3. Static Soil Test, Test No. MWP-6



Date.....	2/23/2015
Test Facility & Site Location.....	Midwest Roadside Safety Facility
In situ soil description (ASTM D2487).....	Low Plasticity Silt (ML)
Fill material description (ASTM D2487).....	Well Graded Gravel (GW) (see sieve analyses above)
Description of fill placement procedure.....	8-inch lifts tamped with a pneumatic compactor

Figure C-4. Static Soil Test, Test No. MWP-7

Appendix D. Vehicle Deformation Records

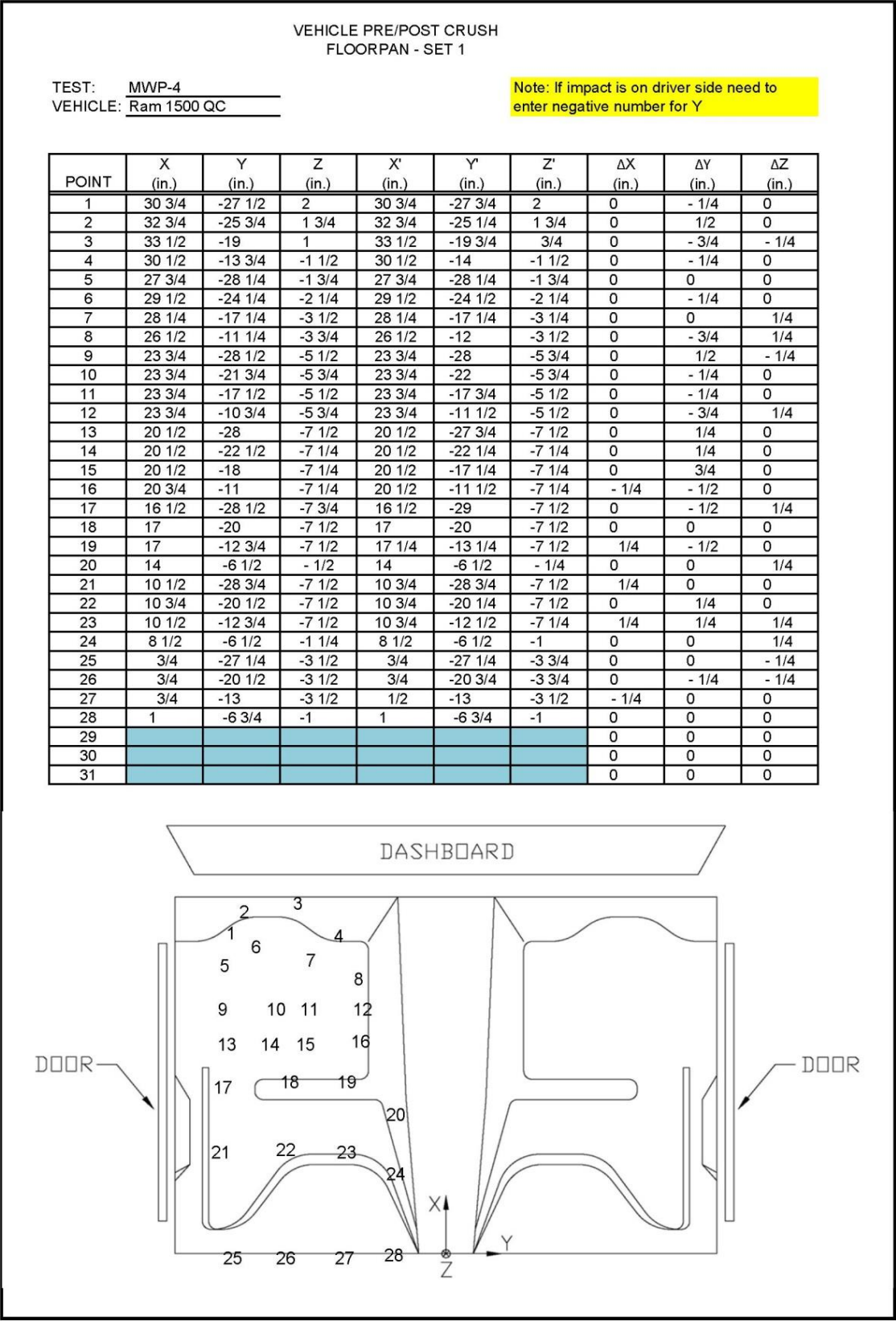


Figure D-1. Floor Pan Deformation Data – Set 1, Test No. MWP-4

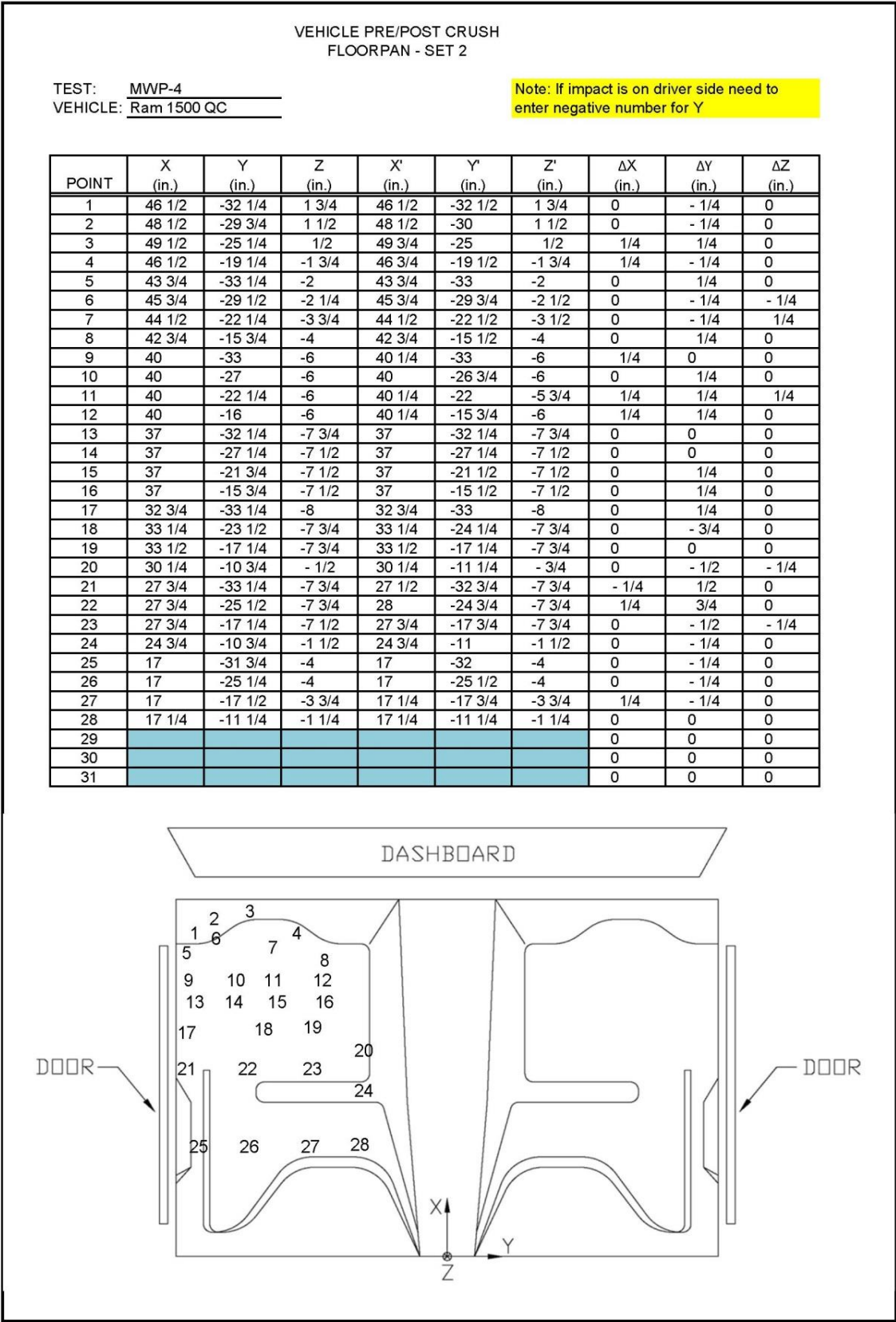


Figure D-2. Floor Pan Deformation Data – Set 2, Test No. MWP-4

VEHICLE PRE/POST CRUSH
INTERIOR CRUSH - SET 1

TEST: MWP-4
VEHICLE: Ram 1500 QC

Note: If impact is on driver side need to enter negative number for Y

	POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔY (in.)	ΔZ (in.)
DASH	A1	40	-55 1/2	25 3/4	40 1/4	-55 1/2	26	1/4	0	1/4
	A2	40	-39 3/4	26	40 1/4	-39	26	1/4	3/4	0
	A3	40	-30 1/4	26 3/4	40	-30 1/4	26 3/4	0	0	0
	A4	34 3/4	-57 1/2	19	34 3/4	-57 1/2	19	0	0	0
	A5	32	-44 3/4	15 1/2	32	-45	15 1/2	0	-1/4	0
	A6	33 1/4	-32 1/4	18 1/2	33 1/4	-32 1/2	18 1/2	0	-1/4	0
SIDE PANEL	B1	20 3/4	-25 1/2	3	20 3/4	-25 1/4	3	0	1/4	0
	B2	20	-25 1/4	-1 3/4	20	-25	-1 3/4	0	1/4	0
	B3	23	-25 3/4	1/2	23	-25 3/4	1/2	0	0	0
IMPACT SIDE DOOR	C1	8 3/4	-35 1/2	19 1/2	8 3/4	-35 3/4	19 1/2	0	-1/4	0
	C2	15 1/2	-35 1/2	19 1/2	15 1/2	-35 1/2	19 1/2	0	0	0
	C3	27	-34 1/4	18 1/4	26 1/2	-34 1/4	18 1/4	-1/2	0	0
	C4	6 1/4	-28 1/4	4 1/4	6	-28 1/4	4 1/4	-1/4	0	0
	C5	17 3/4	-29 1/4	5 1/2	17 3/4	-29	5 1/4	0	1/4	-1/4
	C6	23 1/2	-28 1/2	3	23 1/4	-27 1/2	2 3/4	-1/4	1	-1/4
ROOF	D1							0	0	0
	D2							0	0	0
	D3							0	0	0
	D4							0	0	0
	D5							0	0	0
	D6							0	0	0
	D7							0	0	0
	D8							0	0	0
	D9							0	0	0
	D10							0	0	0
	D11							0	0	0
	D12							0	0	0
	D13							0	0	0
	D14							0	0	0
	D15							0	0	0

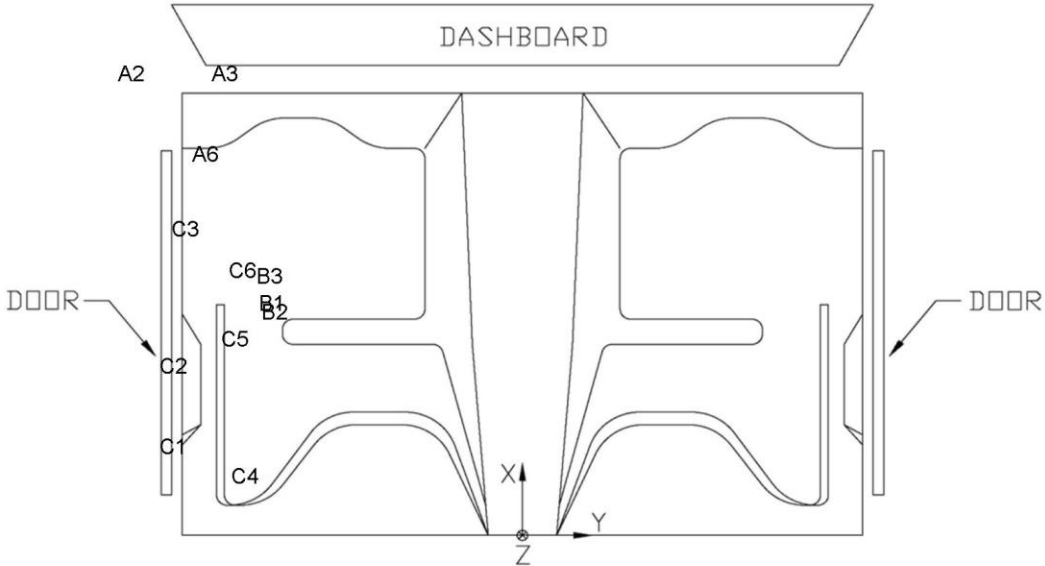


Figure D-3. Occupant Compartment Deformation Data – Set 1, Test No. MWP-4

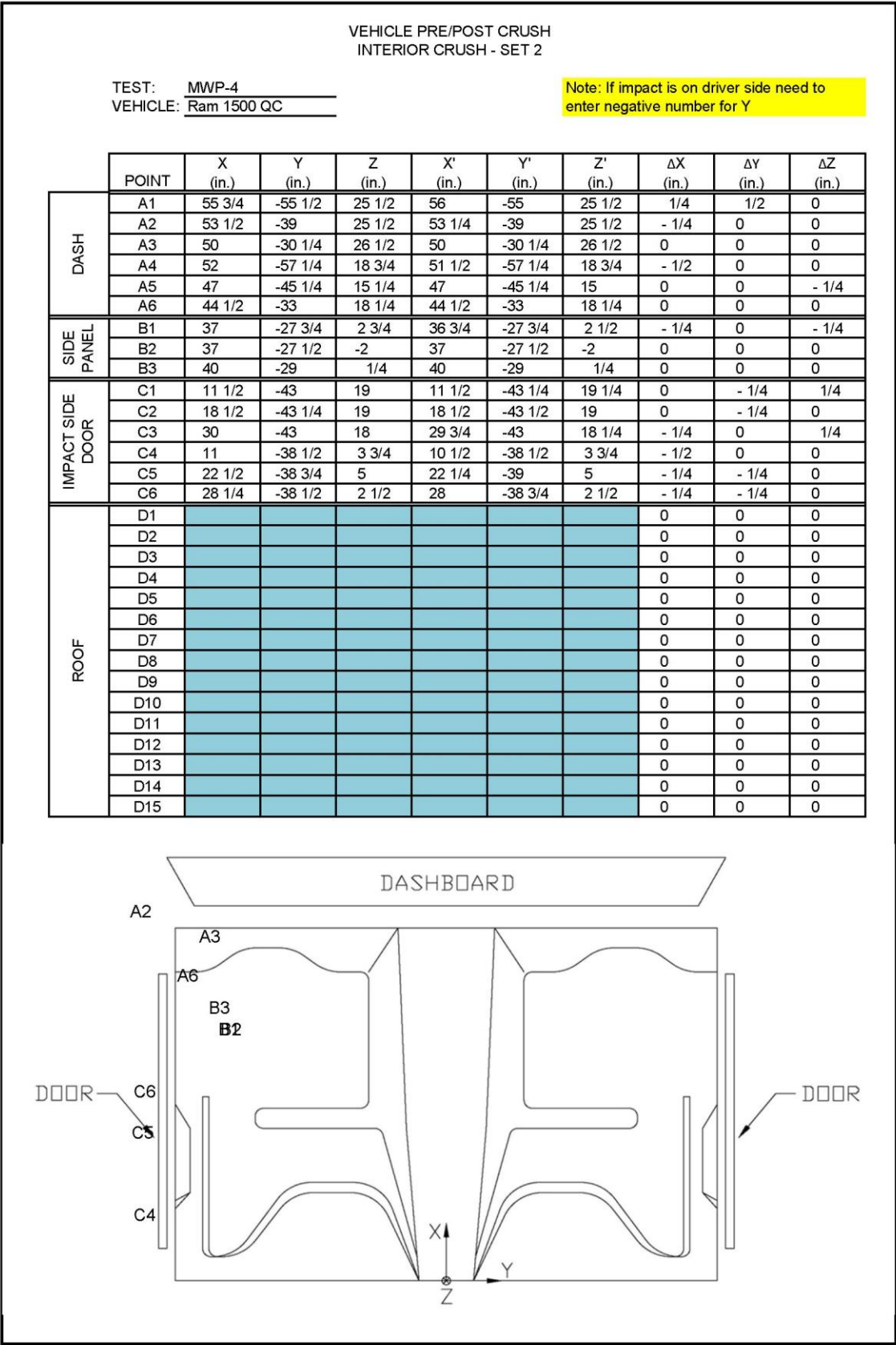


Figure D-4. Occupant Compartment Deformation Data – Set 2, Test No. MWP-4

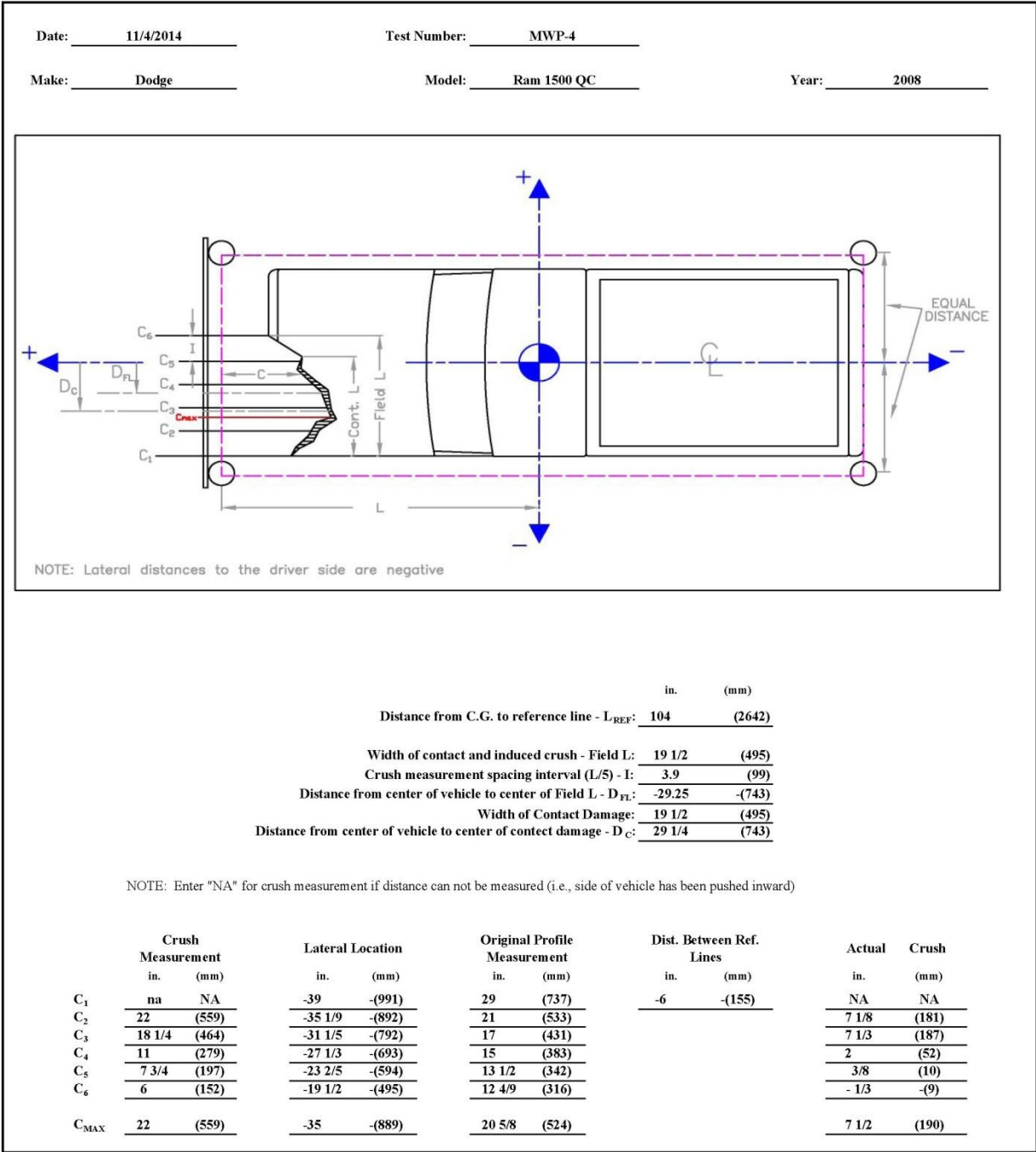


Figure D-5. Exterior Vehicle Crush (NASS) – Front, Test No. MWP-4

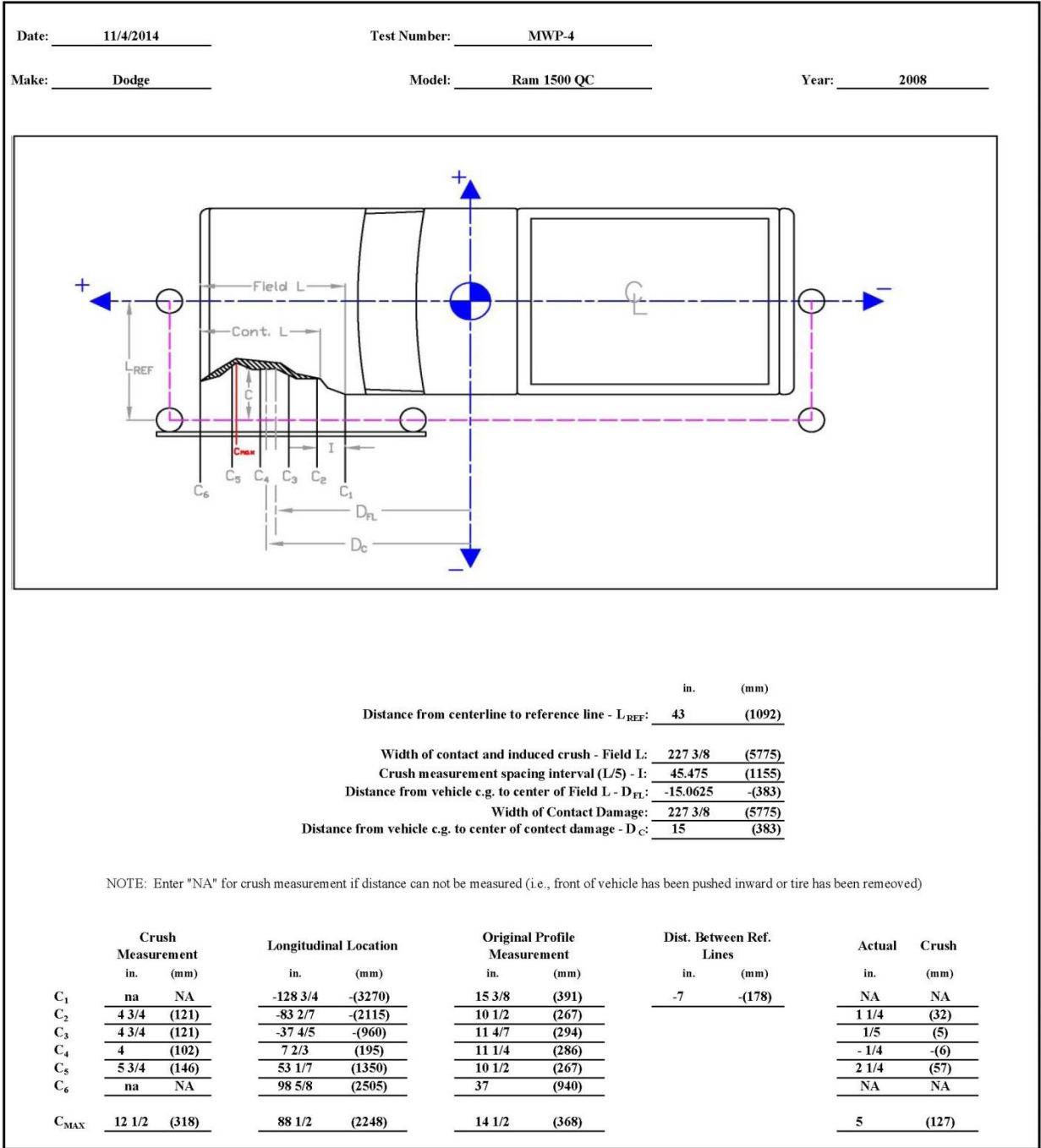


Figure D-6. Exterior Vehicle Crush (NASS) – Side, Test No. MWP-4

VEHICLE PRE/POST CRUSH
FLOORPAN - SET 1

TEST: MWP-6
VEHICLE: 2009 Kia Rio

POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔY (in.)	ΔZ (in.)
1	27.994	20.933	1.677	27.862	21.195	1.195	-0.132	0.262	-0.482
2	29.737	17.772	1.220	29.569	18.172	0.755	-0.168	0.400	-0.465
3	32.954	15.211	0.645	32.830	15.624	0.189	-0.124	0.413	-0.456
4	33.124	11.844	-0.152	33.024	12.132	-0.688	-0.100	0.289	-0.537
5	30.537	3.835	-2.707	30.488	4.208	-3.083	-0.049	0.373	-0.376
6	28.560	17.687	-2.679	28.398	18.035	-3.125	-0.163	0.347	-0.446
7	29.388	12.035	-3.424	29.268	12.390	-3.841	-0.120	0.355	-0.417
8	28.618	7.001	-3.910	28.557	7.348	-4.259	-0.061	0.347	-0.349
9	28.006	2.850	-4.273	27.972	3.188	-4.618	-0.033	0.338	-0.344
10	22.268	18.048	-6.943	22.099	18.320	-7.364	-0.169	0.272	-0.421
11	22.801	13.481	-6.685	22.659	13.757	-7.071	-0.142	0.276	-0.387
12	22.012	7.048	-7.049	21.796	7.415	-6.873	-0.216	0.367	0.176
13	16.672	21.975	-7.288	16.469	22.186	-7.699	-0.203	0.211	-0.411
14	16.574	17.745	-7.412	16.393	17.962	-7.801	-0.181	0.218	-0.390
15	16.572	12.640	-7.088	16.440	12.862	-7.436	-0.132	0.222	-0.348
16	16.439	6.620	-7.635	16.393	6.875	-6.361	-0.046	0.255	1.274
17	10.614	21.906	-7.488	10.397	22.075	-7.859	-0.217	0.170	-0.372
18	11.465	15.973	-7.044	11.326	16.151	-7.386	-0.139	0.178	-0.342
19	11.592	10.805	-7.069	11.487	11.011	-7.370	-0.105	0.206	-0.301
20	11.740	4.470	-7.654	11.584	4.741	-6.973	-0.156	0.270	0.681
21	7.140	20.615	-7.417	6.935	20.757	-7.751	-0.205	0.141	-0.334
22	7.197	15.328	-7.052	7.040	15.472	-7.362	-0.156	0.144	-0.310
23	7.921	10.947	-7.079	7.804	11.098	-7.359	-0.117	0.151	-0.280
24	8.129	4.670	-7.595	8.066	4.833	-7.613	-0.063	0.163	-0.019
25	2.061	18.731	-3.610	1.921	18.850	-3.897	-0.140	0.118	-0.287
26	1.935	14.083	-3.600	1.777	14.185	-3.871	-0.158	0.102	-0.270
27	1.904	9.988	-3.593	1.785	10.129	-3.840	-0.119	0.140	-0.247
28	1.886	4.191	-3.777	1.869	4.310	-3.982	-0.017	0.119	-0.204

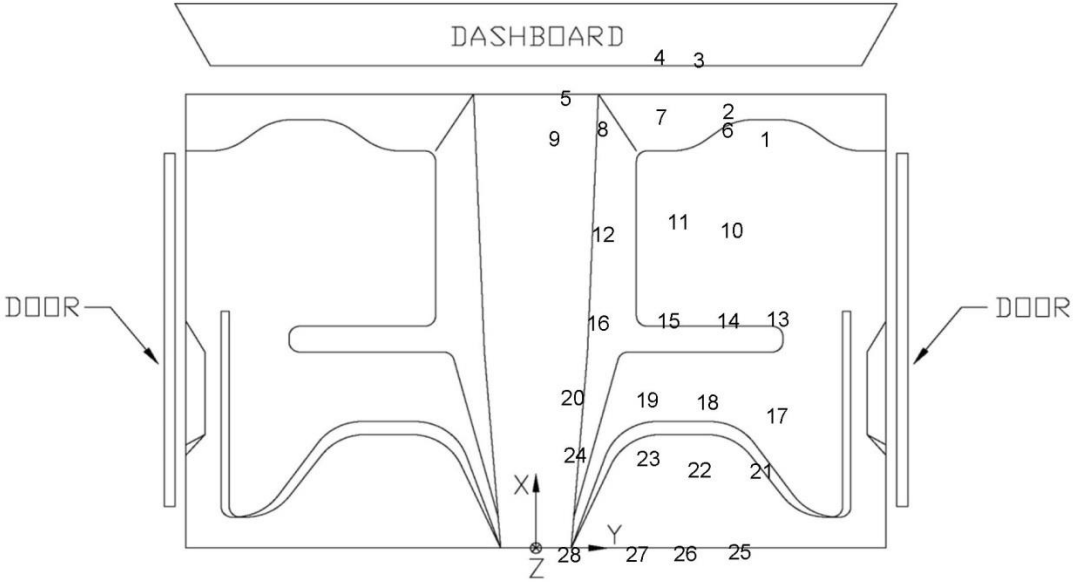


Figure D-7. Floor Pan Deformation Data – Set 1, Test No. MWP-6

VEHICLE PRE/POST CRUSH
FLOORPAN - SET 2

TEST: MWP-6
VEHICLE: 2009 Kia Rio

POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔY (in.)	ΔZ (in.)
1	37.527	25.751	1.875	37.503	25.910	1.816	-0.024	0.159	-0.059
2	39.366	22.620	1.264	39.284	22.893	1.236	-0.082	0.273	-0.028
3	42.573	20.208	0.413	42.532	20.456	0.392	-0.042	0.248	-0.021
4	42.794	16.802	-0.387	42.755	16.999	-0.470	-0.039	0.197	-0.083
5	40.200	8.706	-2.686	40.227	8.981	-2.691	0.027	0.274	-0.005
6	37.778	22.467	-2.563	37.744	22.706	-2.592	-0.034	0.240	-0.028
7	38.769	16.872	-3.302	38.741	17.119	-3.323	-0.028	0.247	-0.021
8	38.154	11.808	-3.685	38.135	12.058	-3.699	-0.019	0.250	-0.015
9	37.659	7.636	-3.973	37.637	7.883	-4.002	-0.022	0.247	-0.029
10	31.146	22.593	-6.190	31.093	22.750	-6.225	-0.053	0.157	-0.035
11	31.870	18.054	-5.958	31.842	18.299	-5.987	-0.028	0.245	-0.029
12	31.144	11.634	-6.212	31.254	11.845	-5.730	0.110	0.211	0.483
13	25.406	26.305	-6.049	25.373	26.546	-6.079	-0.033	0.241	-0.030
14	25.450	22.078	-6.142	25.419	22.322	-6.184	-0.031	0.245	-0.042
15	25.667	16.983	-5.791	25.637	17.227	-5.832	-0.030	0.244	-0.040
16	25.705	10.957	-6.293	25.798	11.340	-4.776	0.093	0.383	1.518
17	19.359	26.023	-5.699	19.329	26.267	-5.728	-0.029	0.244	-0.029
18	20.399	20.084	-5.293	20.425	20.346	-5.344	0.025	0.262	-0.051
19	20.782	14.973	-5.313	20.669	15.205	-5.344	-0.113	0.232	-0.031
20	21.107	8.640	-5.876	21.063	8.954	-4.963	-0.043	0.314	0.913
21	15.970	24.612	-5.303	15.943	24.860	-5.329	-0.028	0.248	-0.026
22	16.239	19.329	-4.921	16.210	19.570	-4.963	-0.030	0.241	-0.042
23	17.150	14.926	-4.994	17.087	15.224	-5.029	-0.064	0.298	-0.035
24	17.509	8.708	-5.493	17.507	8.968	-5.312	-0.002	0.260	0.182
25	11.313	22.558	-1.047	11.303	22.817	-1.071	-0.010	0.259	-0.024
26	11.351	17.921	-1.003	11.313	18.141	-1.040	-0.038	0.220	-0.037
27	11.449	13.852	-0.974	11.445	14.107	-1.019	-0.003	0.254	-0.045
28	11.653	8.026	-1.123	11.647	8.263	-1.170	-0.006	0.237	-0.047

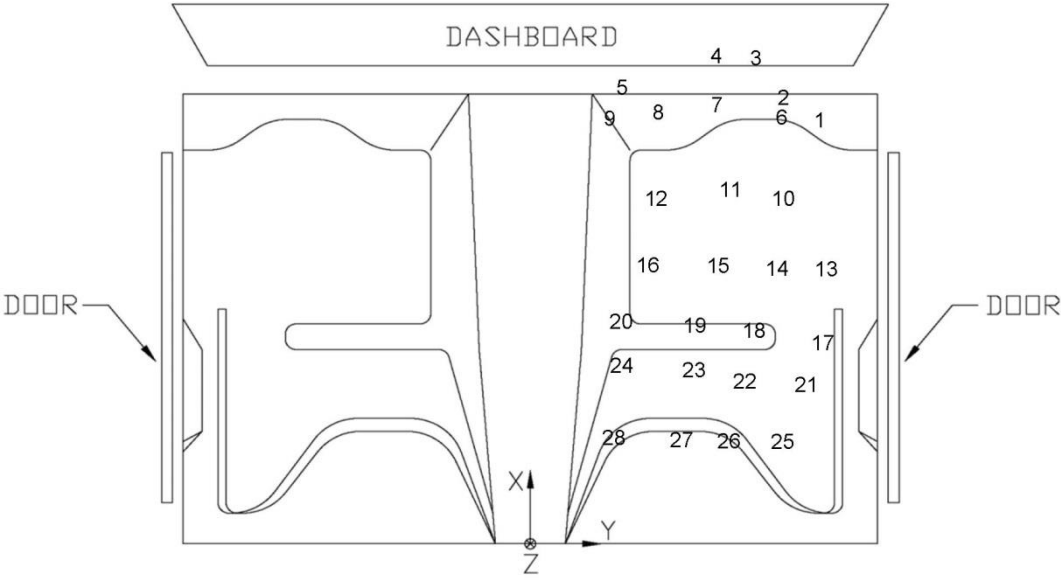


Figure D-8. Floor Pan Deformation Data – Set 2, Test No. MWP-6

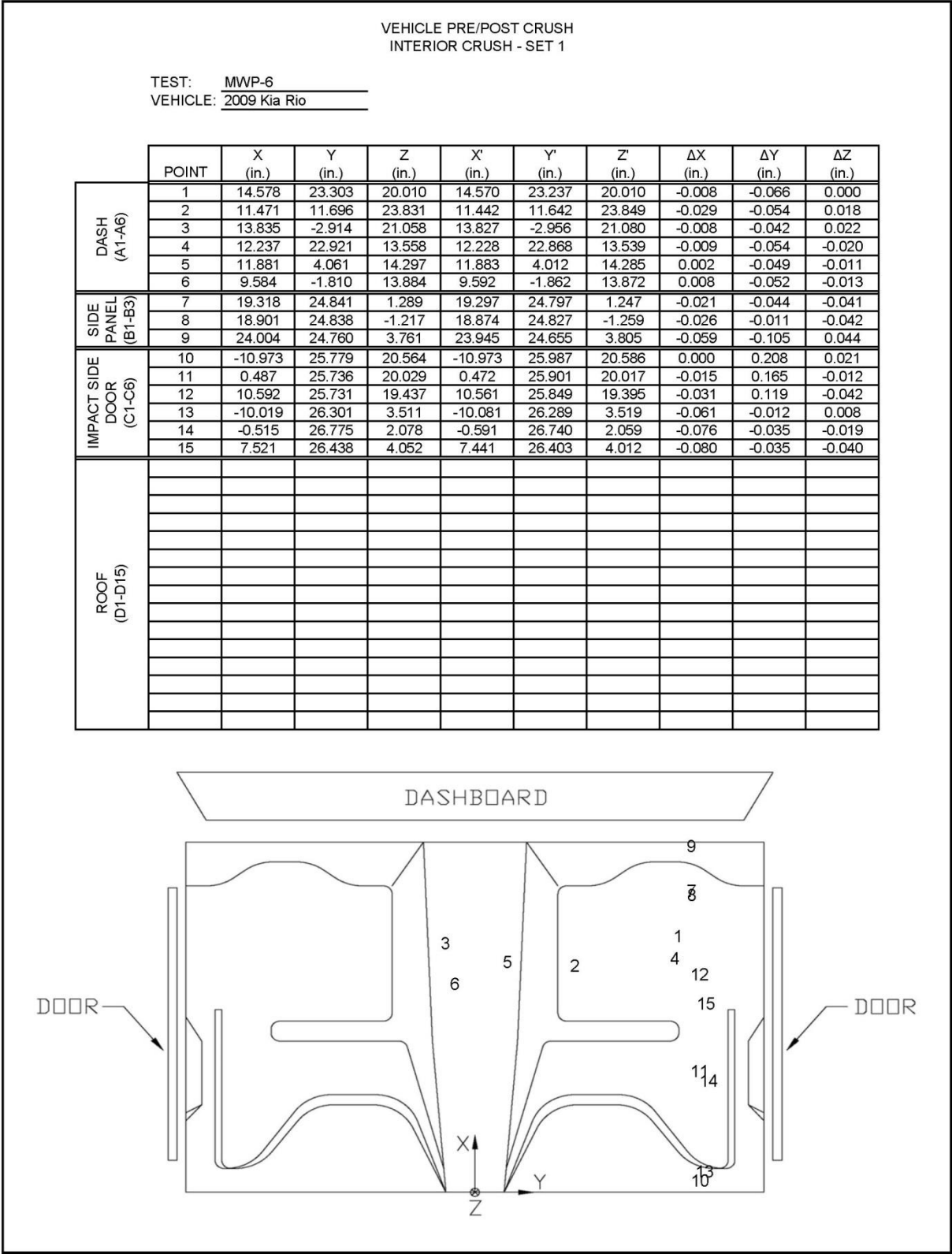


Figure D-9. Occupant Compartment Deformation Data – Set 1, Test No. MWP-6

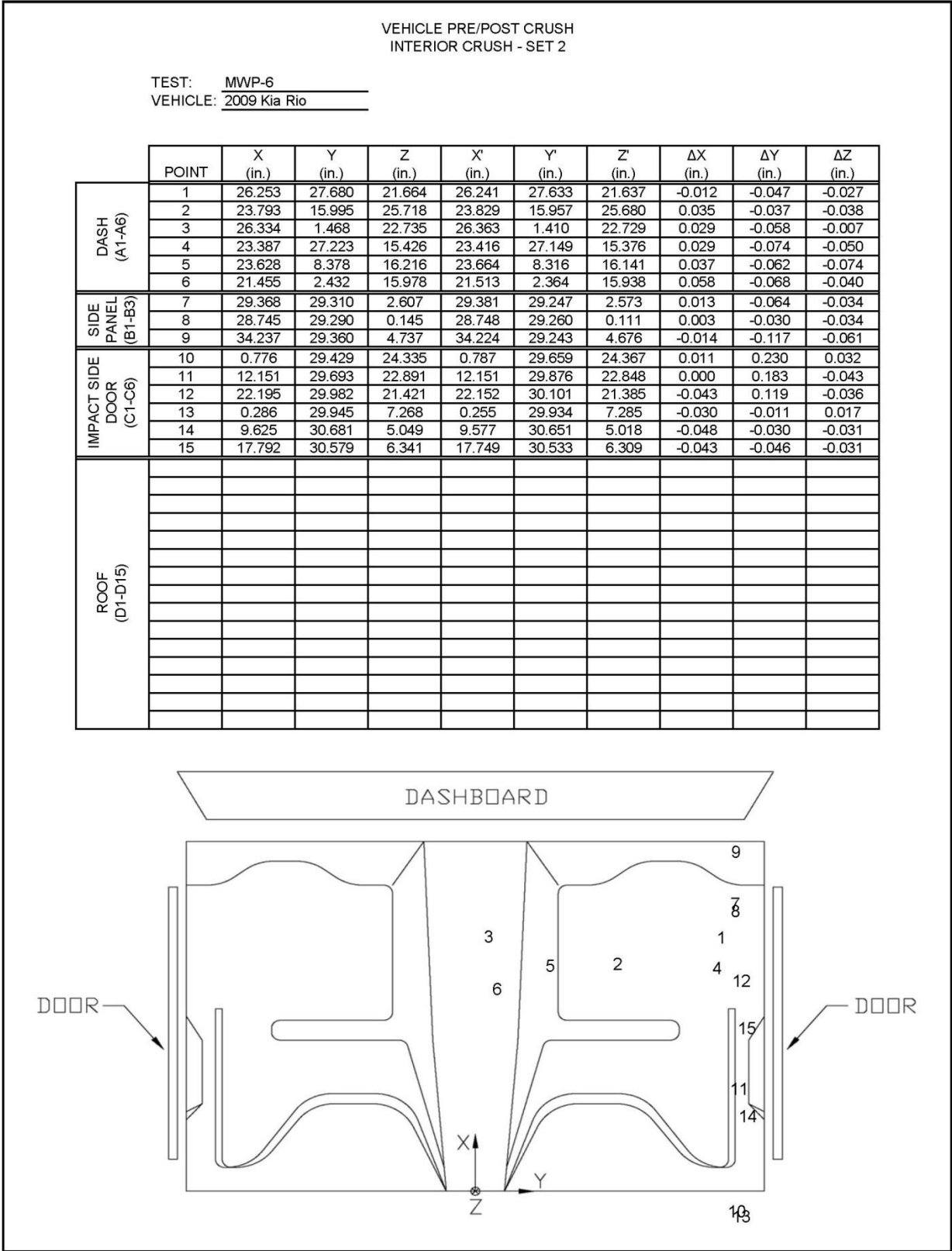


Figure D-10. Occupant Compartment Deformation Data – Set 2, Test No. MWP-6

MWP-6 Roof Crush

Comparative measurement of SFH-2 roof damage to undamaged vehicle:

MWP-6 at max point of crush	6.25"
Undamaged vehicle	5.25"
Total crush	<u>1"</u>



Figure D-11. Roof Deformation Documentation, Test No. MWP-6

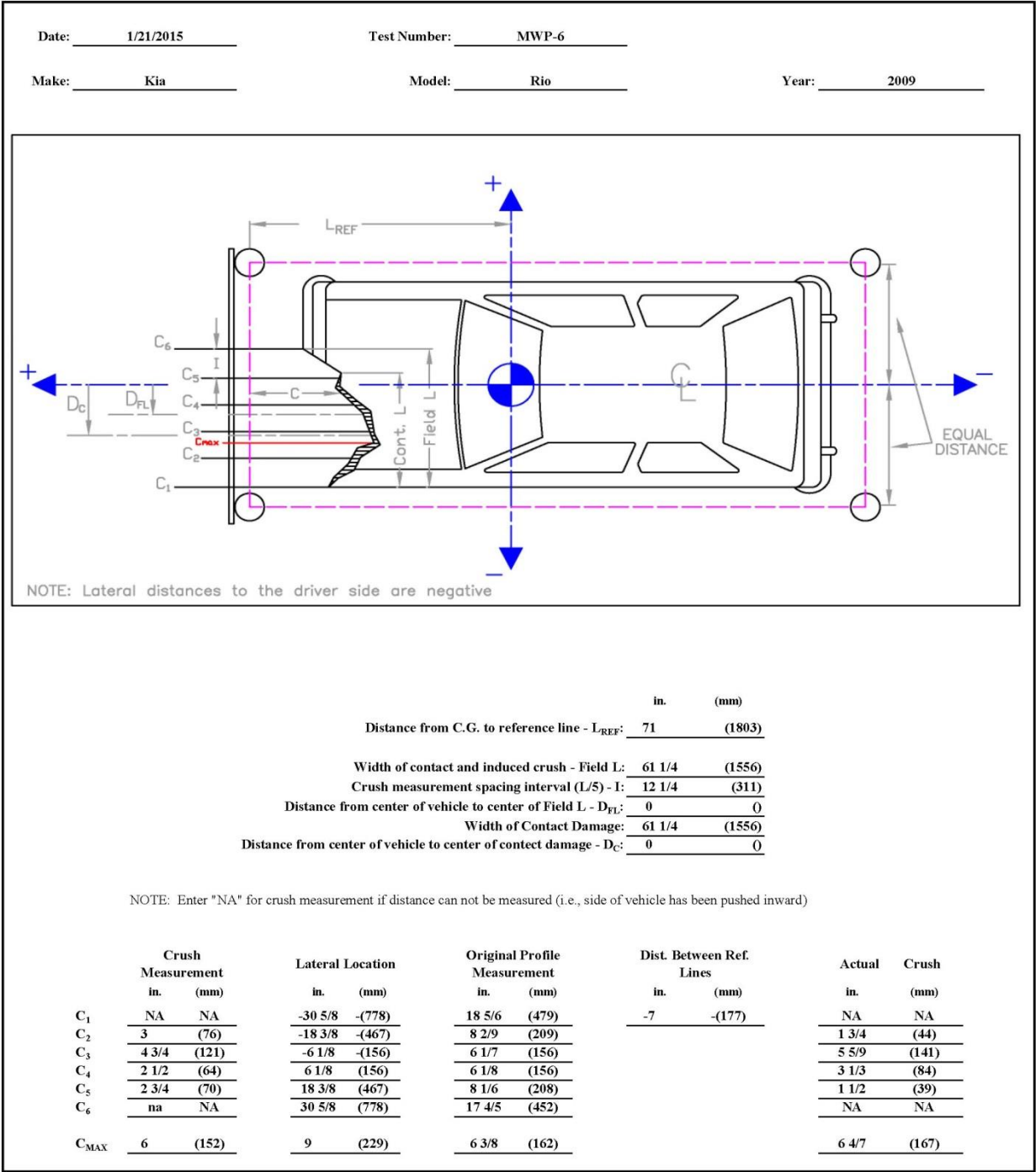


Figure D-12. Exterior Vehicle Crush (NASS) – Front, Test No. MWP-6

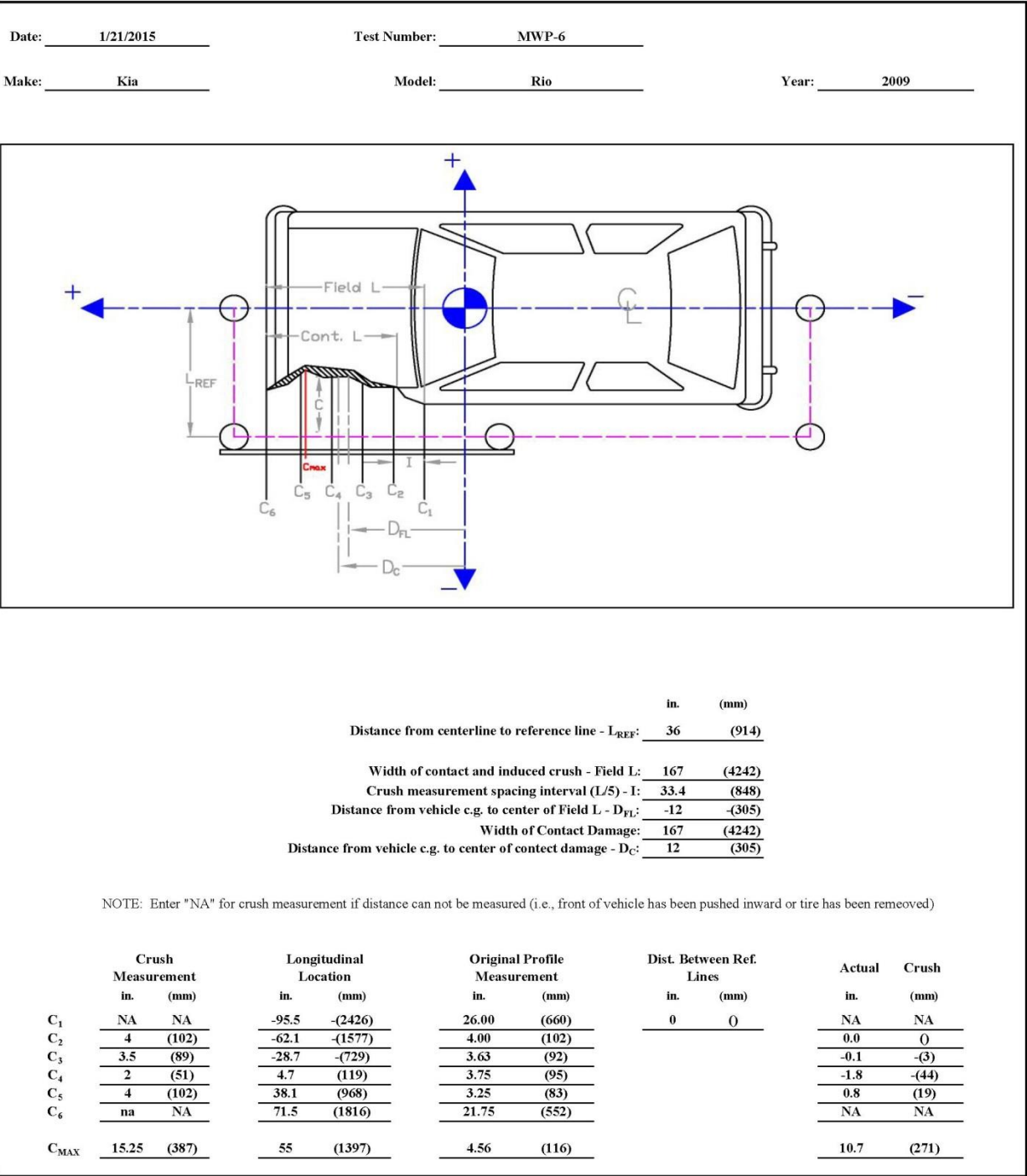


Figure D-13. Exterior Vehicle Crush (NASS) – Side, Test No. MWP-6

VEHICLE PRE/POST CRUSH
FLOORPAN - SET 1

TEST: MWP-7
VEHICLE: 1100C

POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔY (in.)	ΔZ (in.)
1	28.397	20.090	0.597	28.220	19.883	3.999	-0.178	-0.207	3.402
2	30.500	16.692	-0.552	30.450	16.589	2.858	-0.050	-0.102	3.410
3	32.970	13.502	-1.716	33.034	13.483	1.744	0.063	-0.020	3.460
4	30.723	4.341	-3.735	30.993	4.396	-0.932	0.270	0.055	2.803
5	27.775	17.645	-3.824	28.061	17.693	-0.587	0.286	0.047	3.237
6	29.364	13.722	-4.197	29.696	13.861	-1.003	0.332	0.139	3.194
7	28.655	9.983	-4.730	28.982	10.124	-1.830	0.327	0.141	2.900
8	28.128	3.545	-4.981	28.526	3.738	-2.447	0.398	0.193	2.534
9	24.217	17.537	-6.526	24.783	17.812	-3.605	0.566	0.275	2.921
10	24.123	13.278	-6.281	24.688	13.554	-3.576	0.566	0.276	2.706
11	24.014	9.616	-6.610	24.599	9.896	-4.091	0.585	0.280	2.519
12	23.954	3.773	-6.671	24.534	4.054	-4.478	0.580	0.281	2.193
13	19.099	18.936	-6.647	19.670	19.240	-4.107	0.571	0.304	2.540
14	19.037	14.049	-6.547	19.596	14.349	-4.289	0.559	0.300	2.258
15	18.977	8.651	-6.766	19.578	8.993	-4.660	0.601	0.342	2.105
16	19.182	4.633	-6.643	19.856	4.945	-4.602	0.674	0.312	2.041
17	15.563	21.748	-6.506	16.133	22.005	-4.134	0.570	0.256	2.372
18	15.450	16.312	-6.245	15.997	16.610	-4.194	0.547	0.298	2.051
19	14.793	11.237	-6.165	15.384	11.541	-4.440	0.591	0.304	1.725
20	15.136	4.499	-6.653	15.785	4.798	-4.012	0.649	0.298	2.641
21	9.652	19.901	-6.048	10.192	20.206	-4.321	0.539	0.306	1.727
22	9.611	16.211	-5.326	10.150	16.467	-3.815	0.539	0.257	1.512
23	9.353	10.456	-5.302	9.852	10.715	-4.077	0.498	0.259	1.225
24	9.150	5.848	-5.994	9.694	6.148	-3.866	0.544	0.300	2.128
25	2.231	20.401	-0.887	2.355	20.467	0.168	0.124	0.066	1.055
26	1.818	15.840	-0.610	1.922	15.895	0.161	0.104	0.055	0.771
27	1.734	7.978	-0.596	1.827	8.029	-0.252	0.093	0.050	0.344
28	2.124	4.216	-0.973	2.248	4.261	-0.783	0.124	0.045	0.190

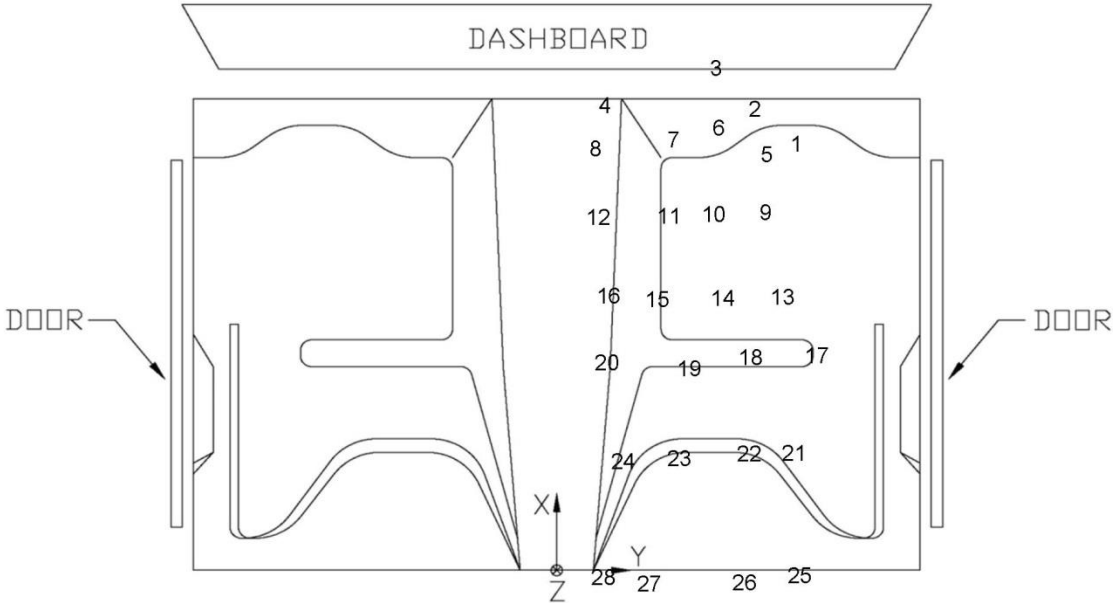


Figure D-14. Floor Pan Deformation Data – Set 1, Test No. MWP-7

VEHICLE PRE/POST CRUSH
FLOORPAN - SET 2

TEST: MWP-7
VEHICLE: 1100C

POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔY (in.)	ΔZ (in.)
1	38.788	24.949	2.006	38.483	24.867	2.041	-0.304	-0.081	0.035
2	40.955	21.543	0.960	40.709	21.495	0.996	-0.246	-0.047	0.037
3	43.523	18.387	-0.042	43.262	18.395	0.025	-0.261	0.007	0.068
4	41.467	9.147	-2.119	41.216	9.196	-2.092	-0.251	0.049	0.027
5	38.502	22.410	-2.490	38.229	22.416	-2.430	-0.273	0.006	0.059
6	40.120	18.542	-2.699	39.885	18.557	-2.659	-0.235	0.016	0.041
7	39.426	14.819	-3.287	39.158	14.833	-3.266	-0.267	0.015	0.021
8	38.982	8.345	-3.528	38.736	8.299	-3.507	-0.246	-0.046	0.022
9	35.143	22.354	-5.384	34.924	22.352	-5.370	-0.220	-0.002	0.014
10	35.059	18.109	-5.126	34.787	18.084	-5.127	-0.272	-0.025	-0.001
11	34.960	14.420	-5.463	34.712	14.423	-5.429	-0.248	0.003	0.034
12	34.891	8.606	-5.529	34.701	8.597	-5.466	-0.190	-0.009	0.063
13	30.006	23.762	-5.869	29.749	23.769	-5.864	-0.257	0.007	0.005
14	29.947	18.834	-5.764	29.709	18.850	-5.768	-0.238	0.016	-0.003
15	29.945	13.481	-5.971	29.659	13.487	-5.832	-0.286	0.006	0.139
16	30.131	9.434	-5.825	29.970	9.412	-5.545	-0.161	-0.021	0.280
17	26.462	26.525	-5.980	26.214	26.493	-5.972	-0.249	-0.032	0.008
18	26.331	21.069	-5.717	26.089	21.070	-5.728	-0.242	0.001	-0.010
19	25.710	16.044	-5.670	25.494	16.029	-5.675	-0.216	-0.015	-0.005
20	26.094	9.265	-6.111	25.906	9.328	-4.873	-0.188	0.062	1.238
21	20.486	24.657	-5.919	20.279	24.650	-5.934	-0.207	-0.007	-0.015
22	20.516	20.997	-5.204	20.261	20.964	-5.219	-0.256	-0.033	-0.015
23	20.256	15.209	-5.181	20.013	15.233	-5.157	-0.242	0.024	0.024
24	20.073	10.599	-5.872	19.825	10.588	-4.664	-0.248	-0.011	1.209
25	12.796	25.148	-1.299	12.535	25.153	-1.310	-0.262	0.005	-0.011
26	12.389	20.567	-1.033	12.106	20.579	-1.045	-0.284	0.012	-0.012
27	12.289	12.745	-0.999	12.071	12.725	-1.019	-0.218	-0.020	-0.020
28	12.703	8.920	-1.326	12.484	8.925	-1.351	-0.219	0.006	-0.024

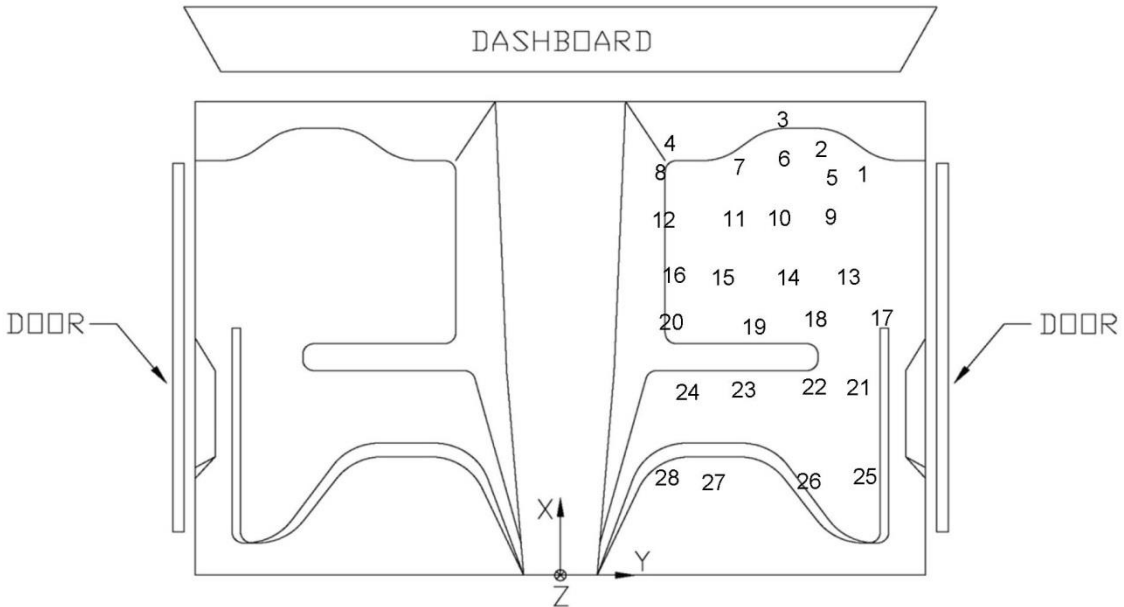


Figure D-15. Floor Pan Deformation Data – Set 2, Test No. MWP-7

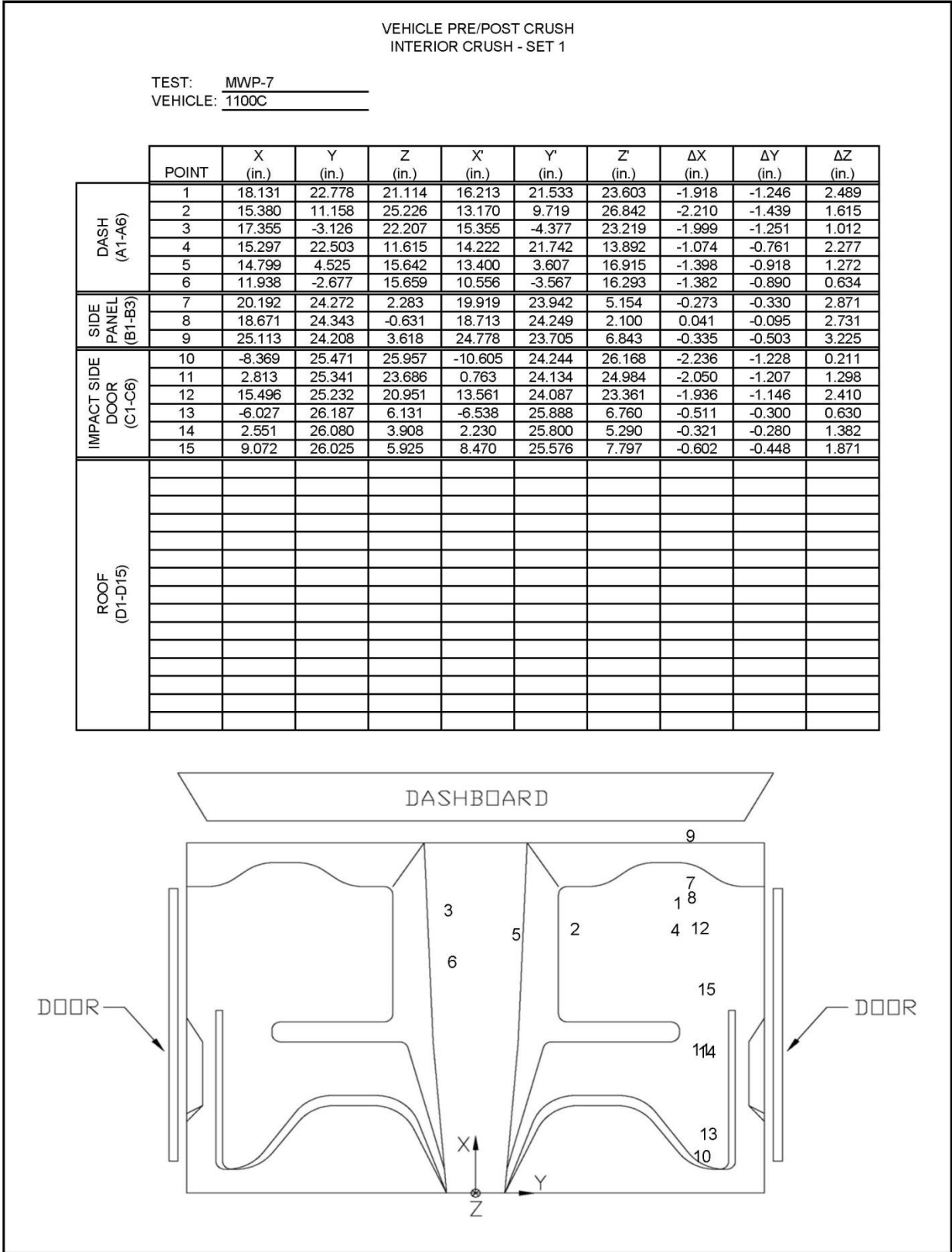


Figure D-16. Occupant Compartment Deformation Data – Set 1, Test No. MWP-7

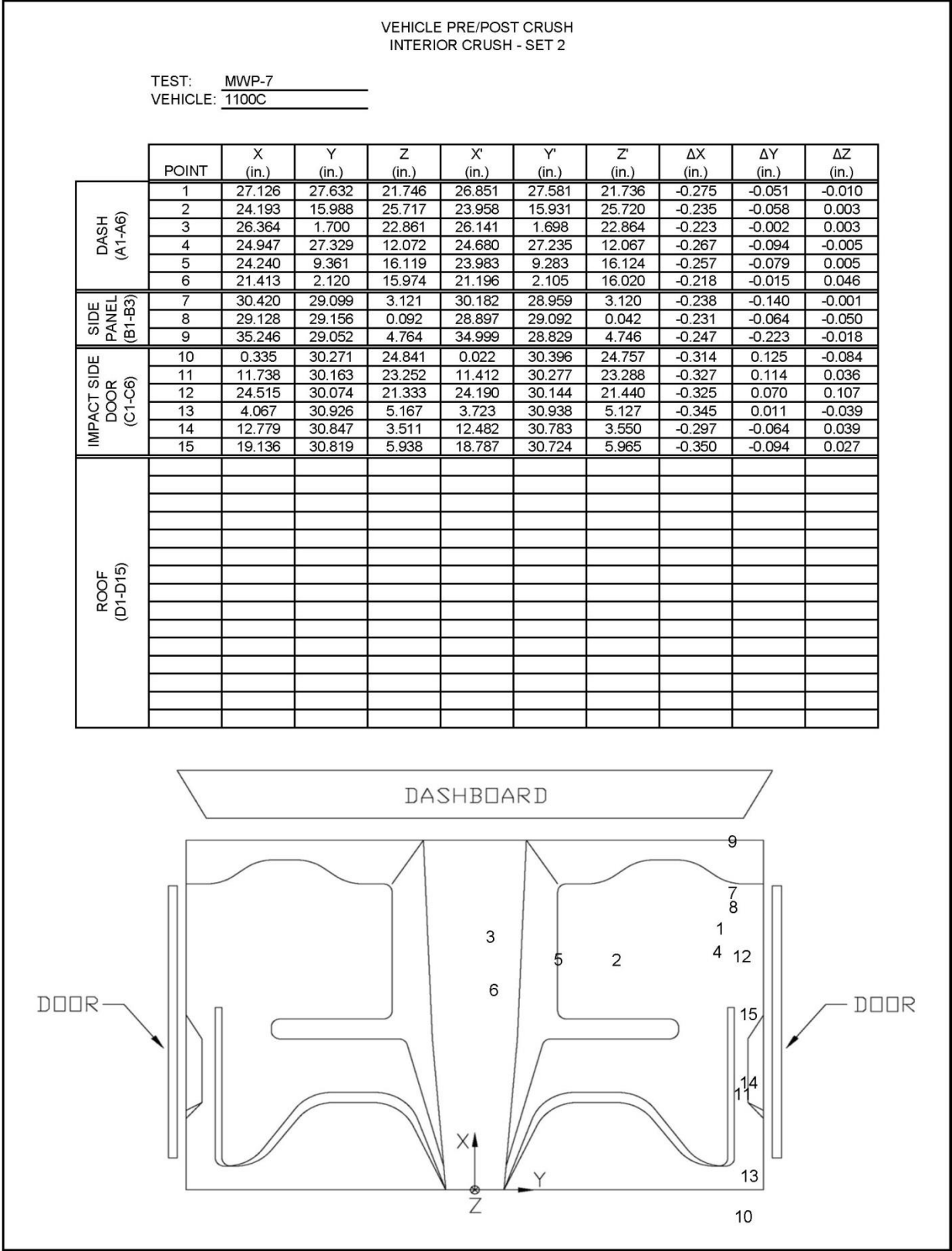


Figure D-17. Occupant Compartment Deformation Data – Set 2, Test No. MWP-7

MWP-7 Roof Crush

Comparative measurement of SFH-2 roof damage to undamaged vehicle:

MWP-7 at max point of crush	6.00"
Undamaged vehicle	<u>5.5"</u>
Total crush	.5"



Figure D-18. Roof Deformation Documentation, Test No. MWP-7

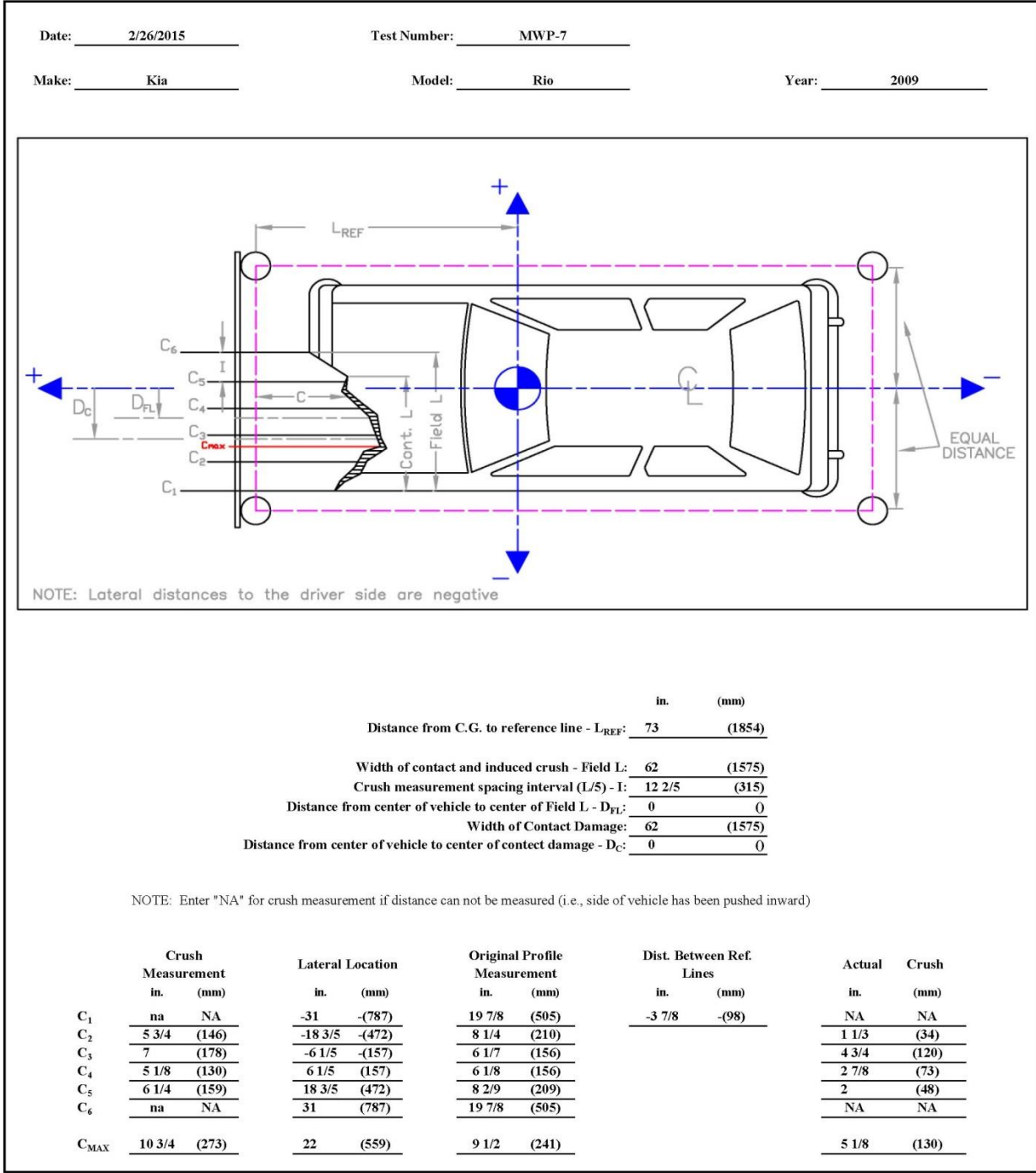


Figure D-19. Exterior Vehicle Crush (NASS) – Front, Test No. MWP-7

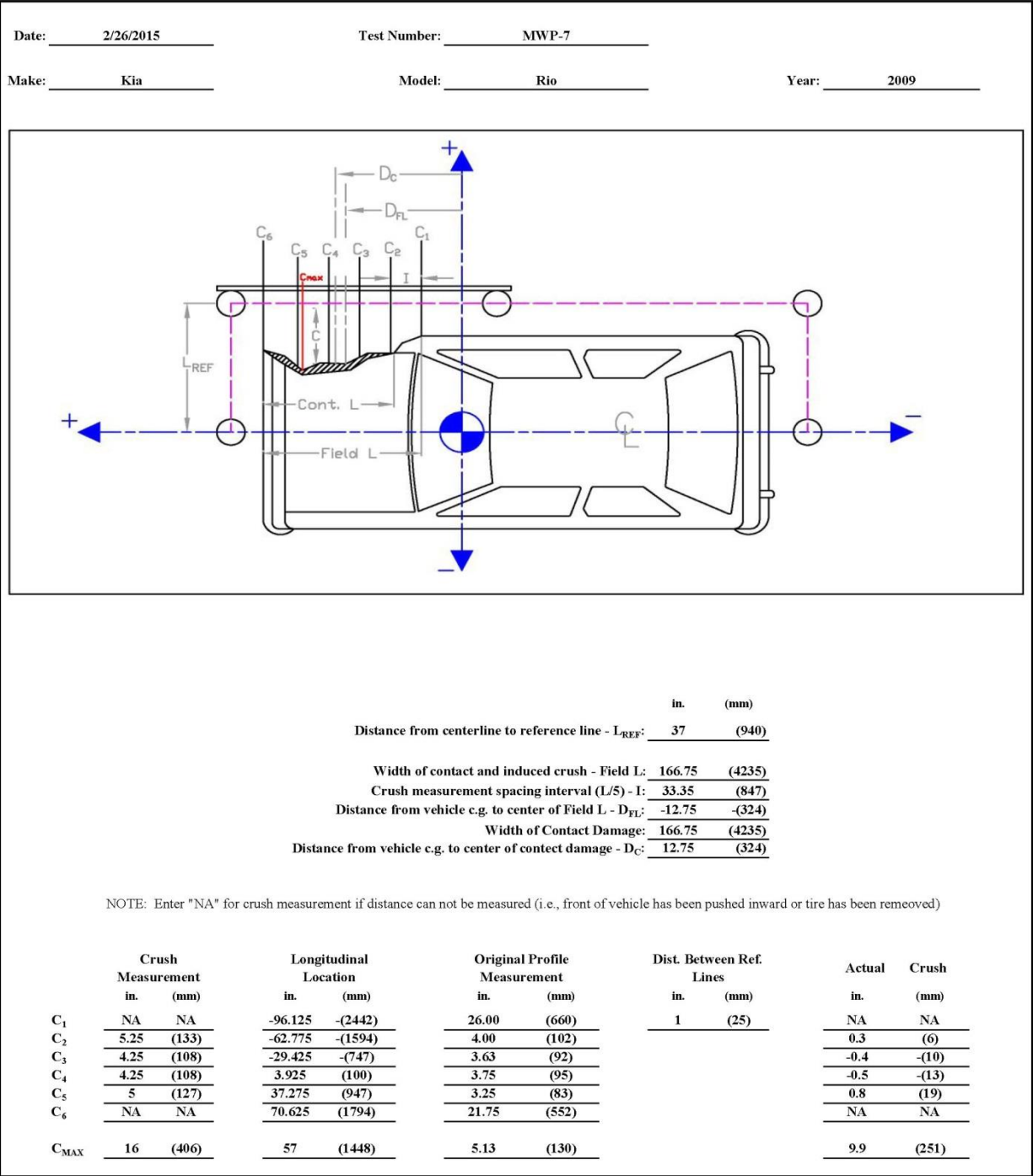


Figure D-20. Exterior Vehicle Crush (NASS) – Side, Test No. MWP-7

Appendix E. Accelerometer and Rate Transducer Data Plots, Test No. MWP-4

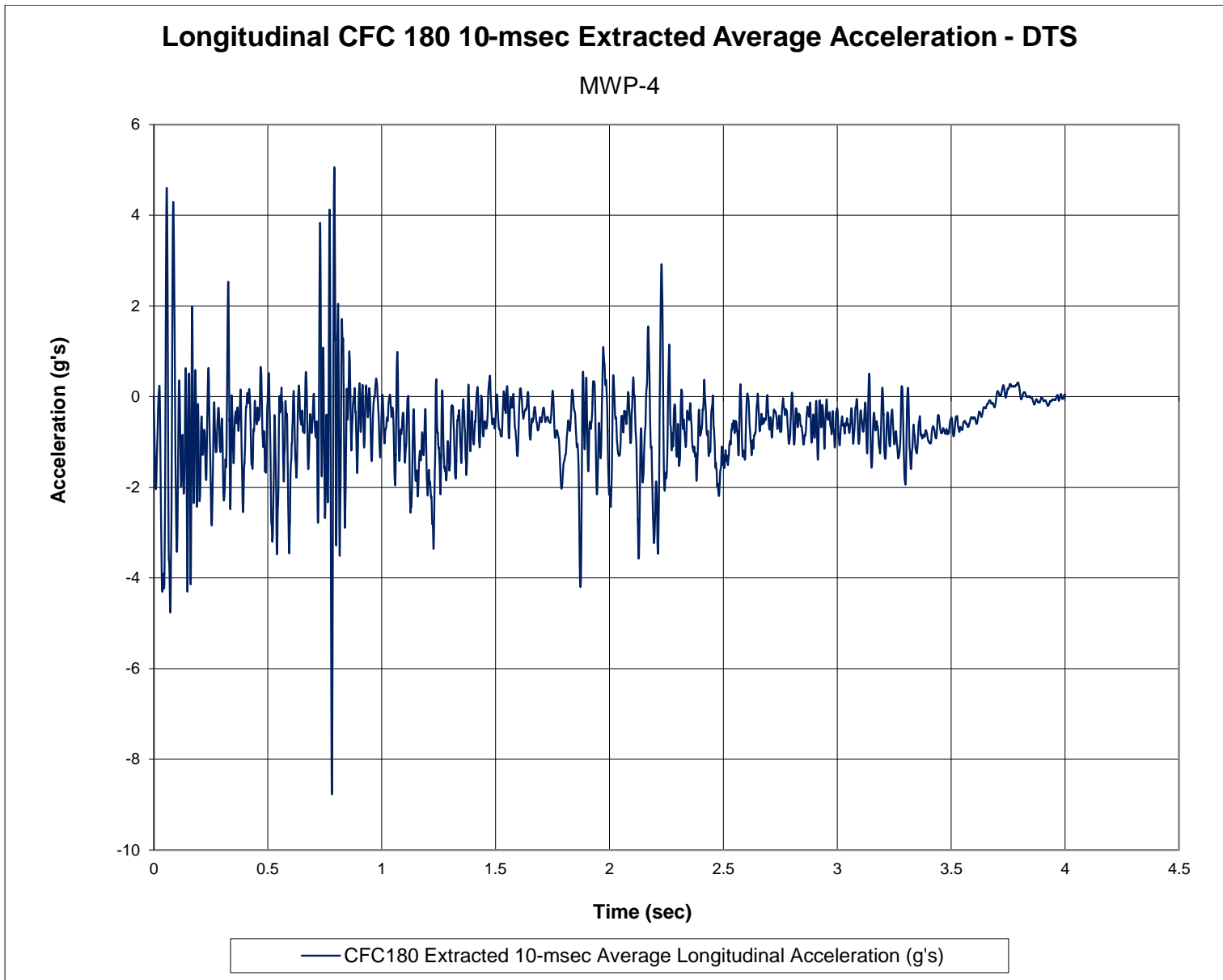


Figure E-1. 10-ms Average Longitudinal Deceleration (SLICE 1), Test No. MWP-4

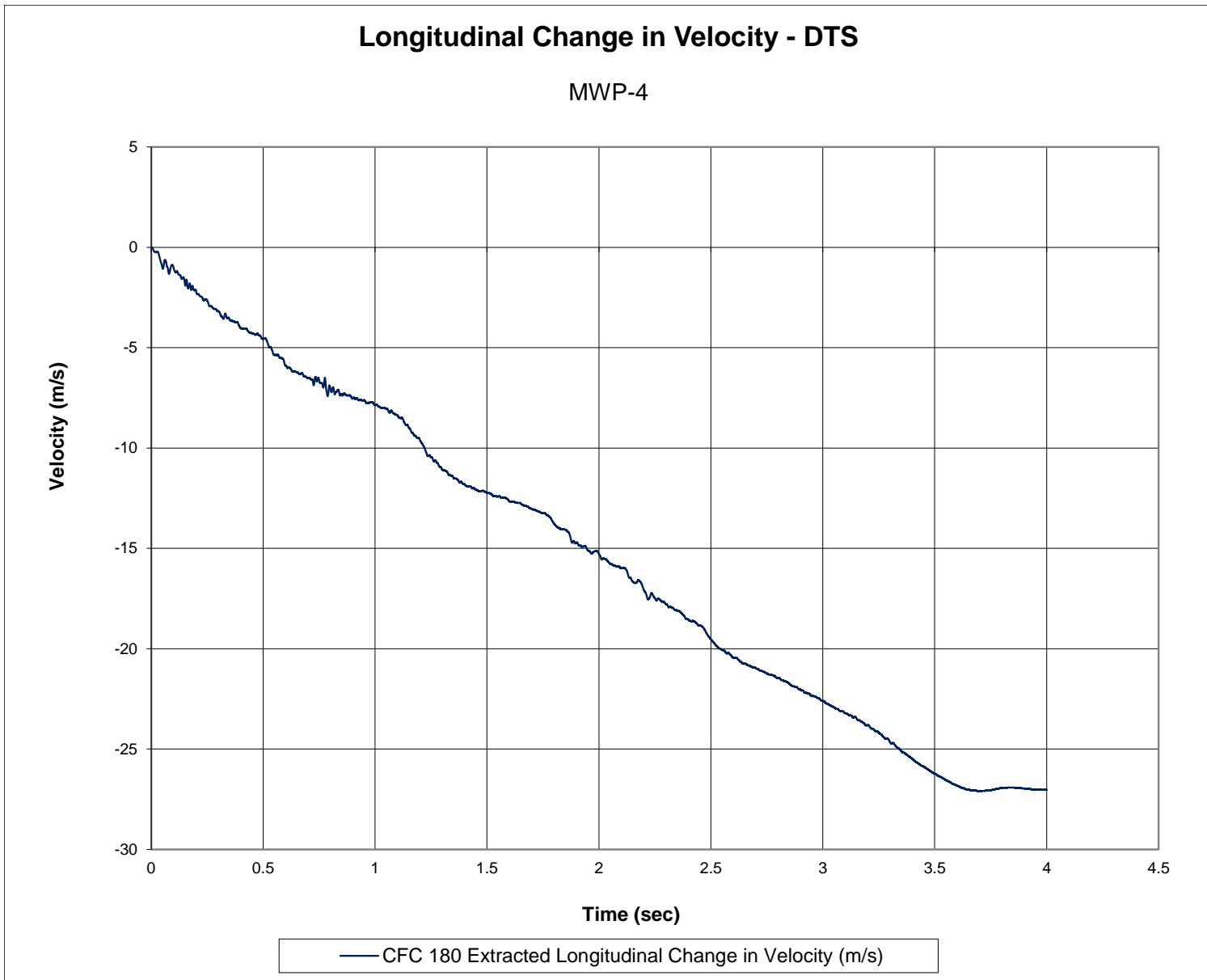


Figure E-2. Longitudinal Occupant Impact Velocity (SLICE 1), Test No. MWP-4

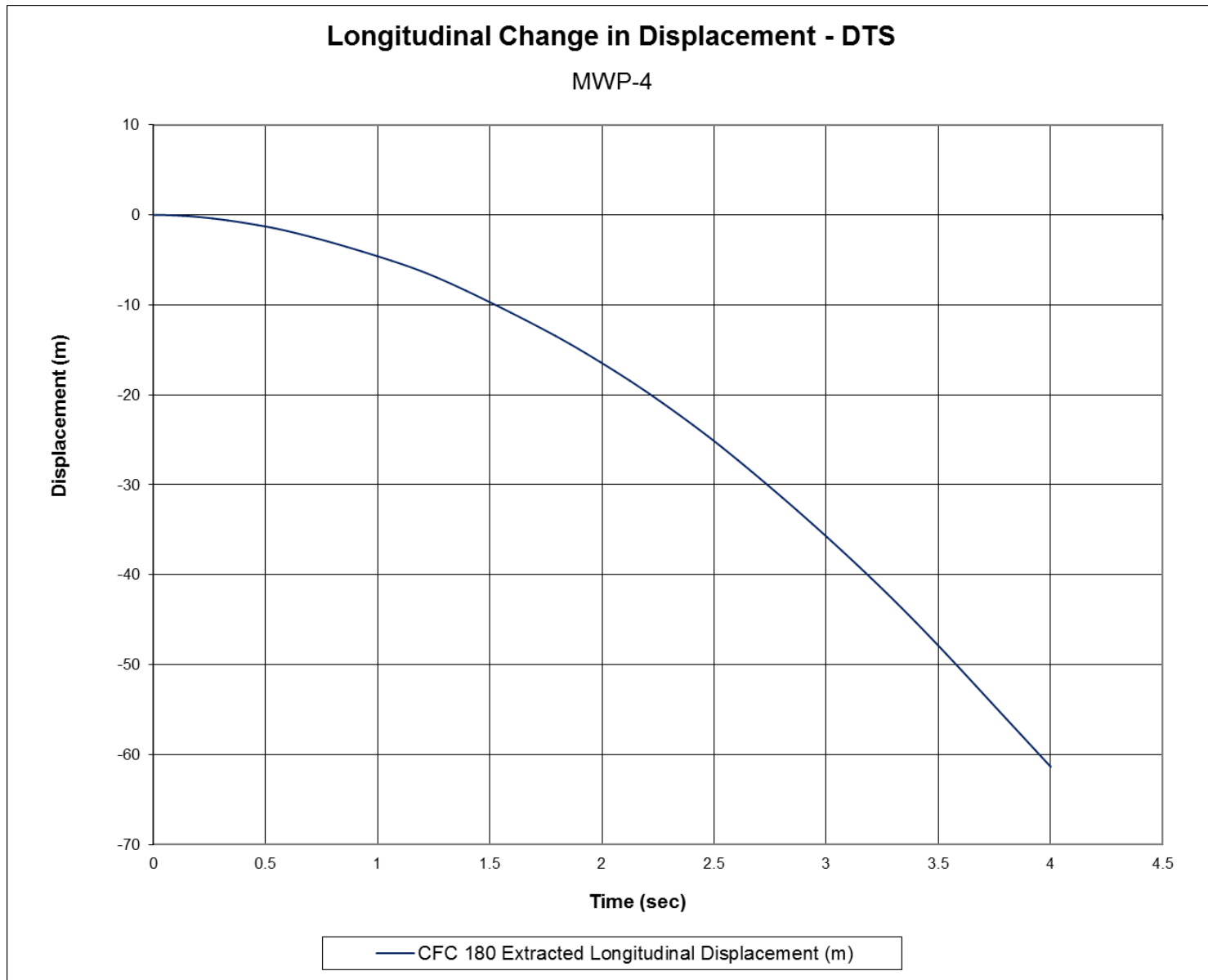


Figure E-3. Longitudinal Occupant Displacement (SLICE 1), Test No. MWP-4

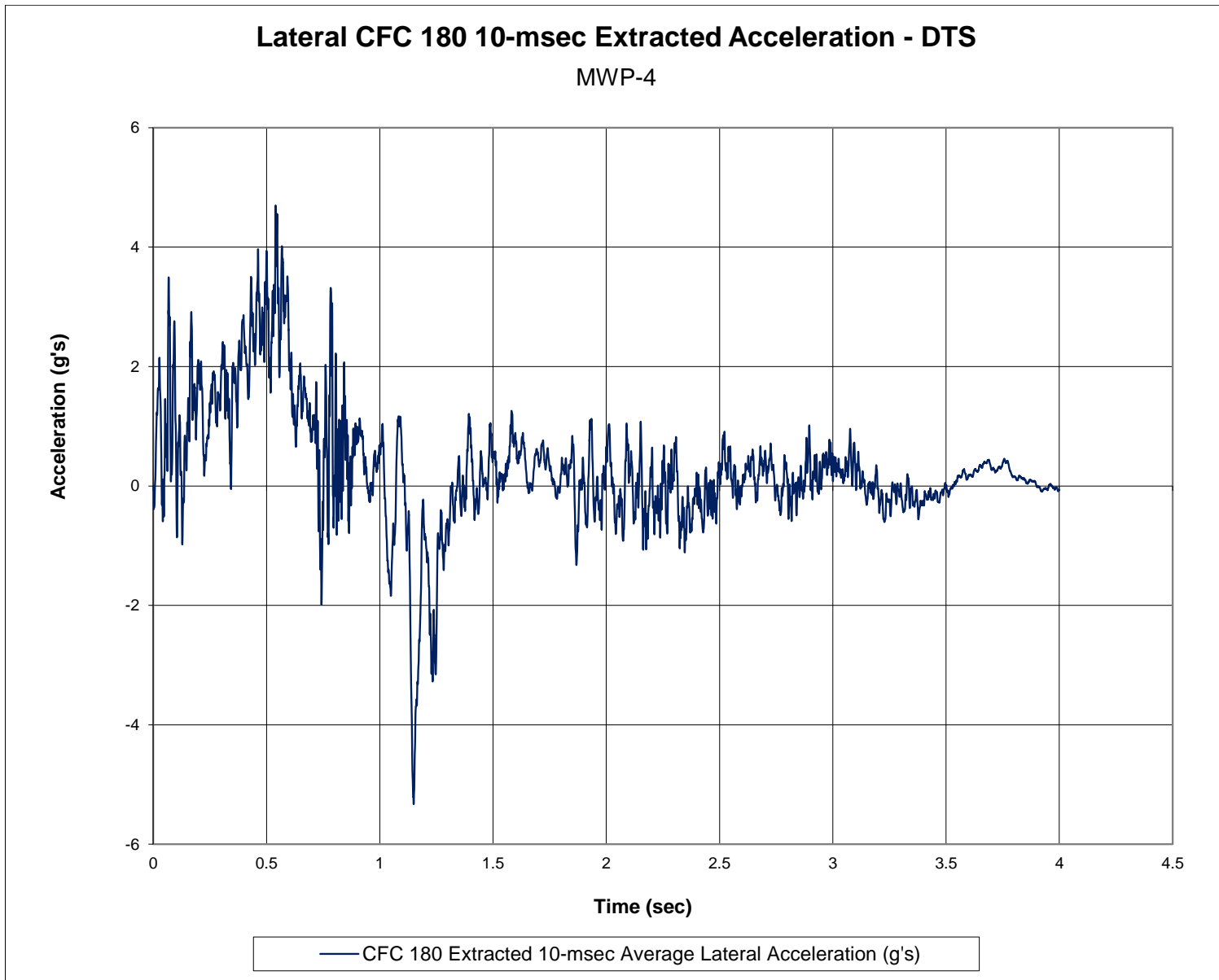


Figure E-4. 10-ms Average Lateral Deceleration (SLICE 1), Test No. MWP-4

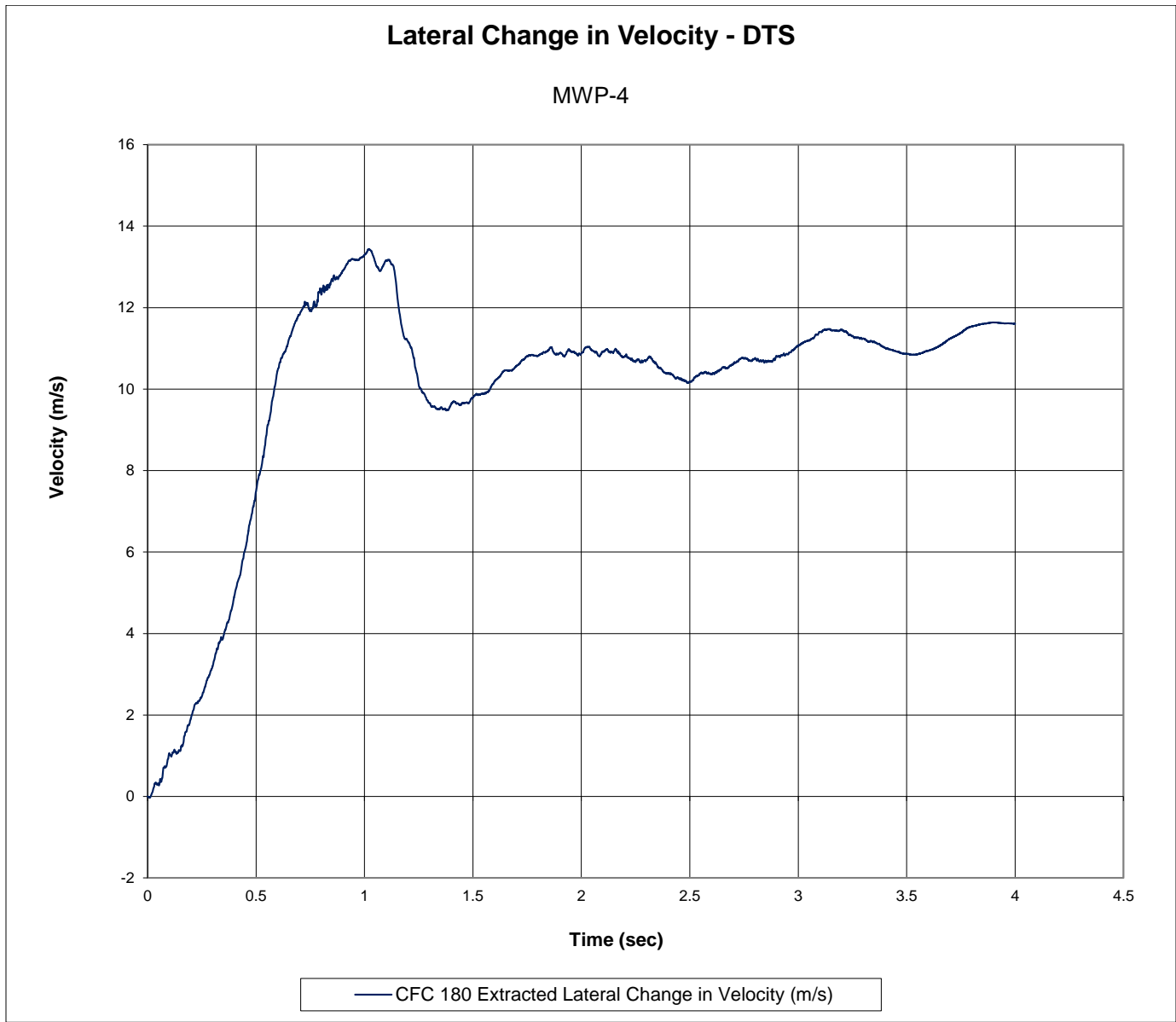


Figure E-5. Lateral Occupant Impact Velocity (SLICE 1), Test No. MWP-4

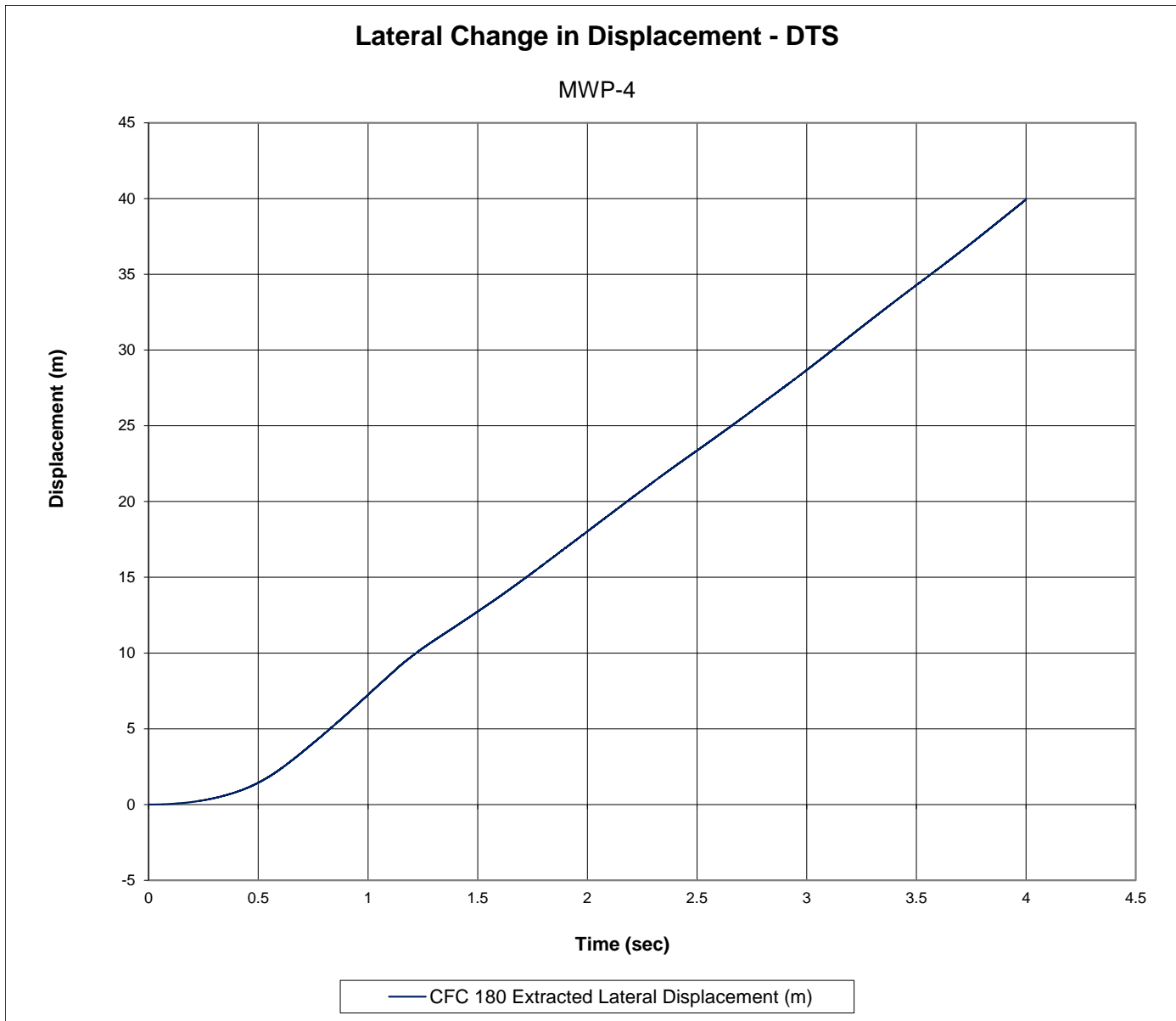


Figure E-6. Lateral Occupant Displacement (SLICE 1), Test No. MWP-4

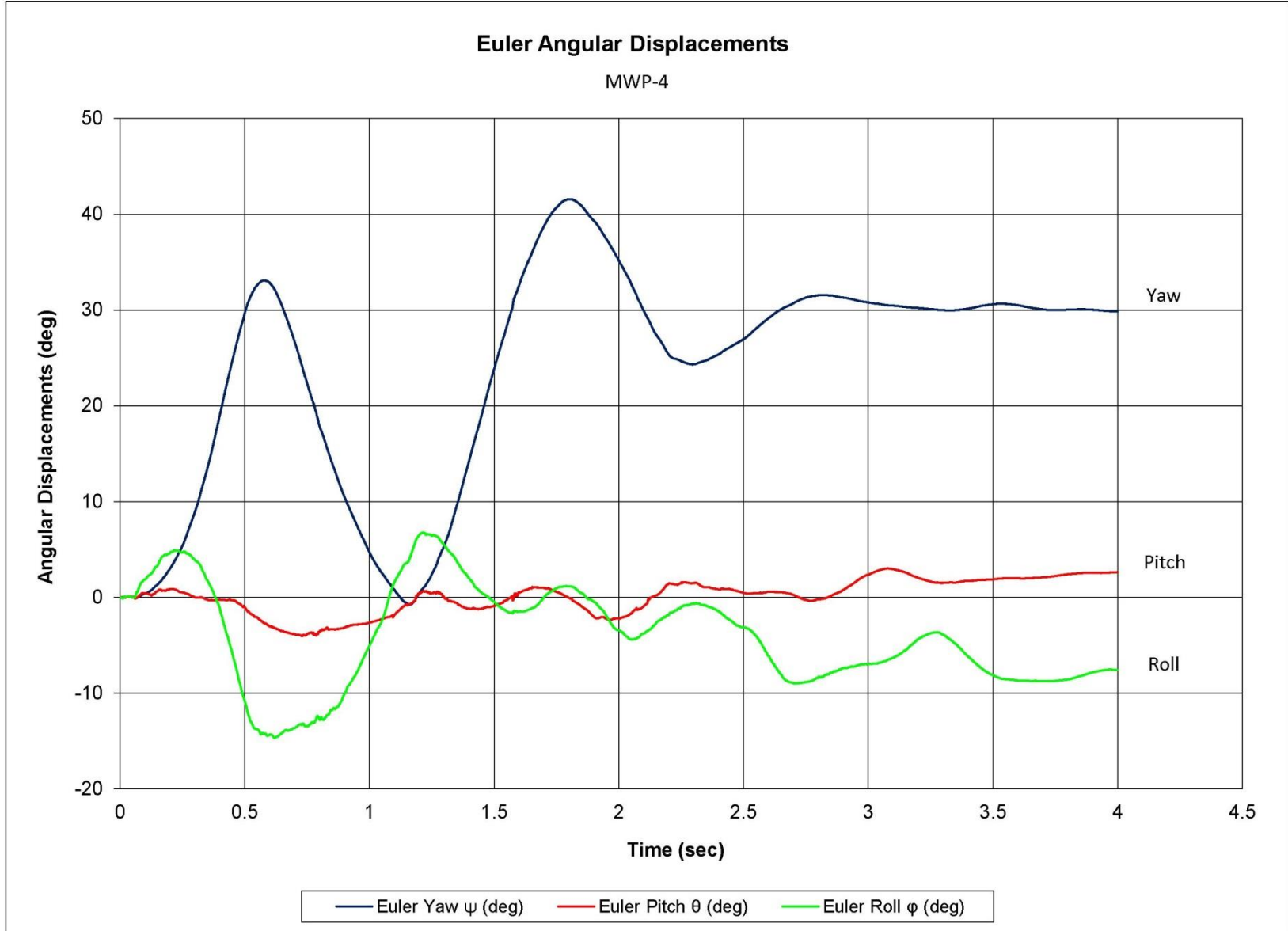


Figure E-7. Vehicle Angular Displacements (SLICE 1), Test No. MWP-4

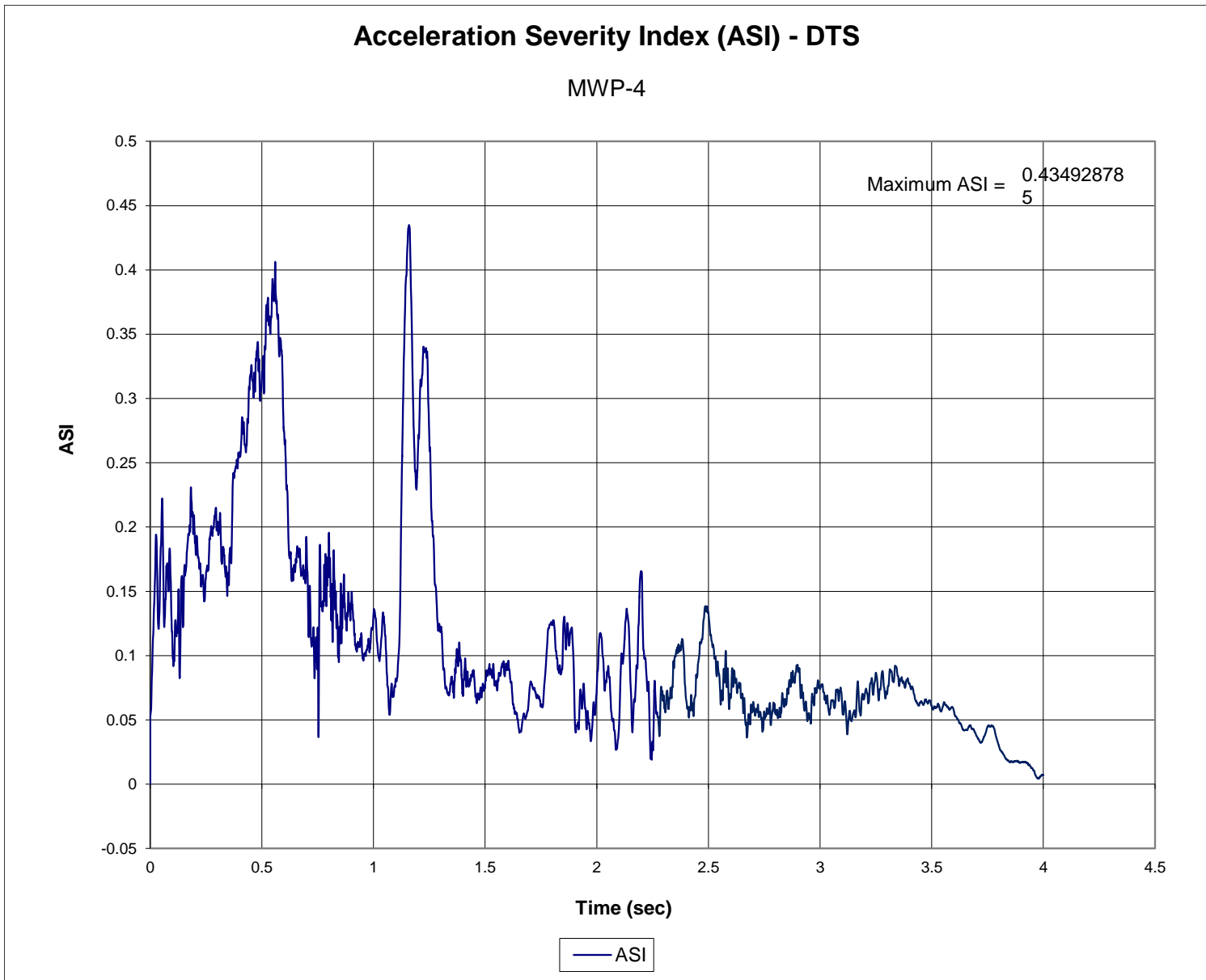


Figure E-8. Acceleration Severity Index (SLICE 1), Test No. MWP-4

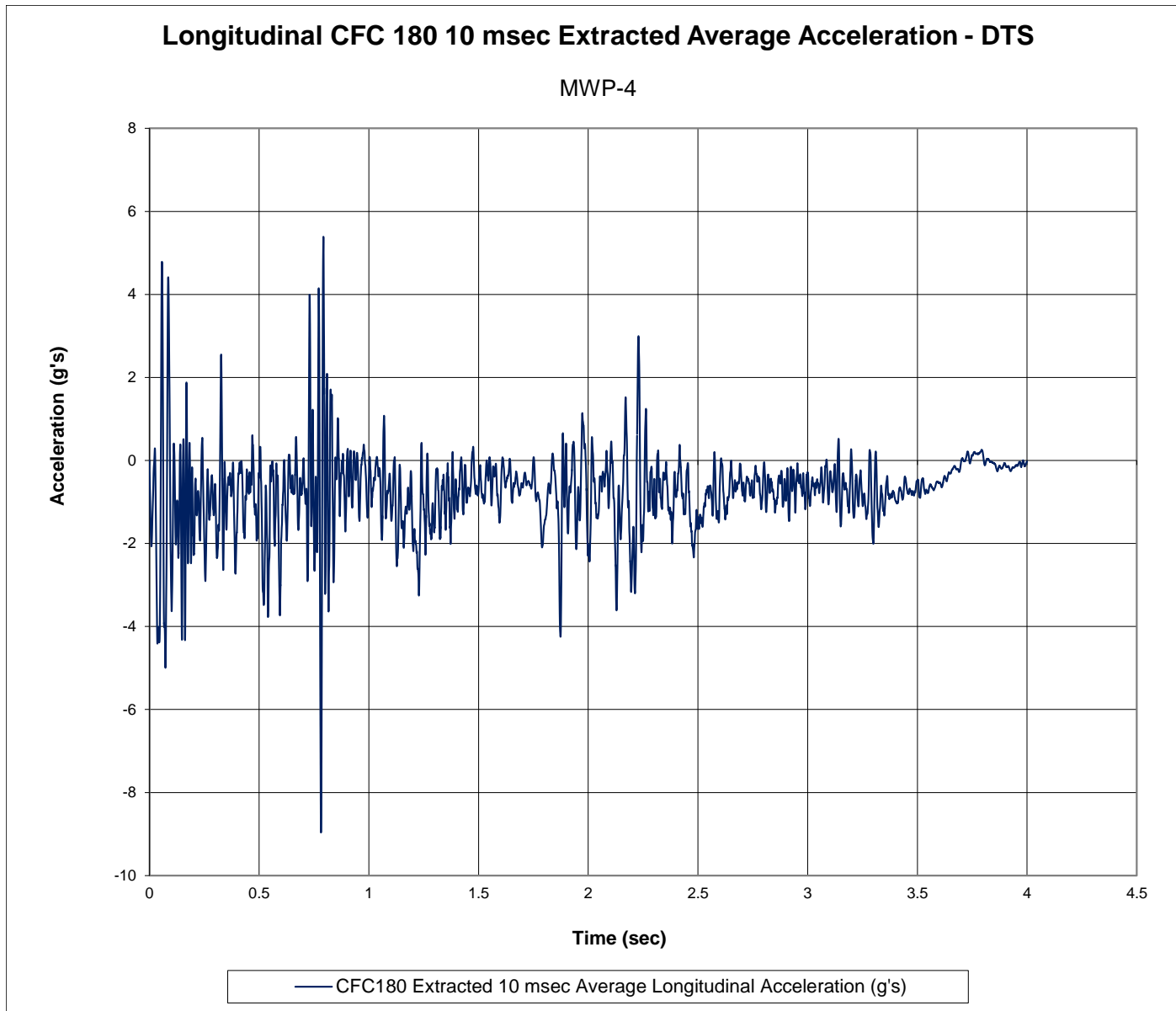


Figure E-9. 10-ms Average Longitudinal Deceleration (SLICE 2), Test No. MWP-4

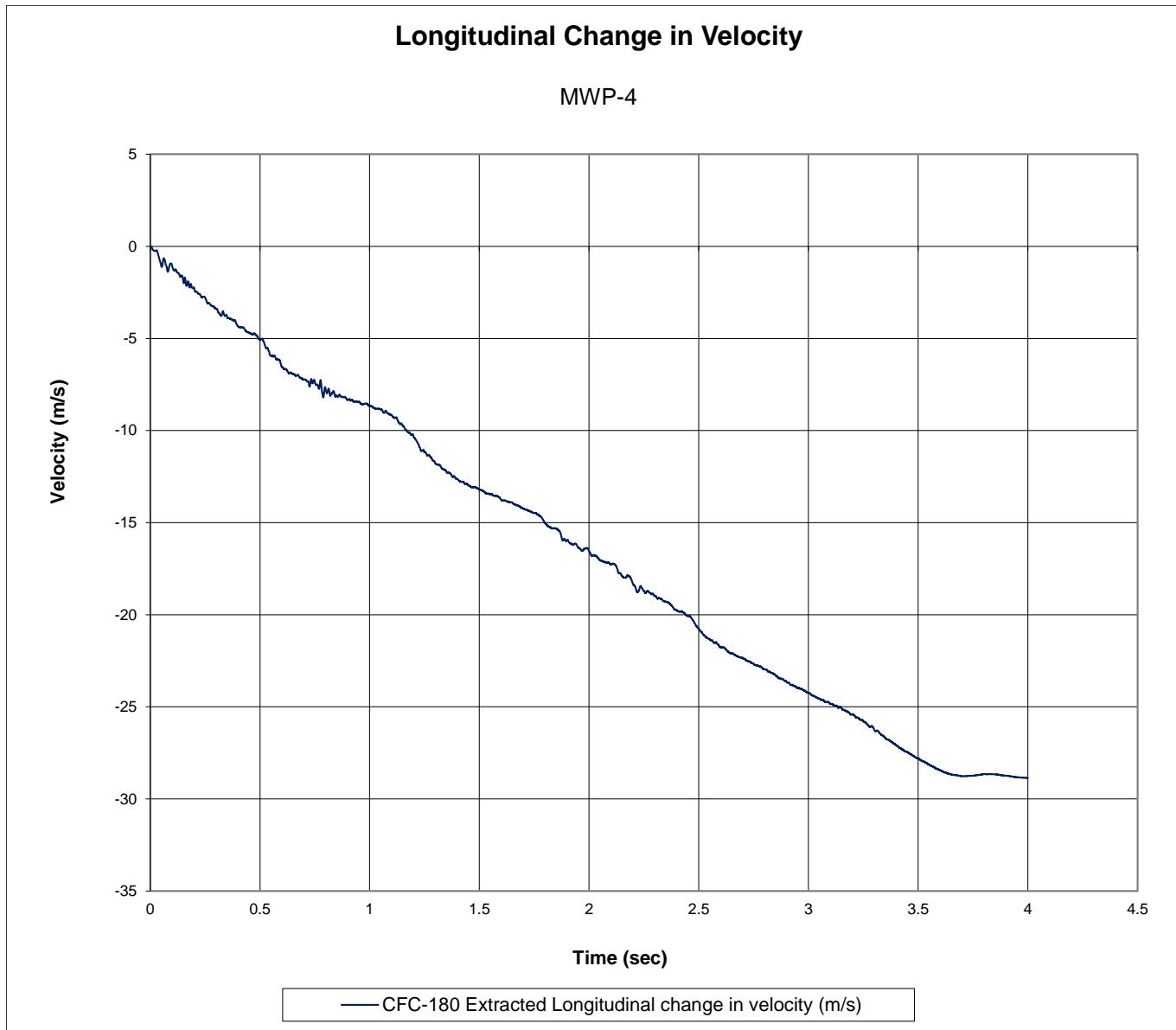


Figure E-10. Longitudinal Occupant Impact Velocity (SLICE 2), Test No. MWP-4

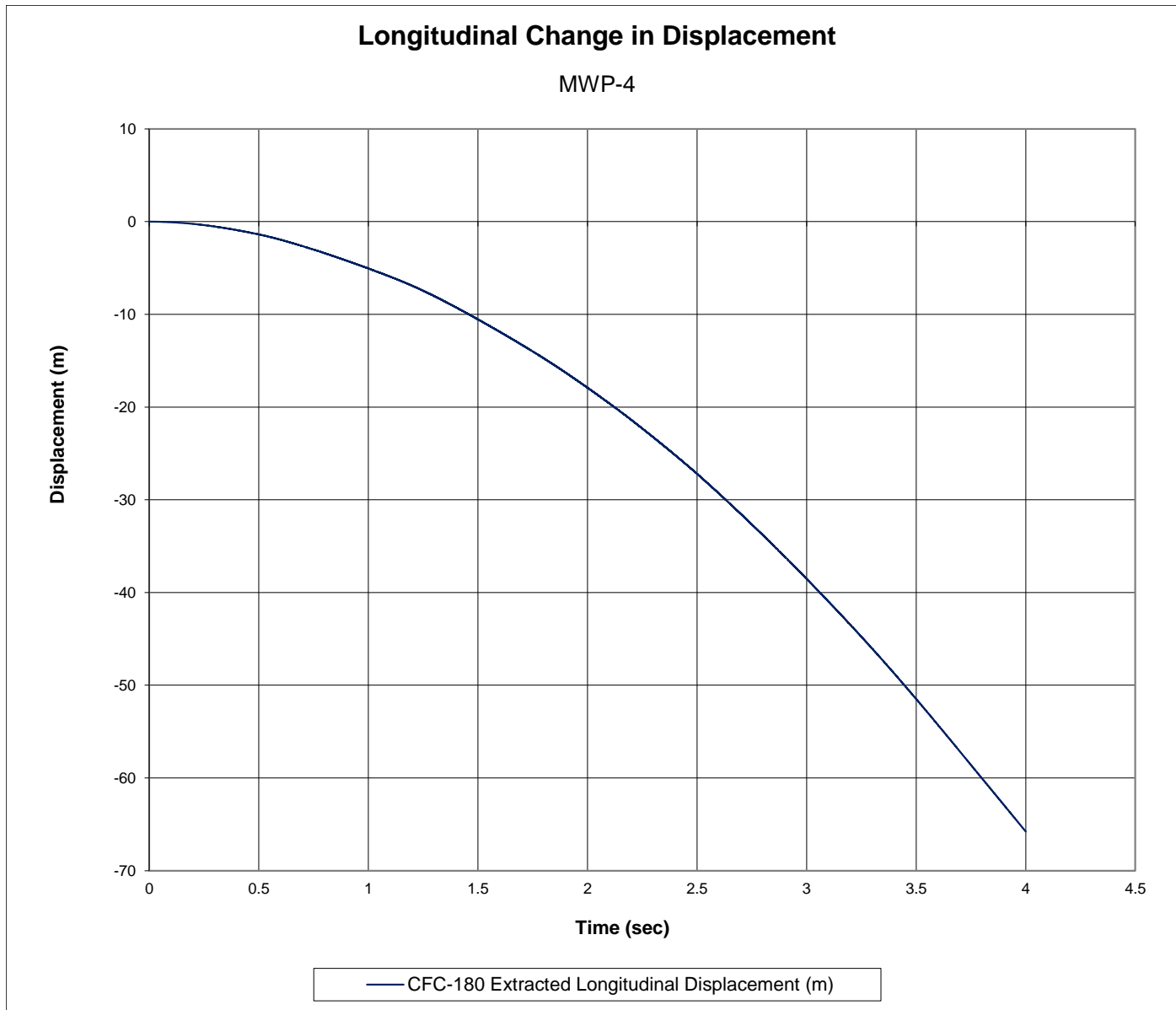


Figure E-11. Longitudinal Occupant Displacement (SLICE 2), Test No. MWP-4

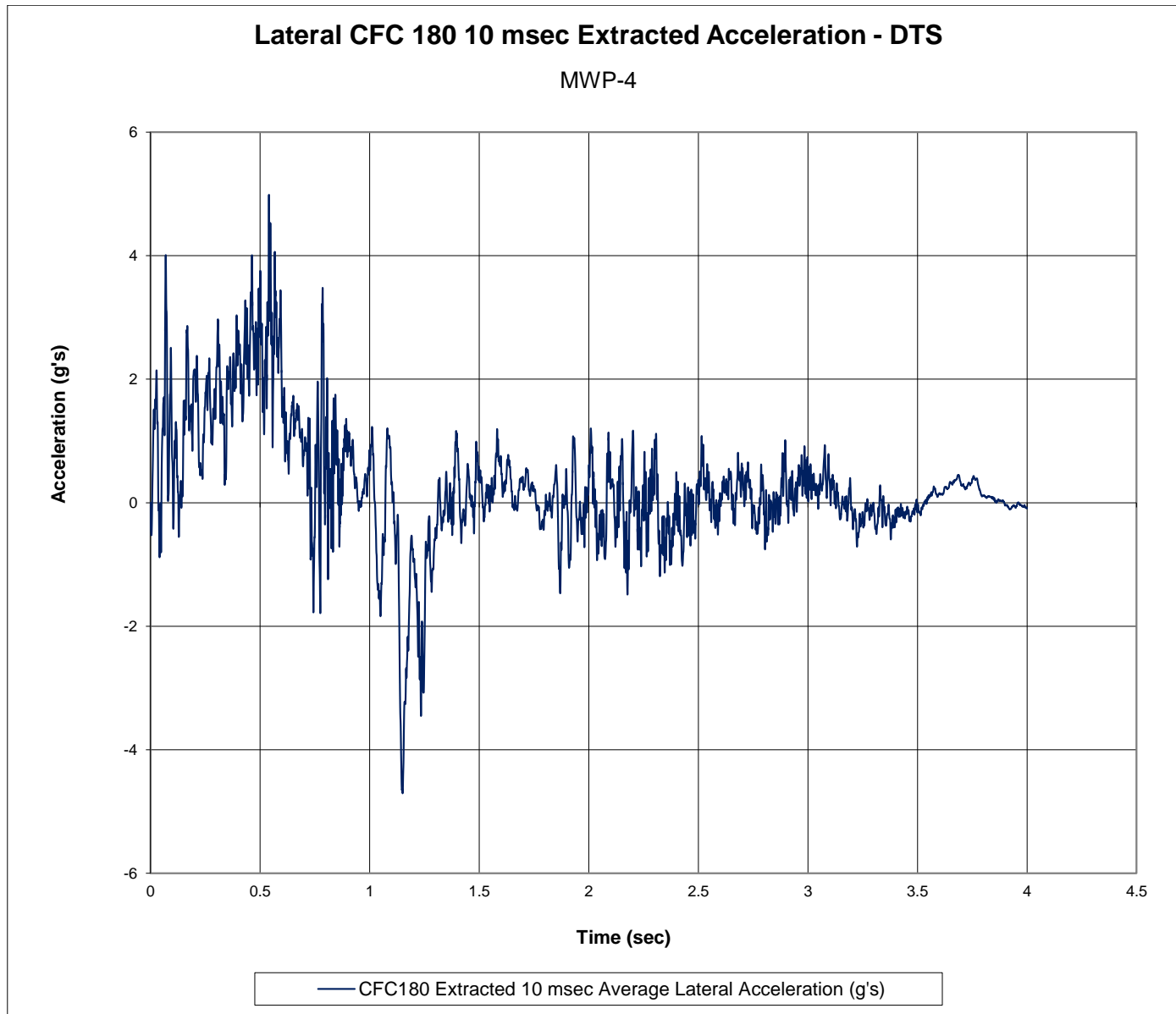


Figure E-12. 10-ms Average Lateral Deceleration (SLICE 2), Test No. MWP-4

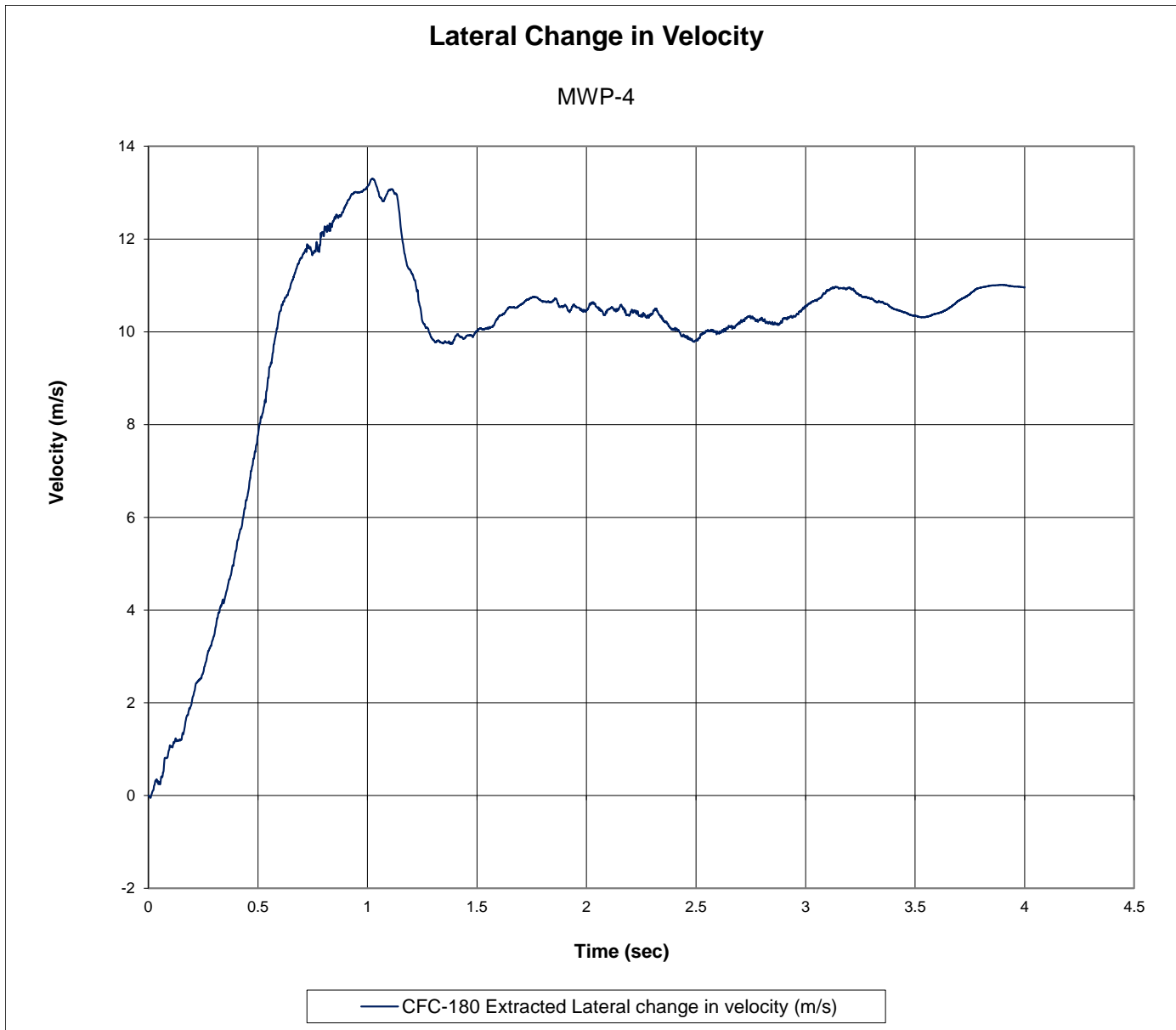


Figure E-13. Lateral Occupant Impact Velocity (SLICE 2), Test No. MWP-4



Figure E-14. Lateral Occupant Displacement (SLICE 2), Test No. MWP-4

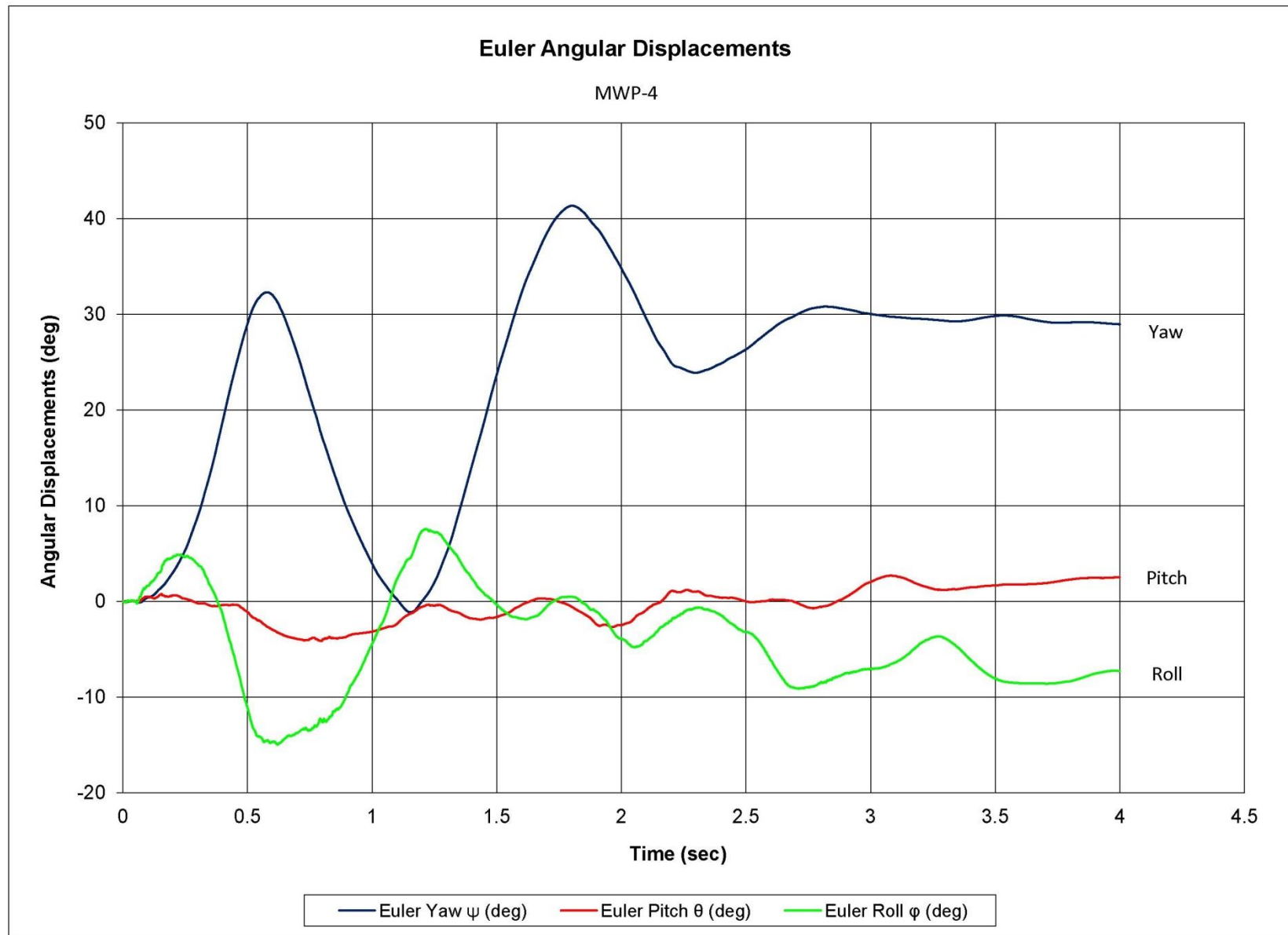


Figure E-15. Vehicle Angular Displacements (SLICE 2), Test No. MWP-4

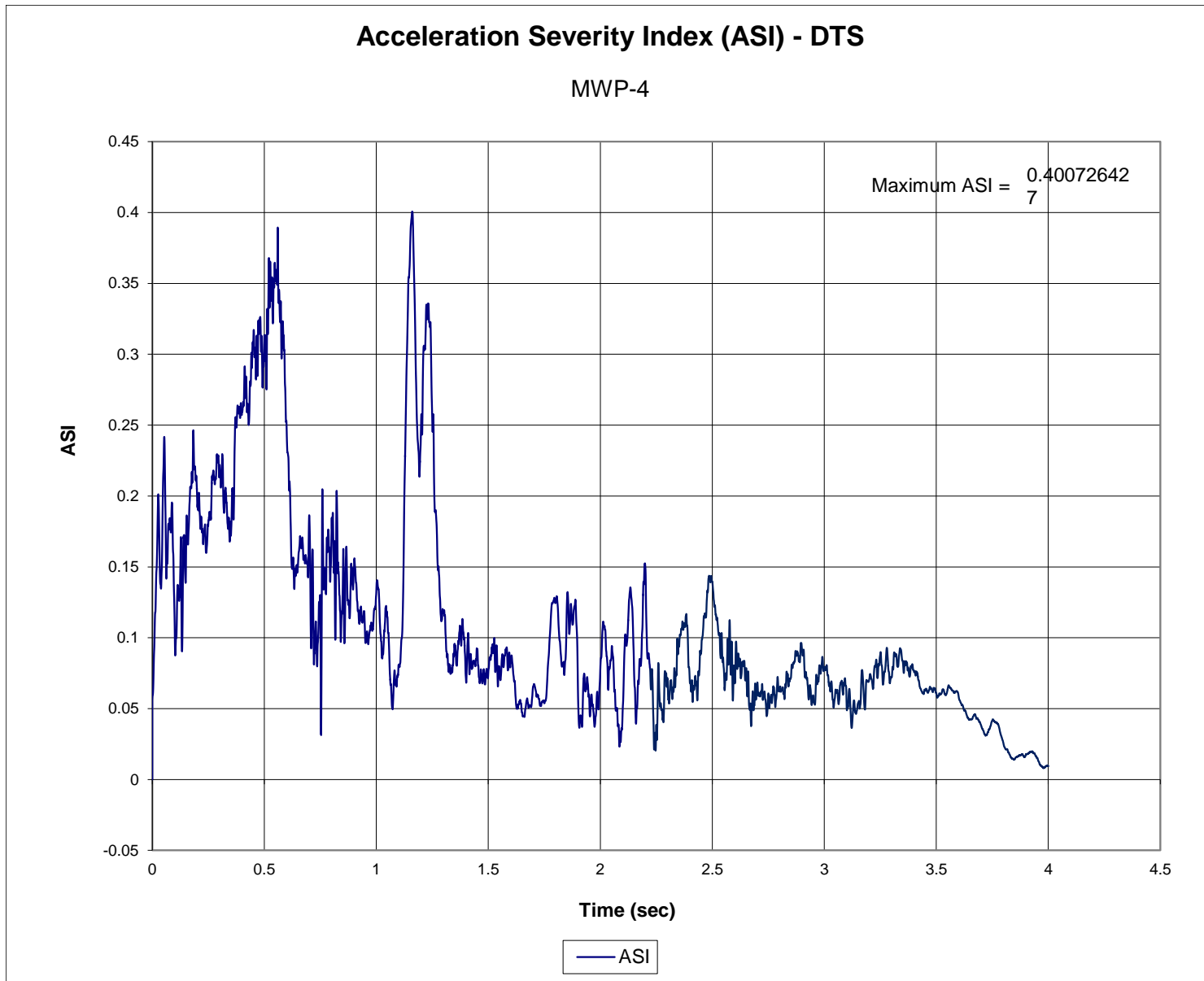


Figure E-16. Acceleration Severity Index (SLICE 2), Test No. MWP-4

Appendix F. Load Cell and String Potentiometer Data, Test No. MWP-4

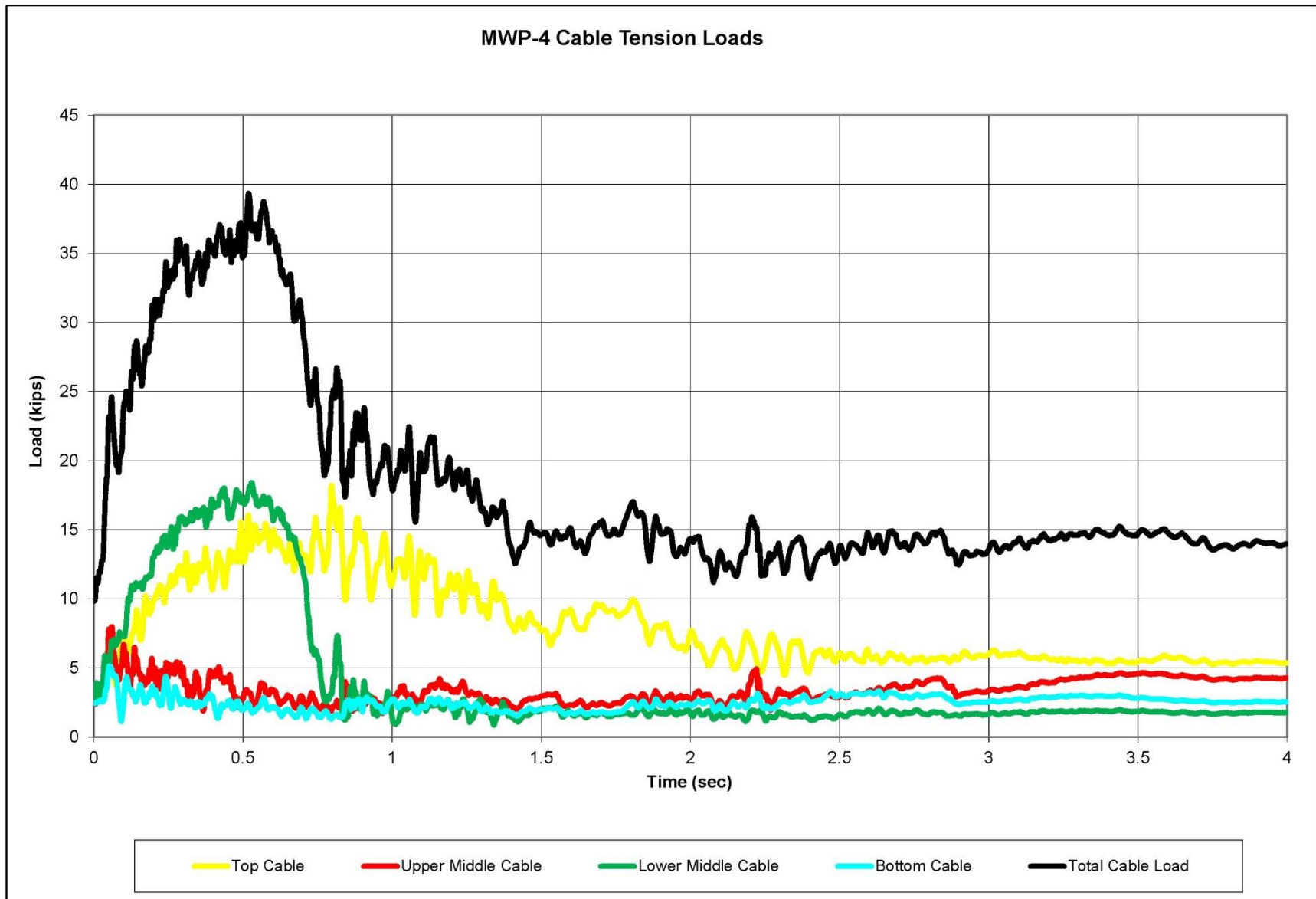


Figure F-1. Combined Load Cell Data, Test No. MWP-4

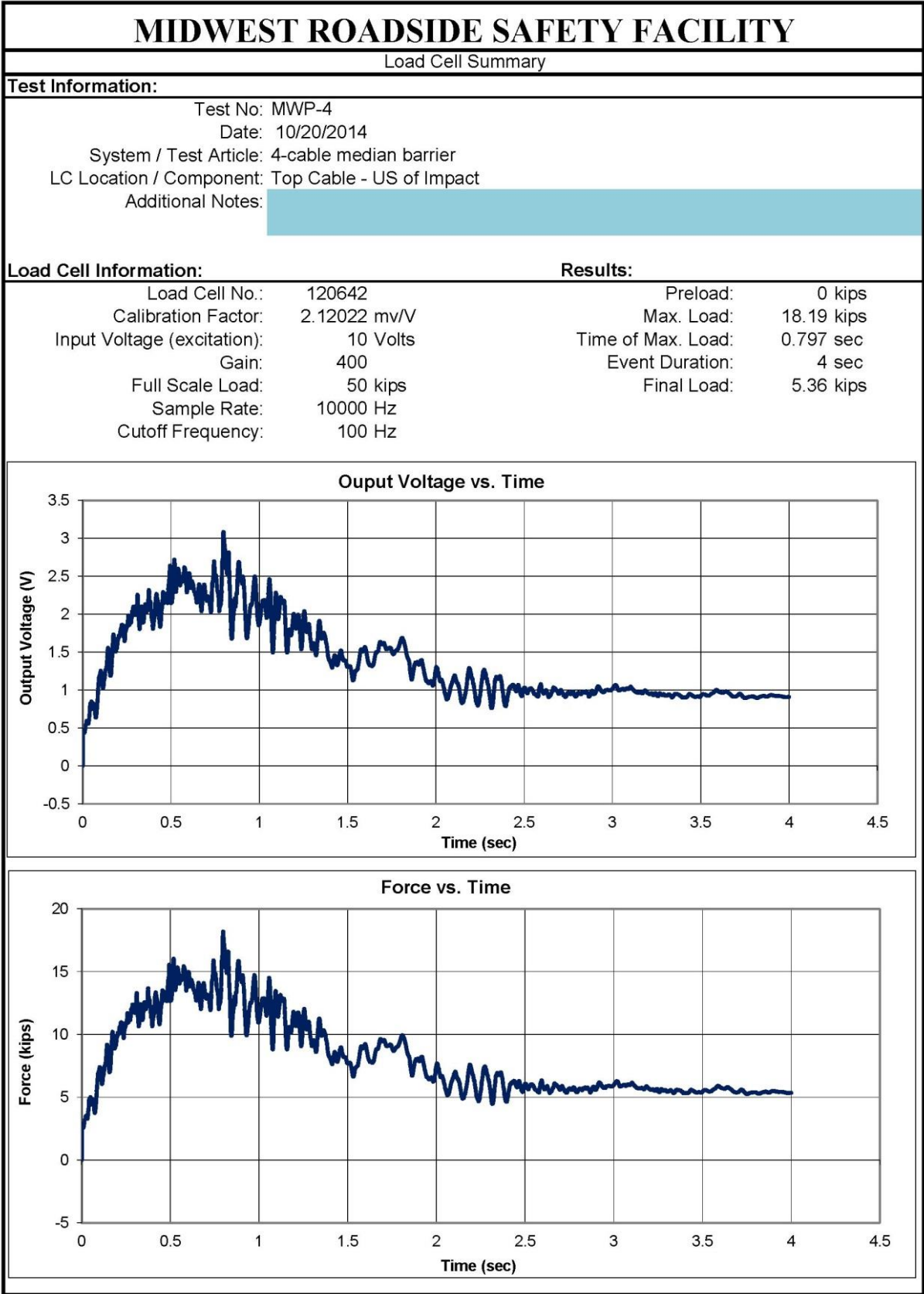


Figure F-2. Load Cell Data, Cable No. 4, Test No. MWP-4

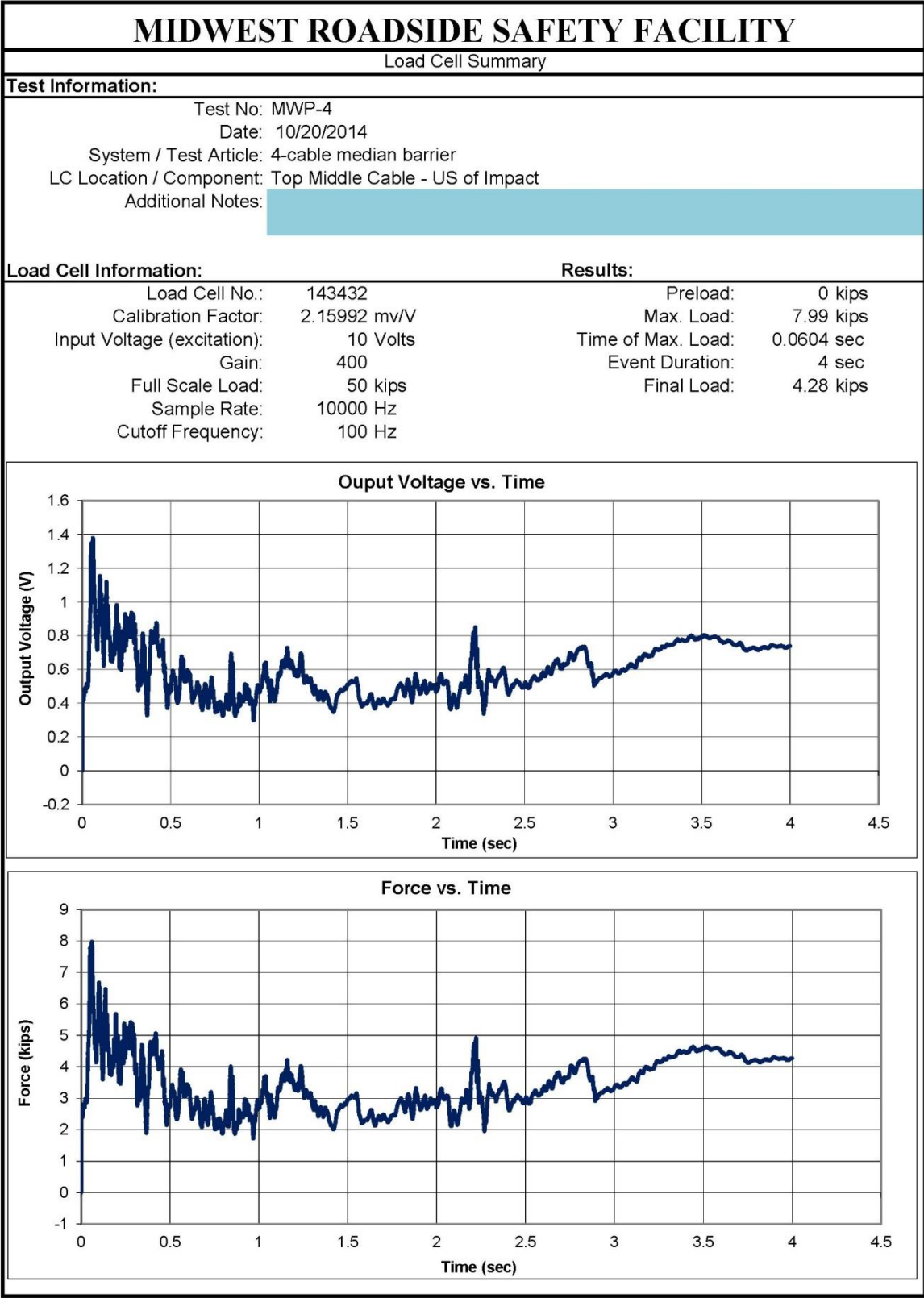


Figure F-3. Load Cell Data, Cable No. 3, Test No. MWP-4

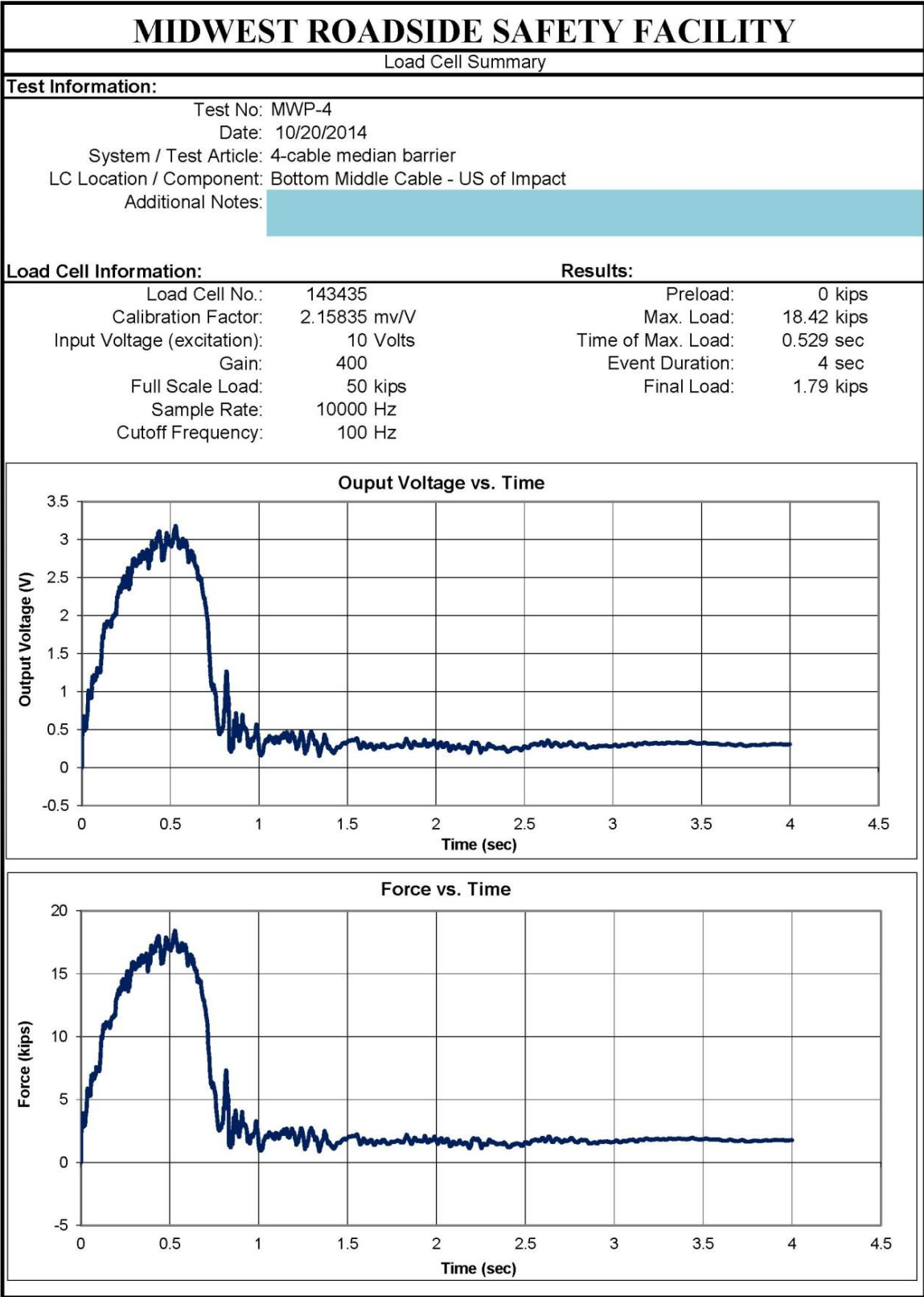


Figure F-4. Load Cell Data, Cable No. 2, Test No. MWP-4

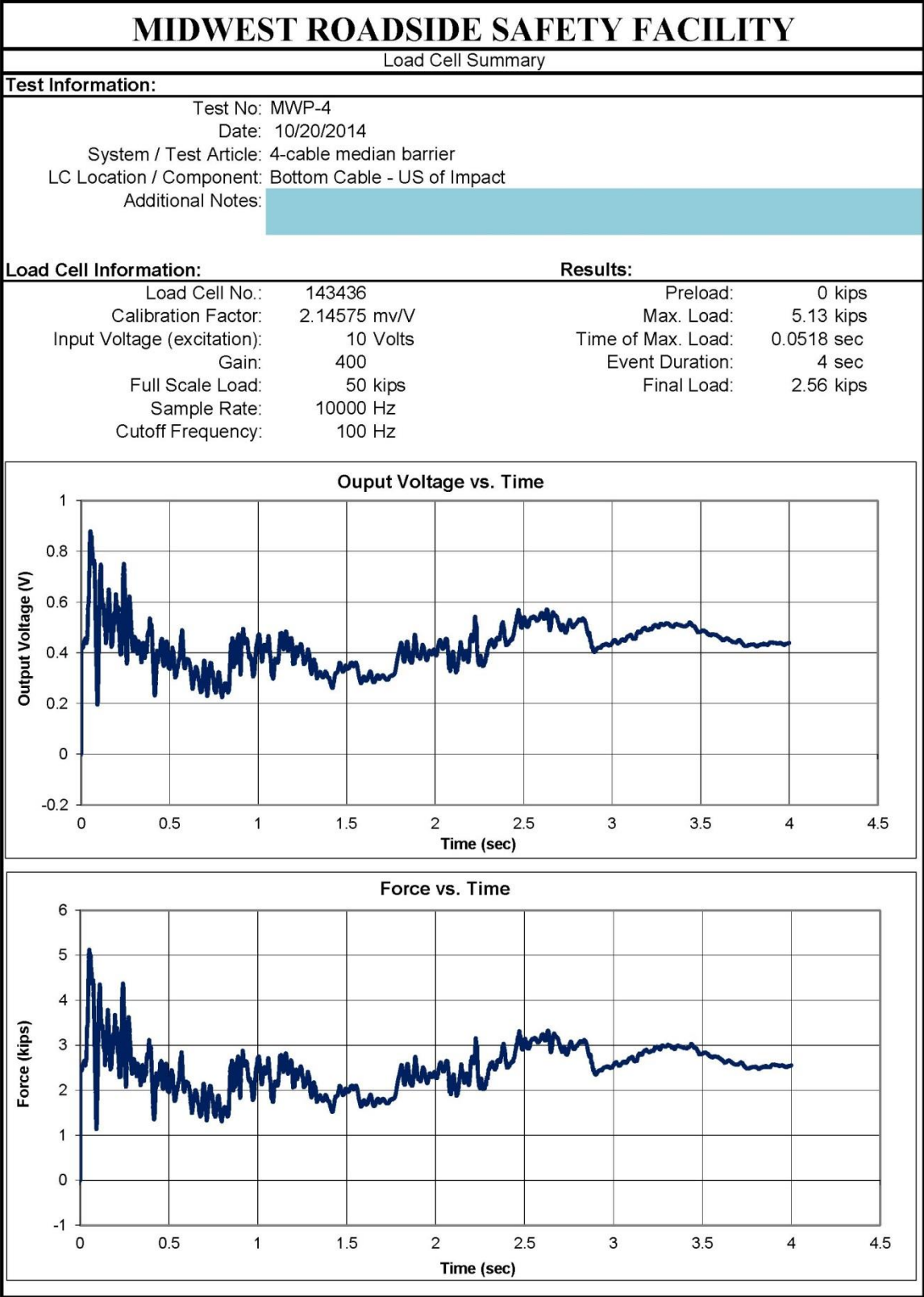


Figure F-5. Load Cell Data, Cable No. 1, Test No. MWP-4

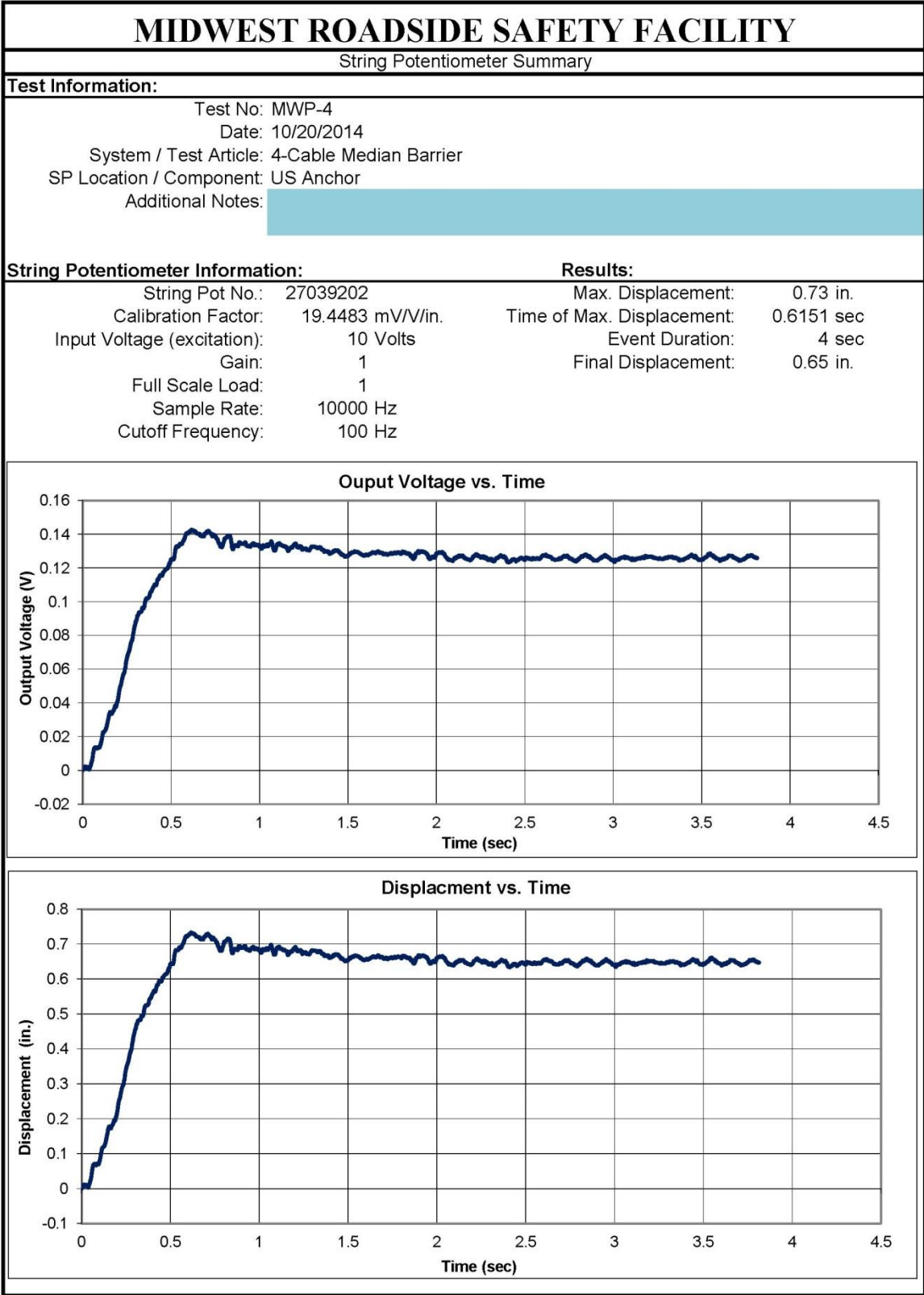


Figure F-6. String Potentiometer Data, Test No. MWP-4

Appendix G. Accelerometer and Rate Transducer Data Plots, Test No. MWP-6

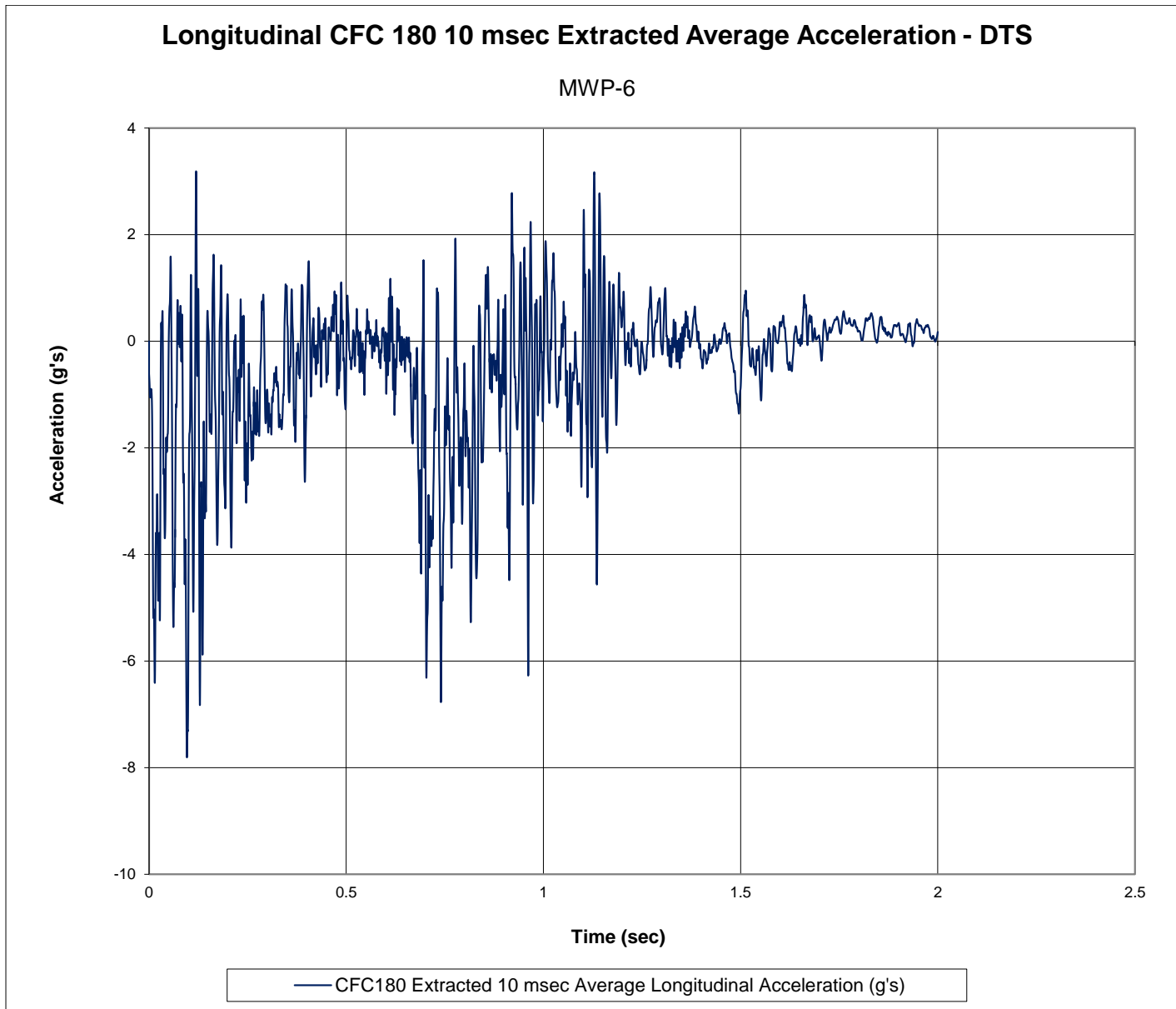


Figure G-1. 10-ms Average Longitudinal Deceleration (SLICE 1), Test No. MWP-6

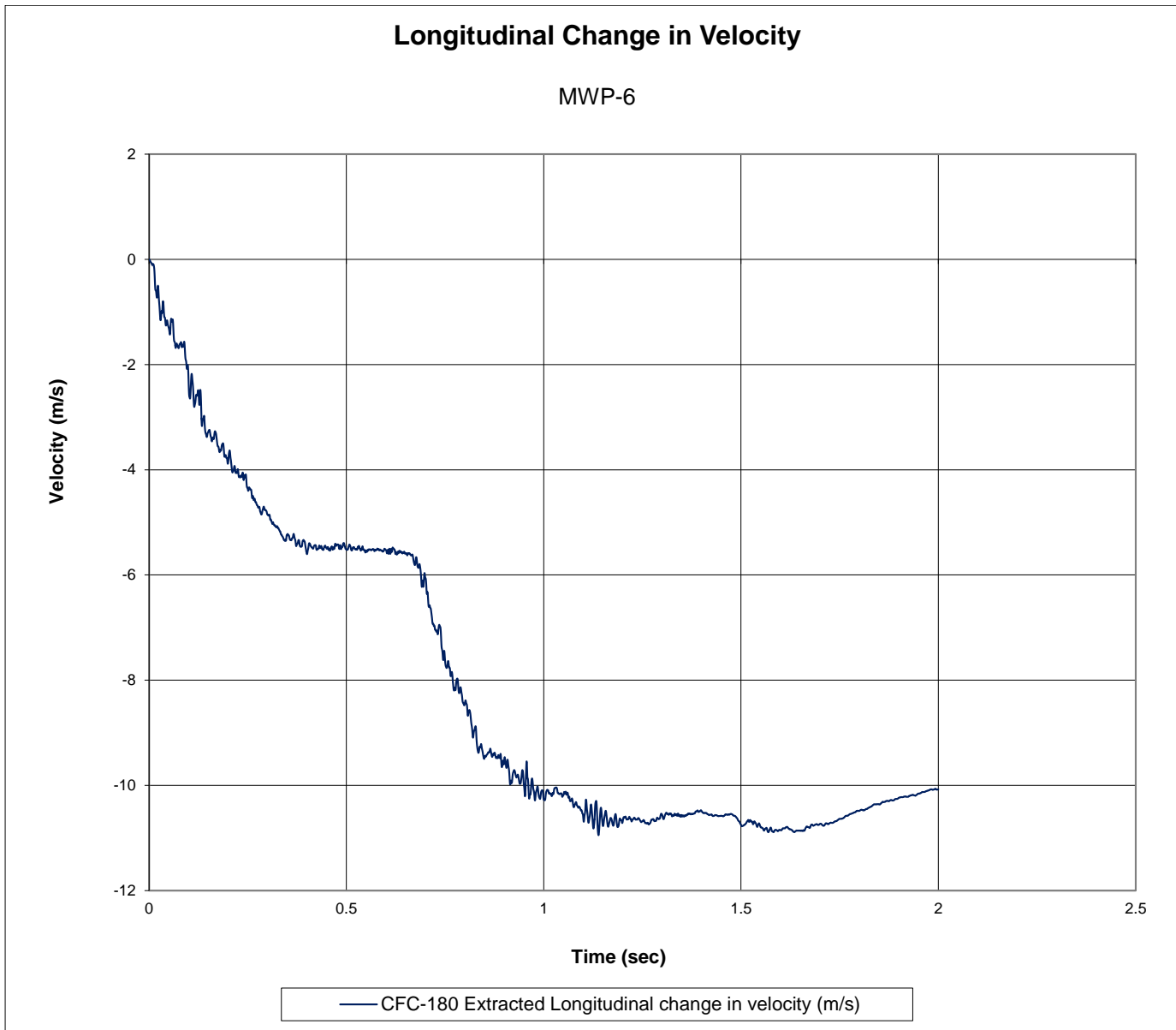


Figure G-2. Longitudinal Occupant Impact Velocity (SLICE 1), Test No. MWP-6

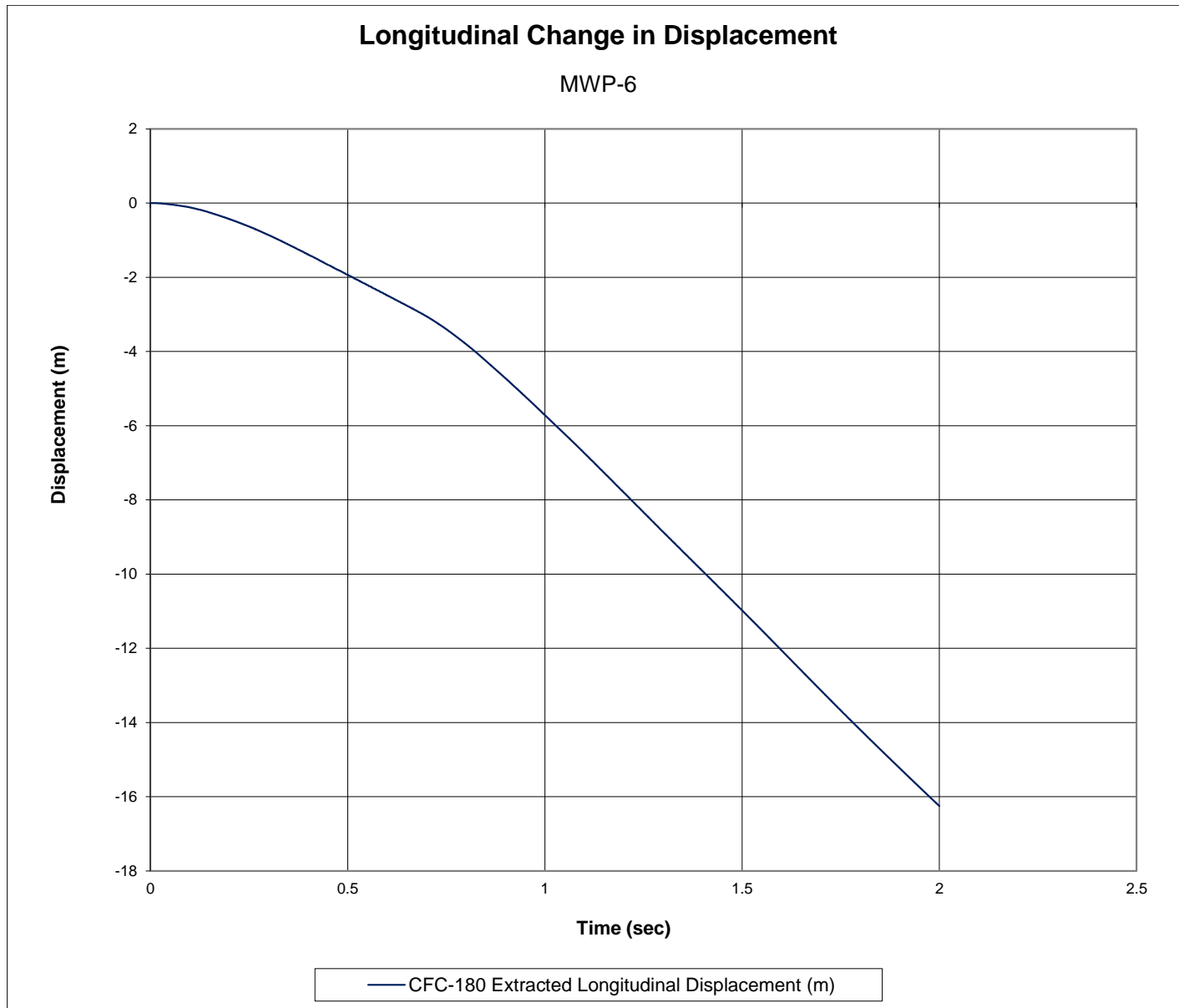


Figure G-3. Longitudinal Occupant Displacement (SLICE 1), Test No. MWP-6

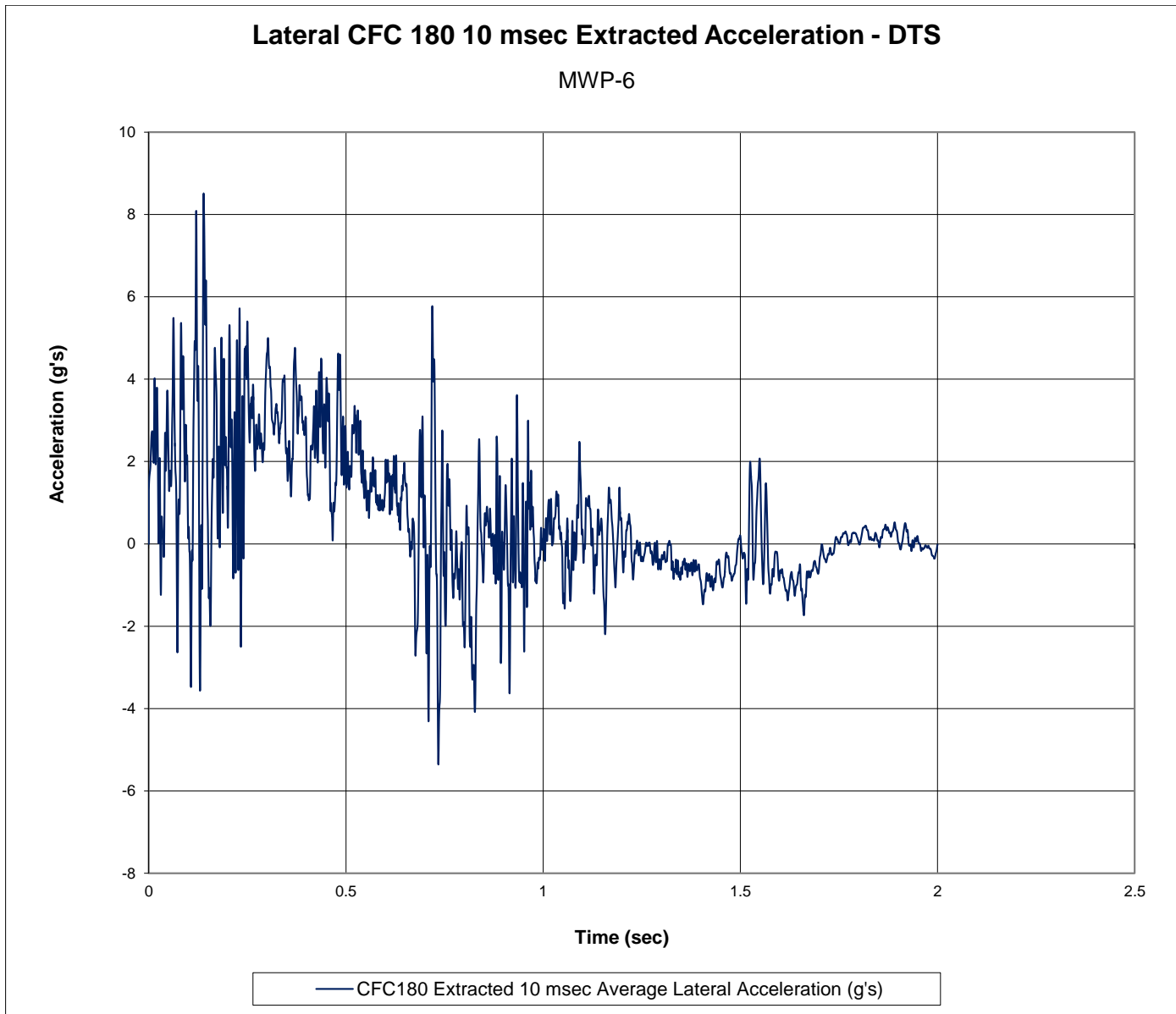


Figure G-4. 10-ms Average Lateral Deceleration (SLICE 1), Test No. MWP-6

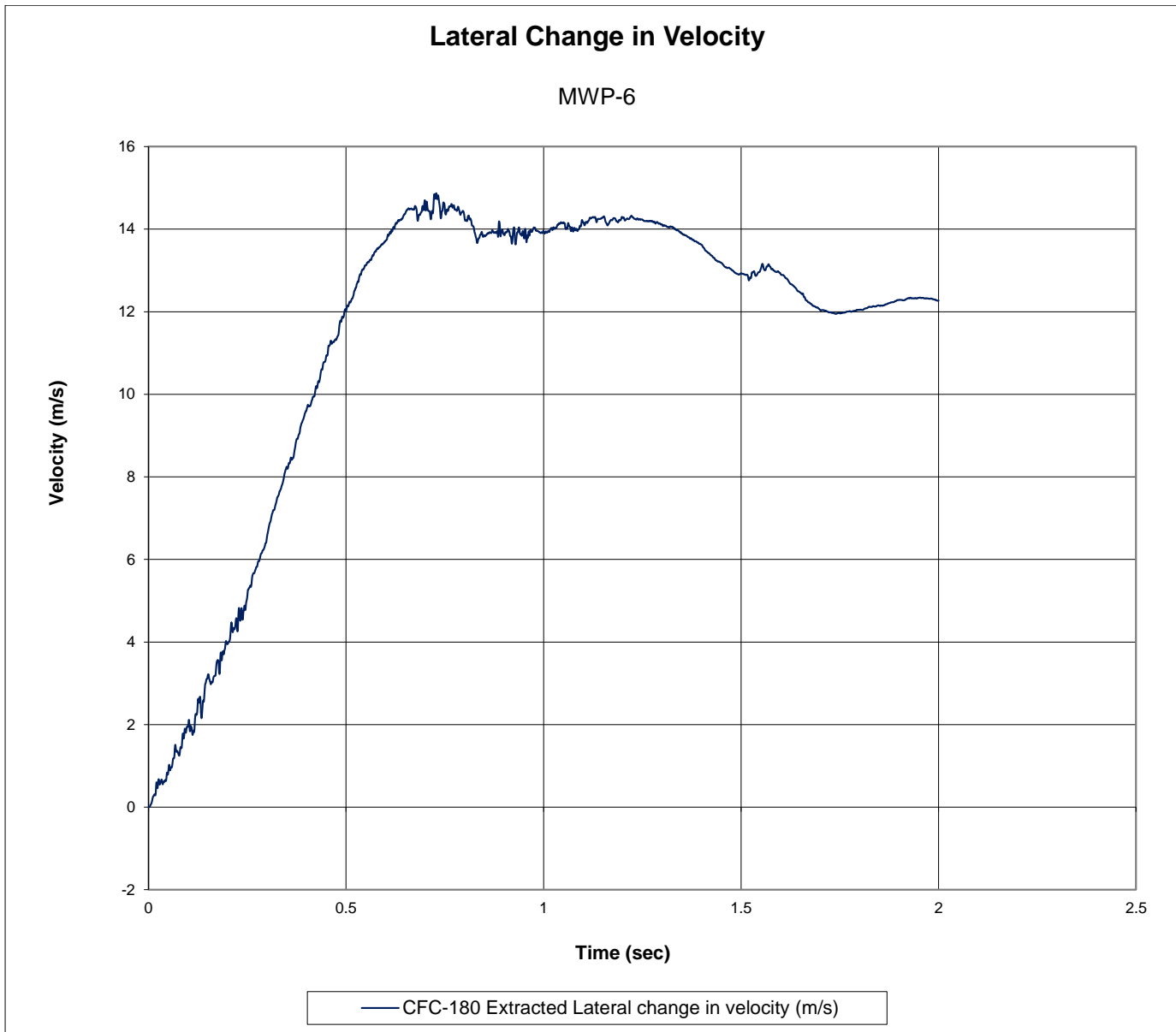


Figure G-5. Lateral Occupation Impact Velocity (SLICE 1), Test No. MWP-6

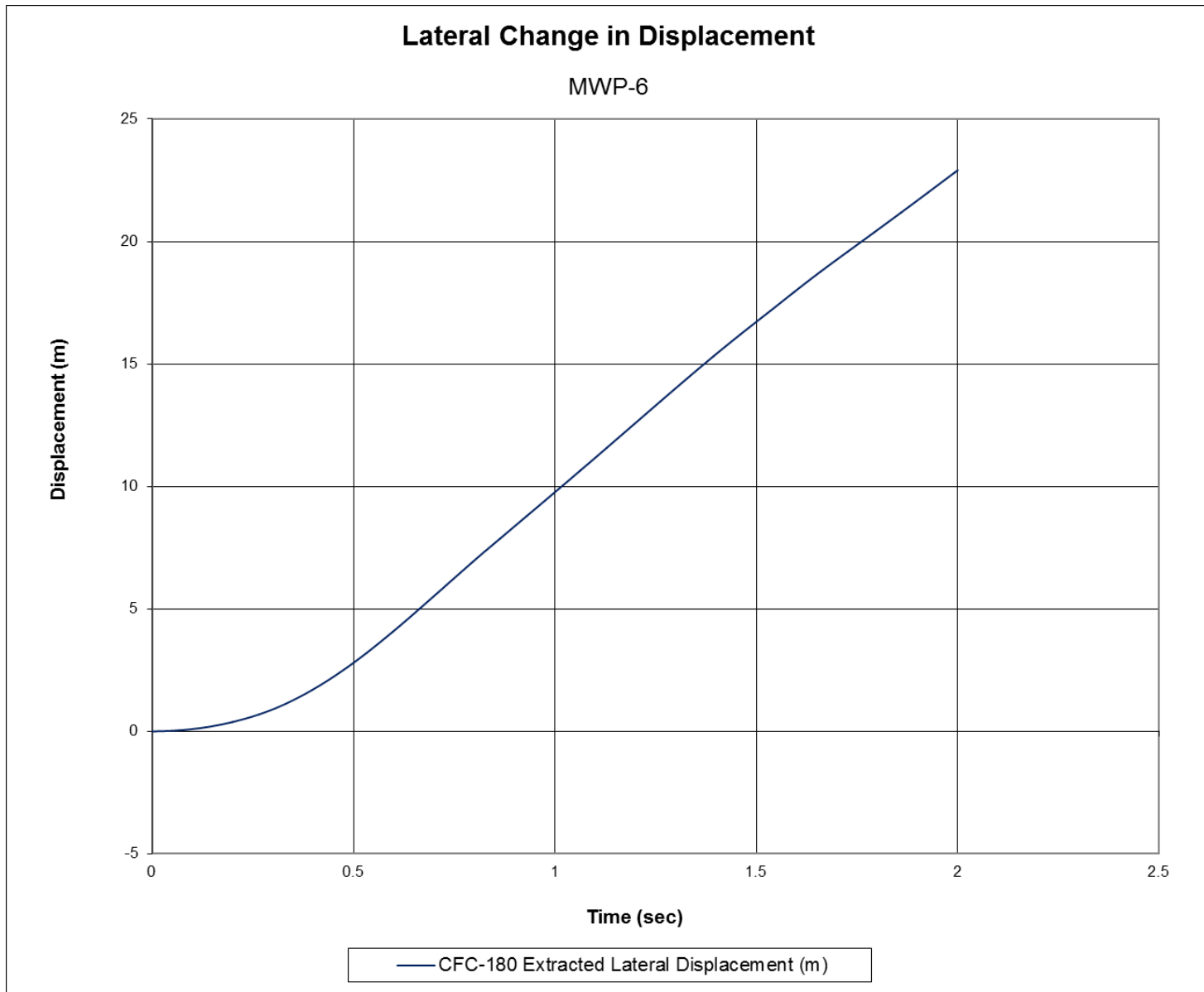


Figure G-6. Lateral Occupant Displacement (SLICE 1), Test No. MWP-6



Figure G-7. Vehicle Angular Displacements (SLICE 1), Test No. MWP-6

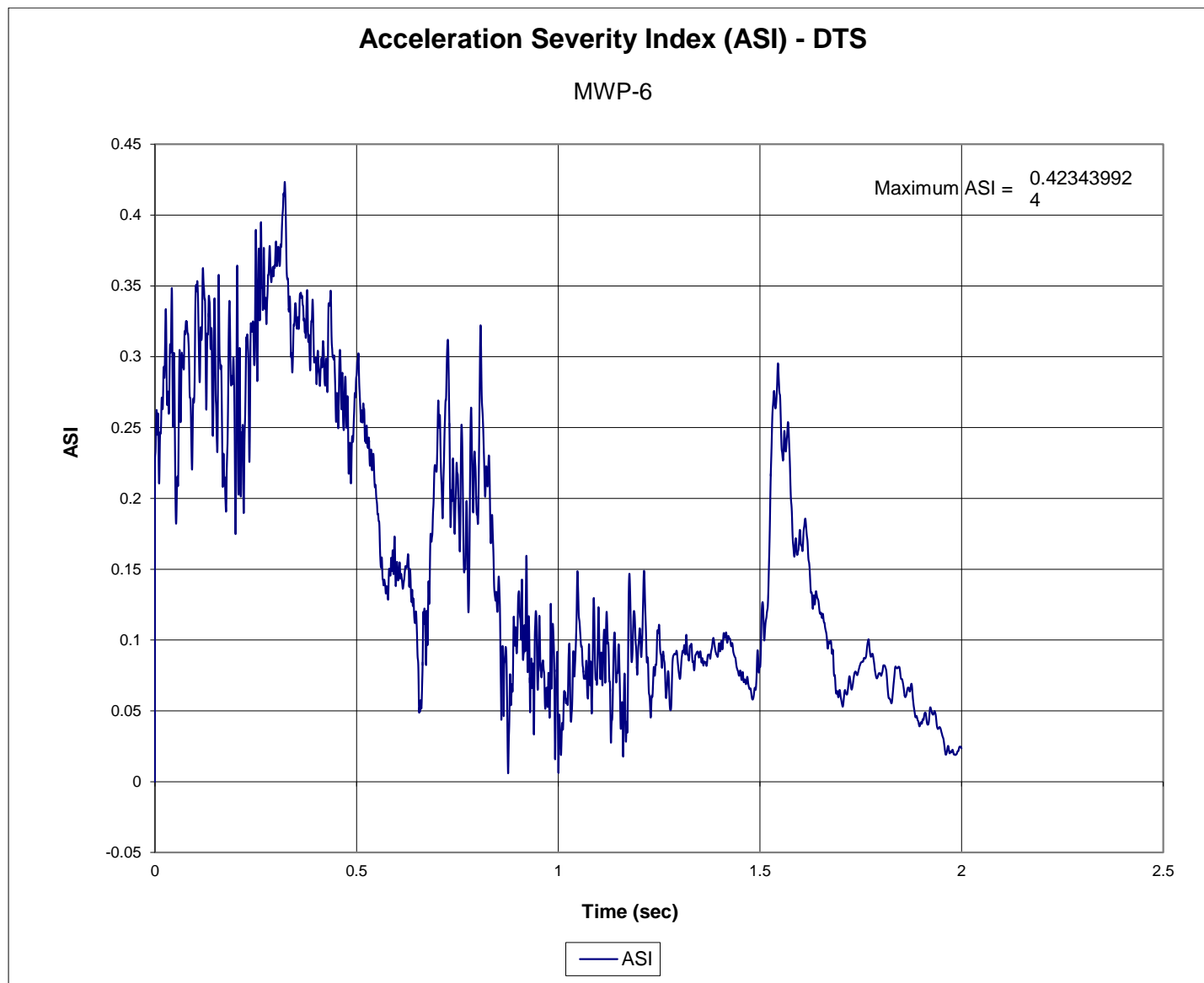


Figure G-8. Acceleration Service Index (SLICE 1), Test No. MWP-6

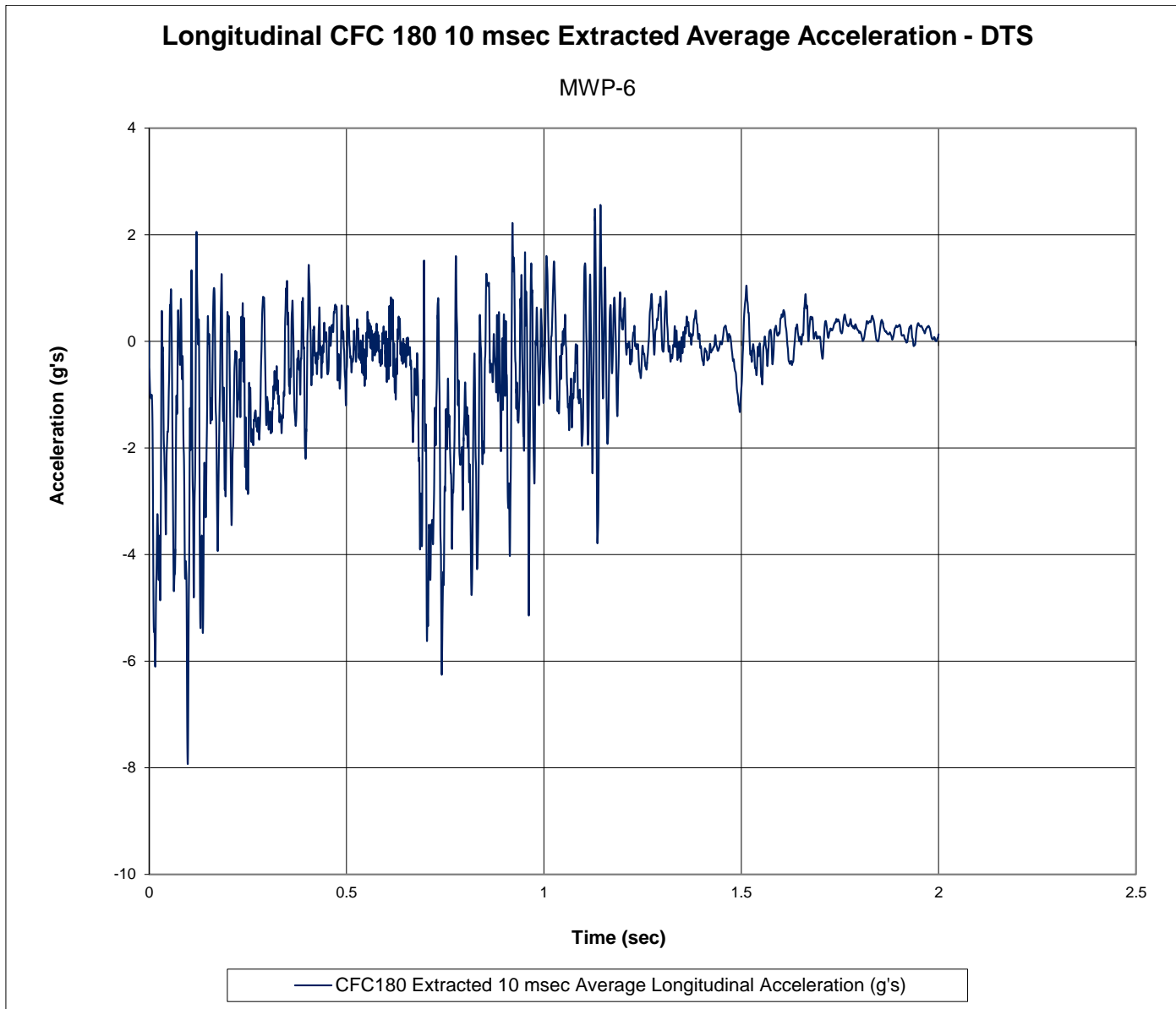


Figure G-9. 10-ms Average Longitudinal Deceleration (SLICE 2), Test No.MWP-6

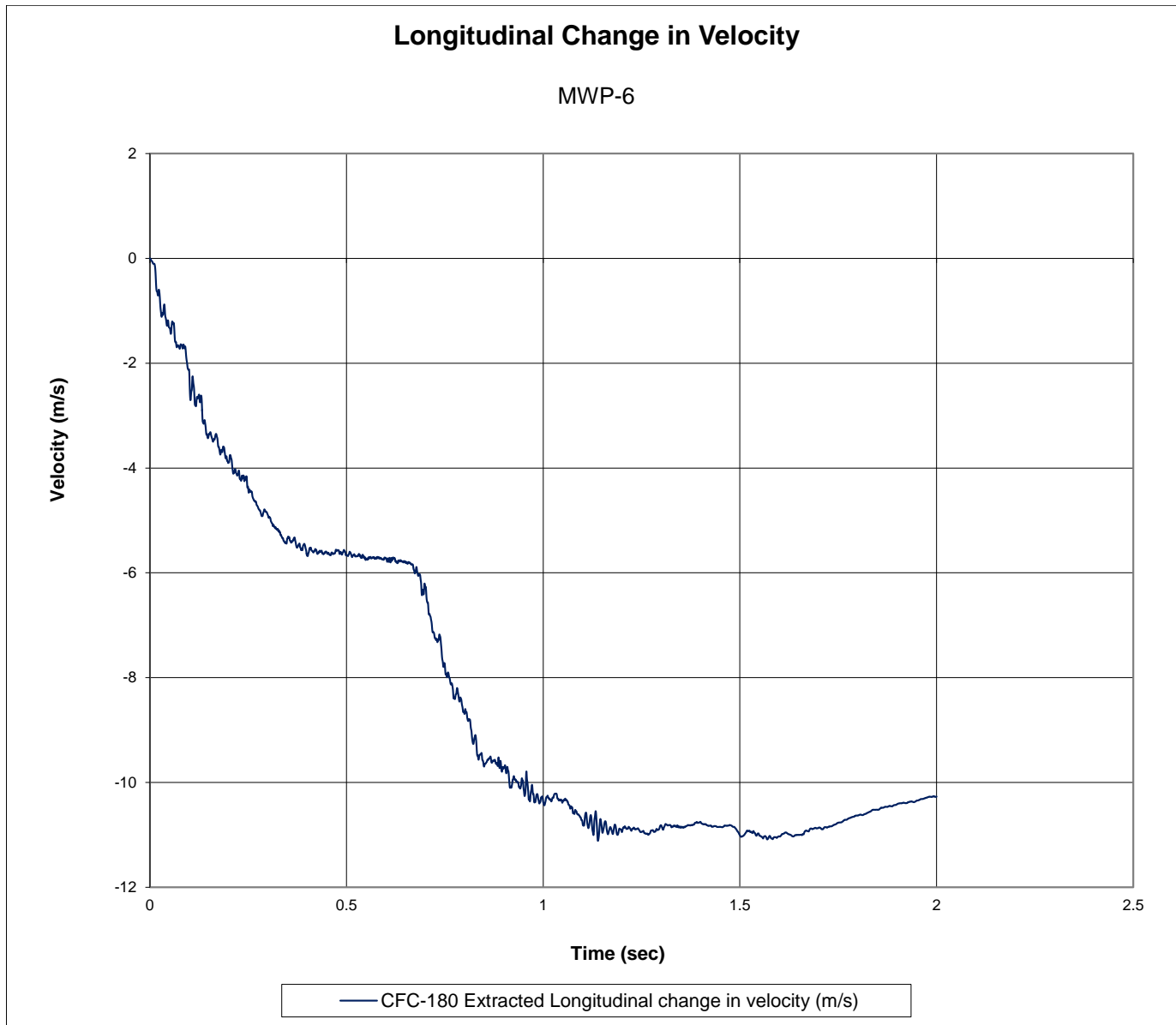


Figure G-10. Longitudinal Occupant Impact Velocity (SLICE 2), Test No. MWP-6

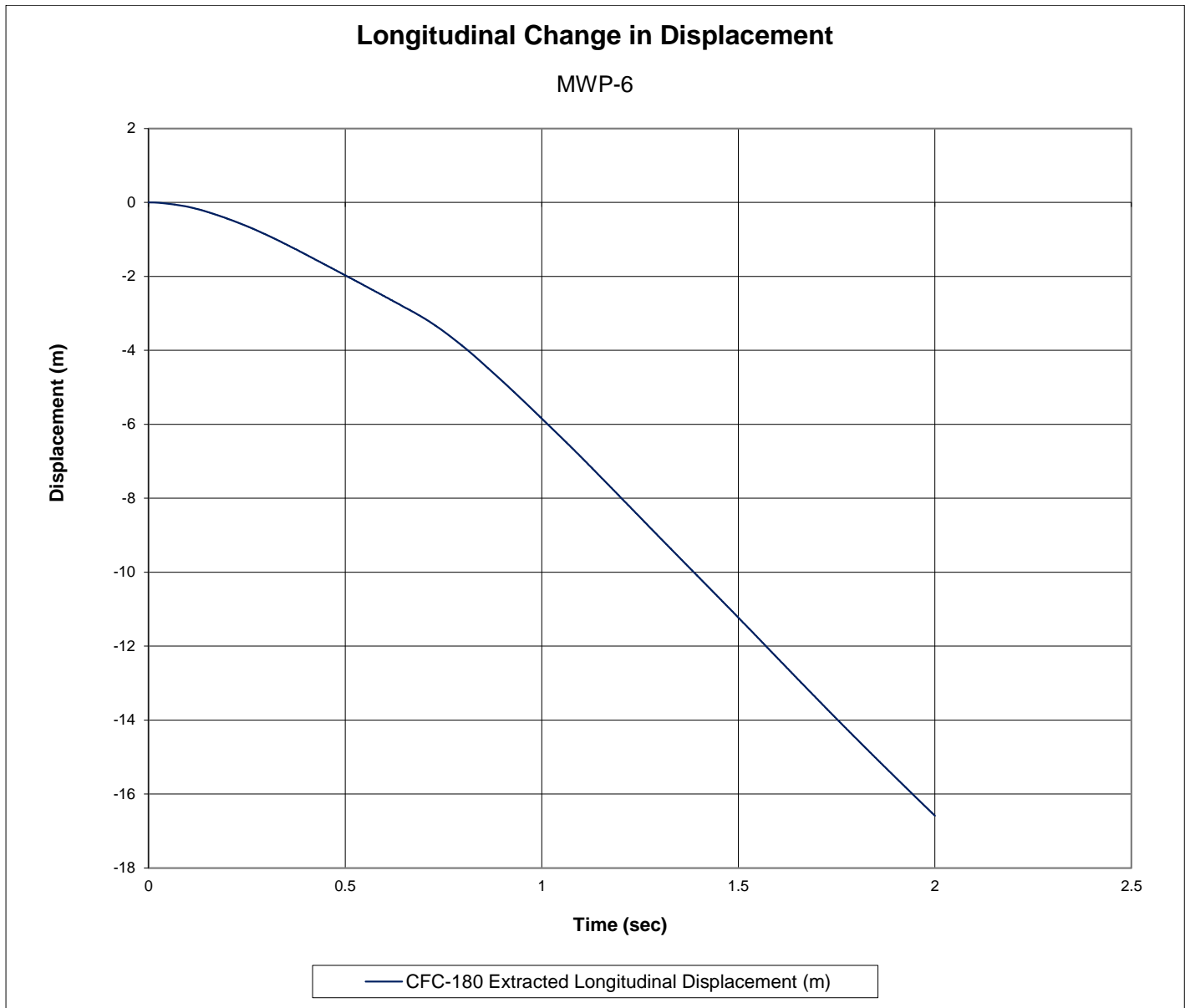


Figure G-11. Longitudinal Occupant Displacement (SLICE 2), Test No. MWP-6

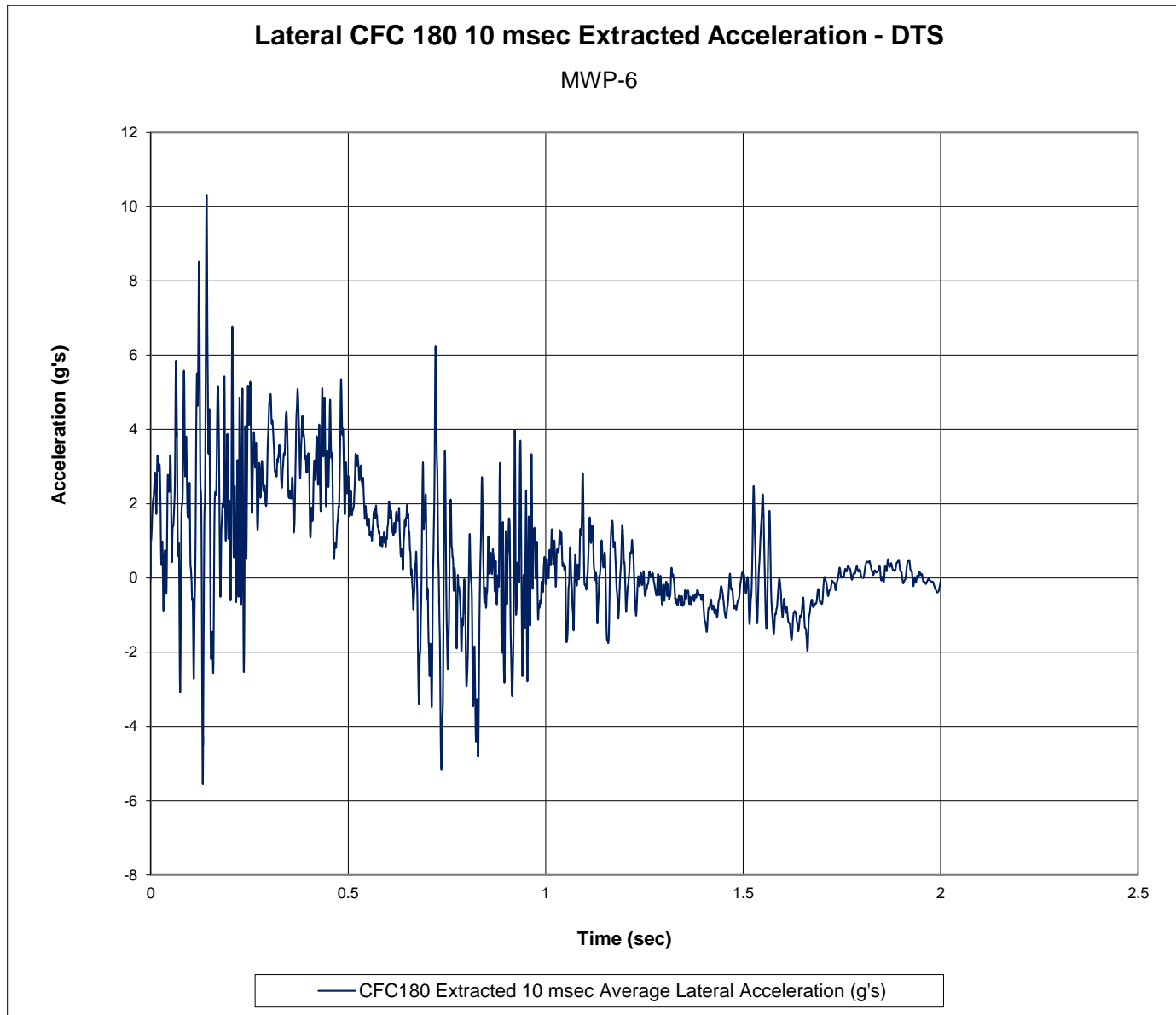


Figure G-12. 10-ms Average Lateral Deceleration (SLICE 2), Test No.MWP-6

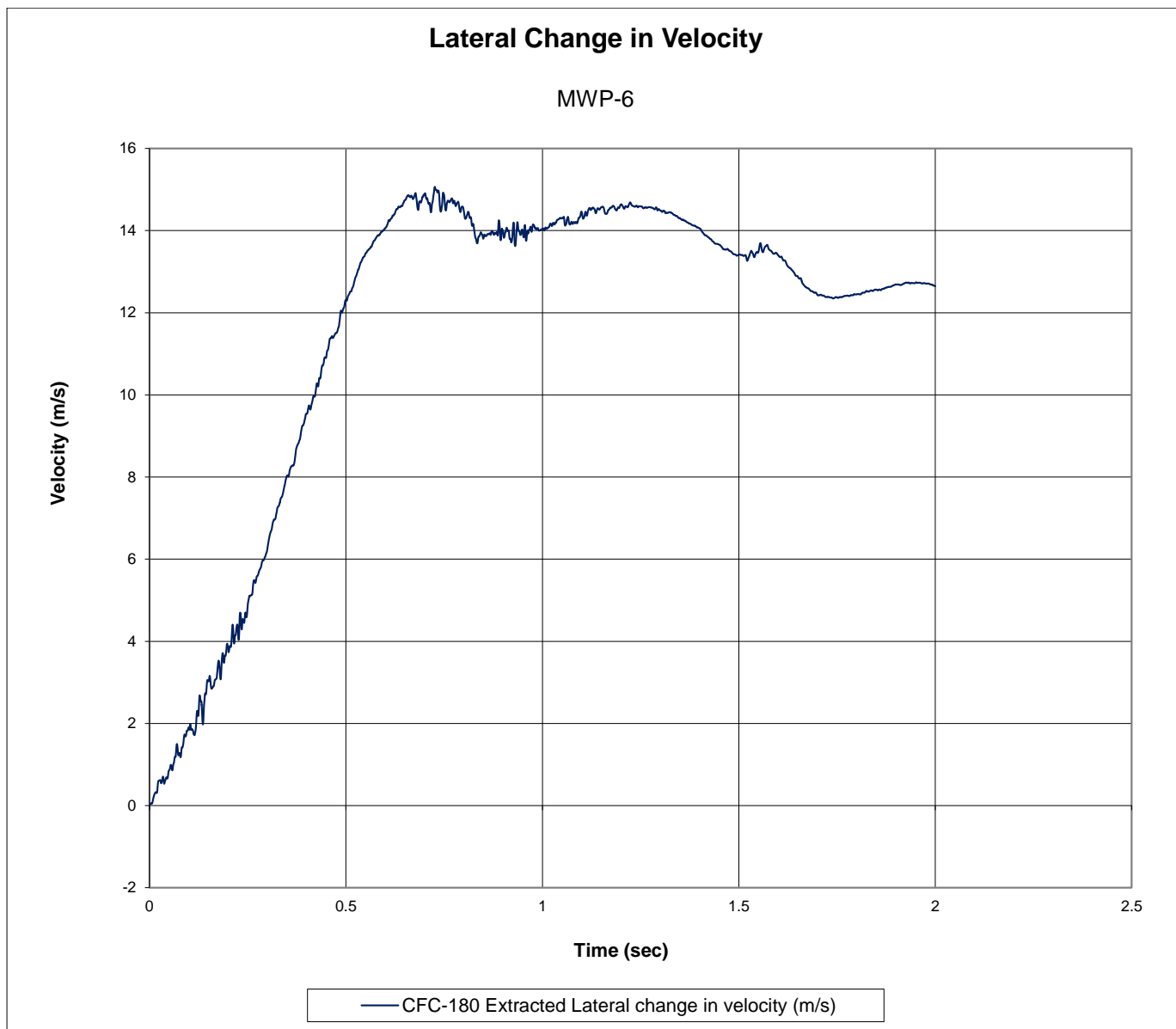


Figure G-13. Lateral Occupant Impact Velocity (SLICE 2), Test No. MWP-6



Figure G-14. Lateral Occupant Displacement (SLICE 2), Test No. MWP-6

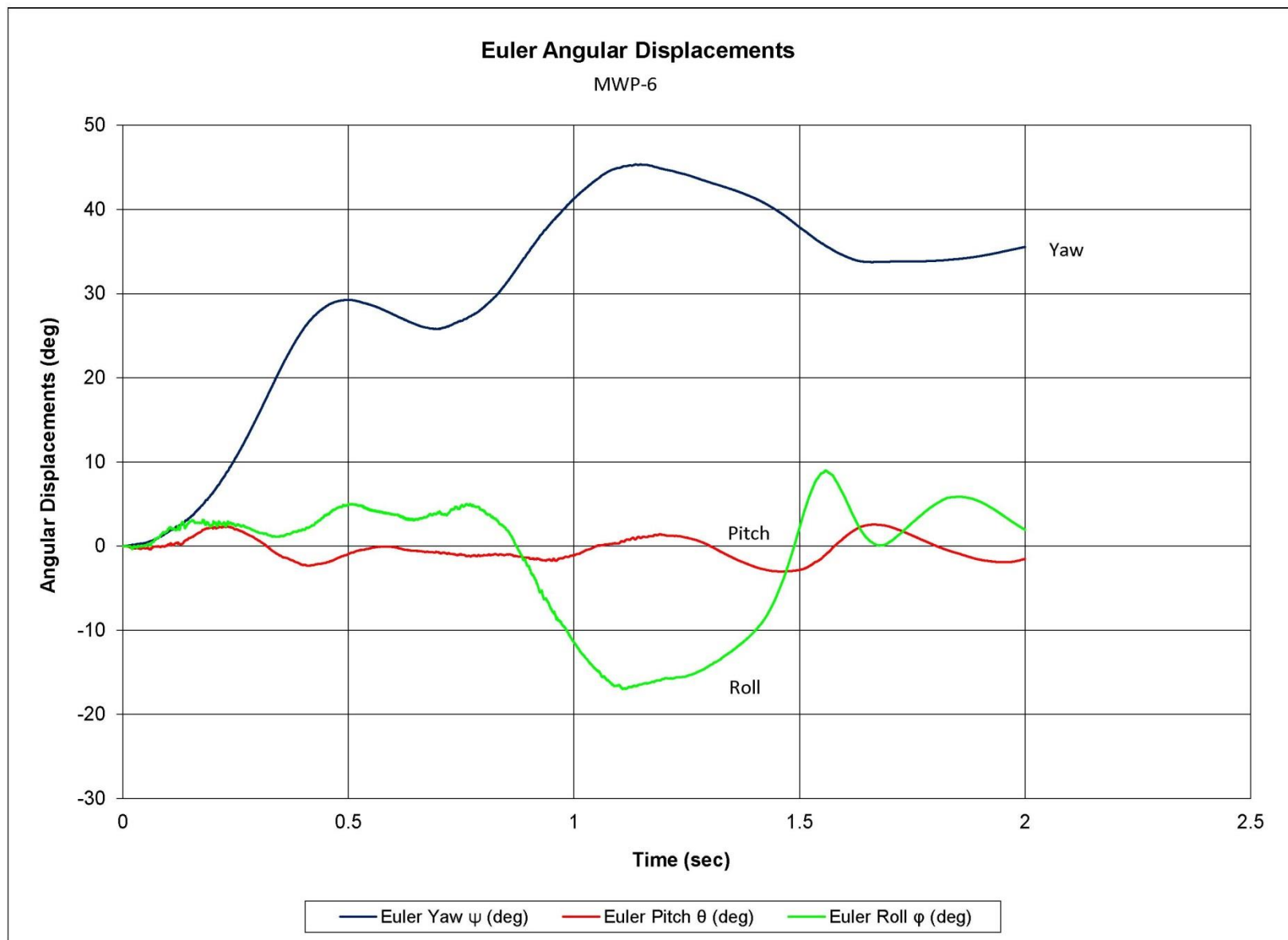


Figure G-15. Vehicle Angular Displacements (SLICE 2), Test No. MWP-6

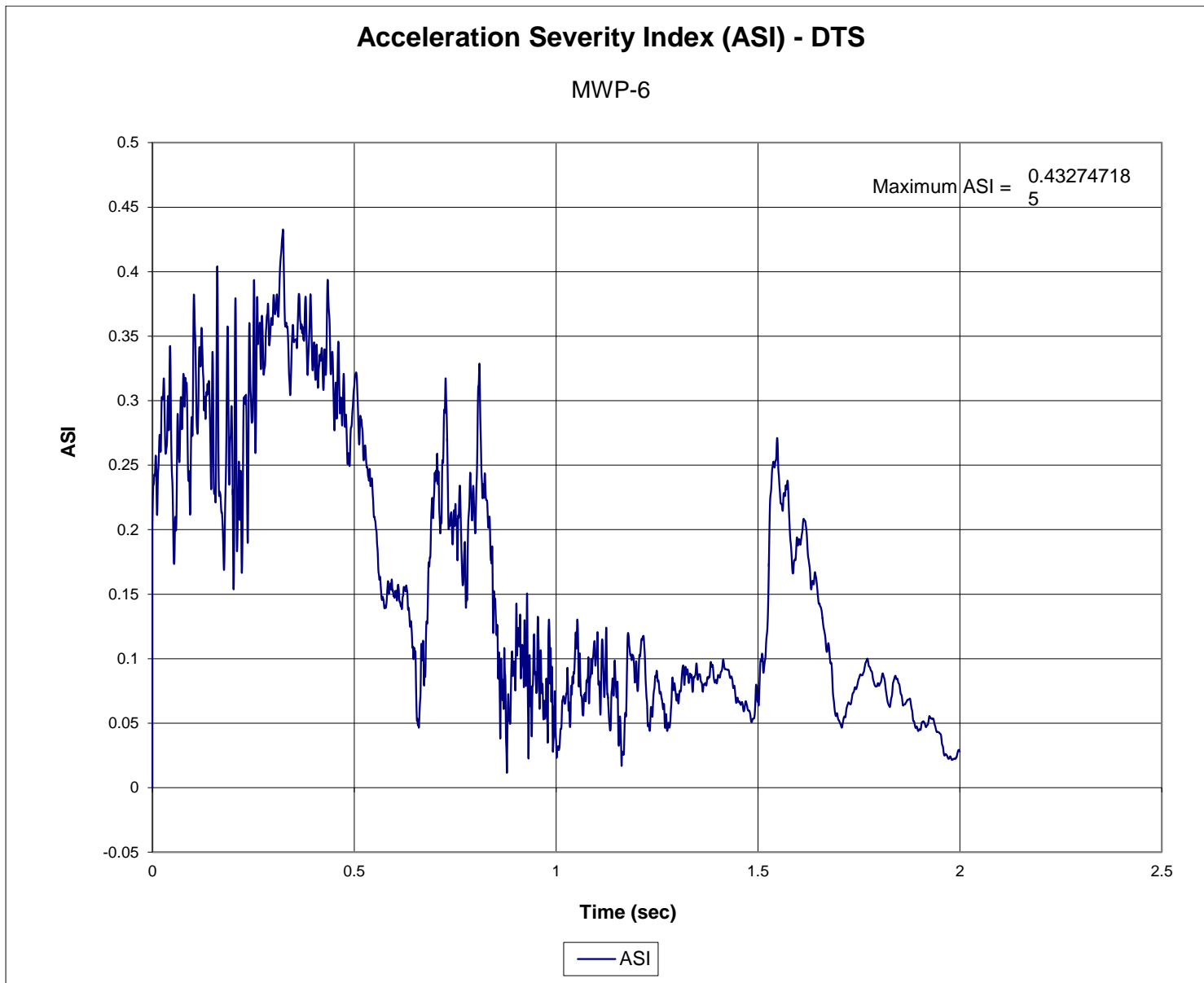


Figure G-16. Acceleration Severity Index (SLICE 2), Test No. MWP-6

Appendix H. Load Cell and String Potentiometer Data, Test No. MWP-6

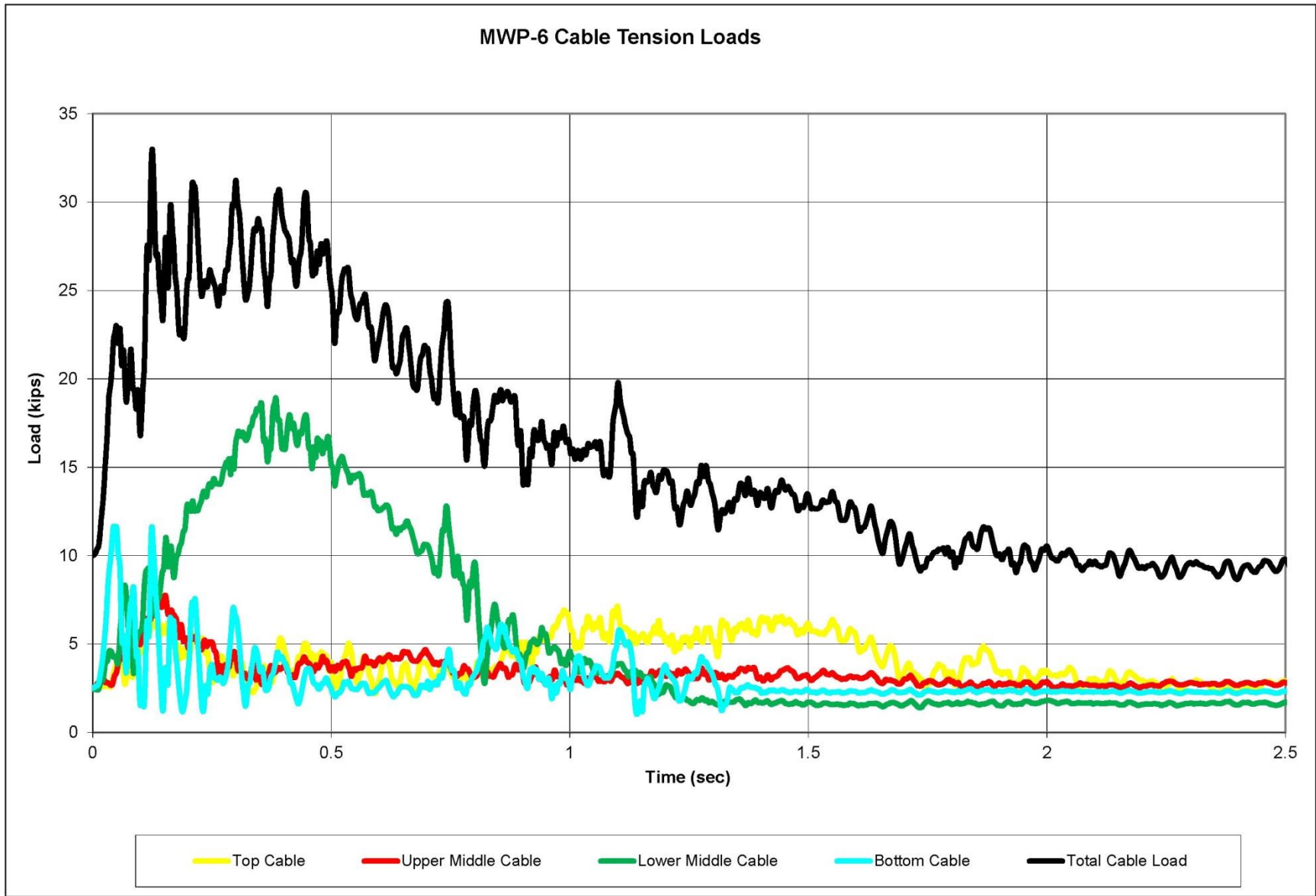


Figure H-1. Combined Load Cell Data, Test No. MWP-6

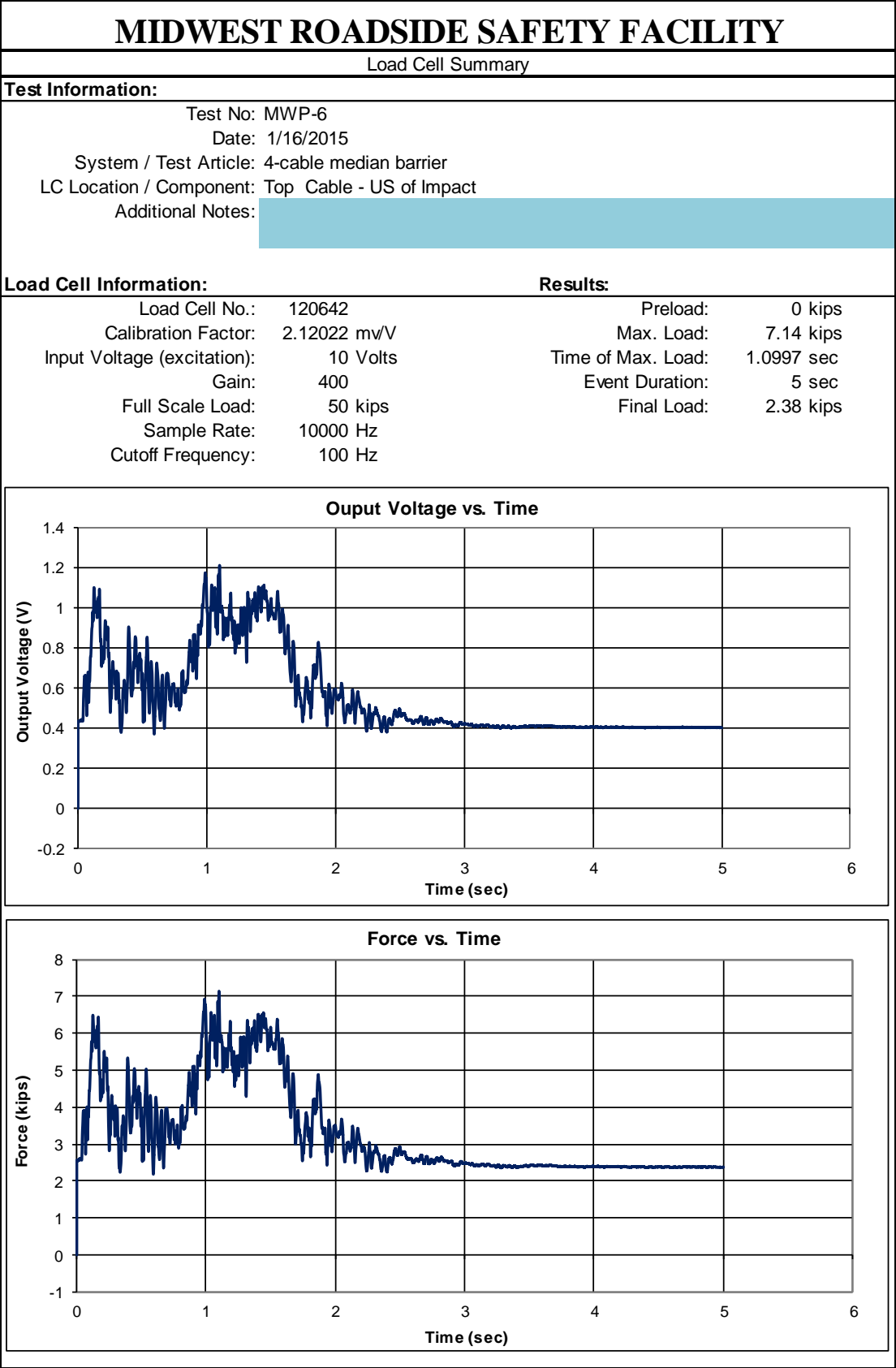


Figure H-2. Load Cell Data, Cable No. 4, Test No. MWP-6

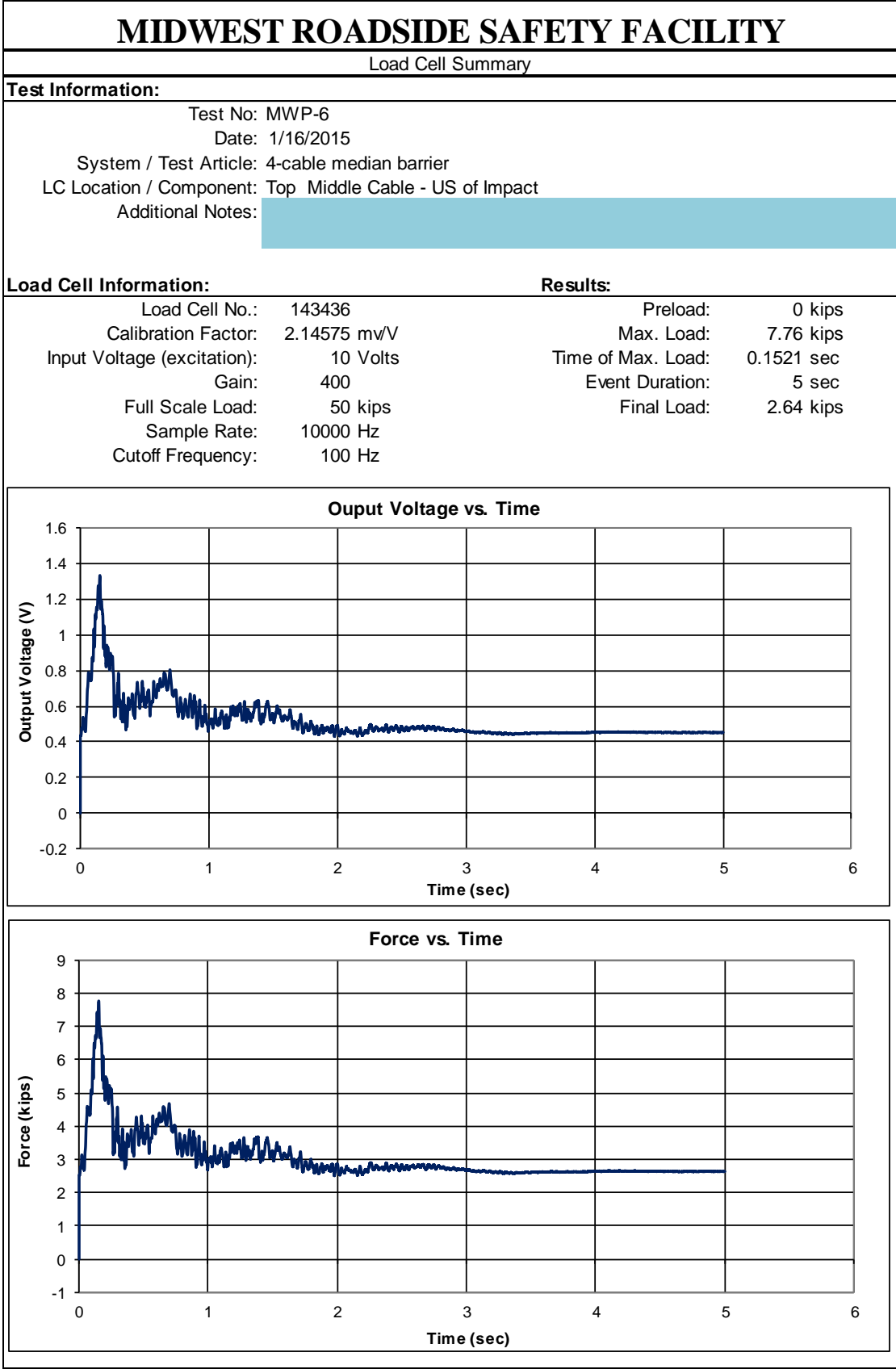


Figure H-3. Load Cell Data, Cable No. 3, Test No. MWP-6

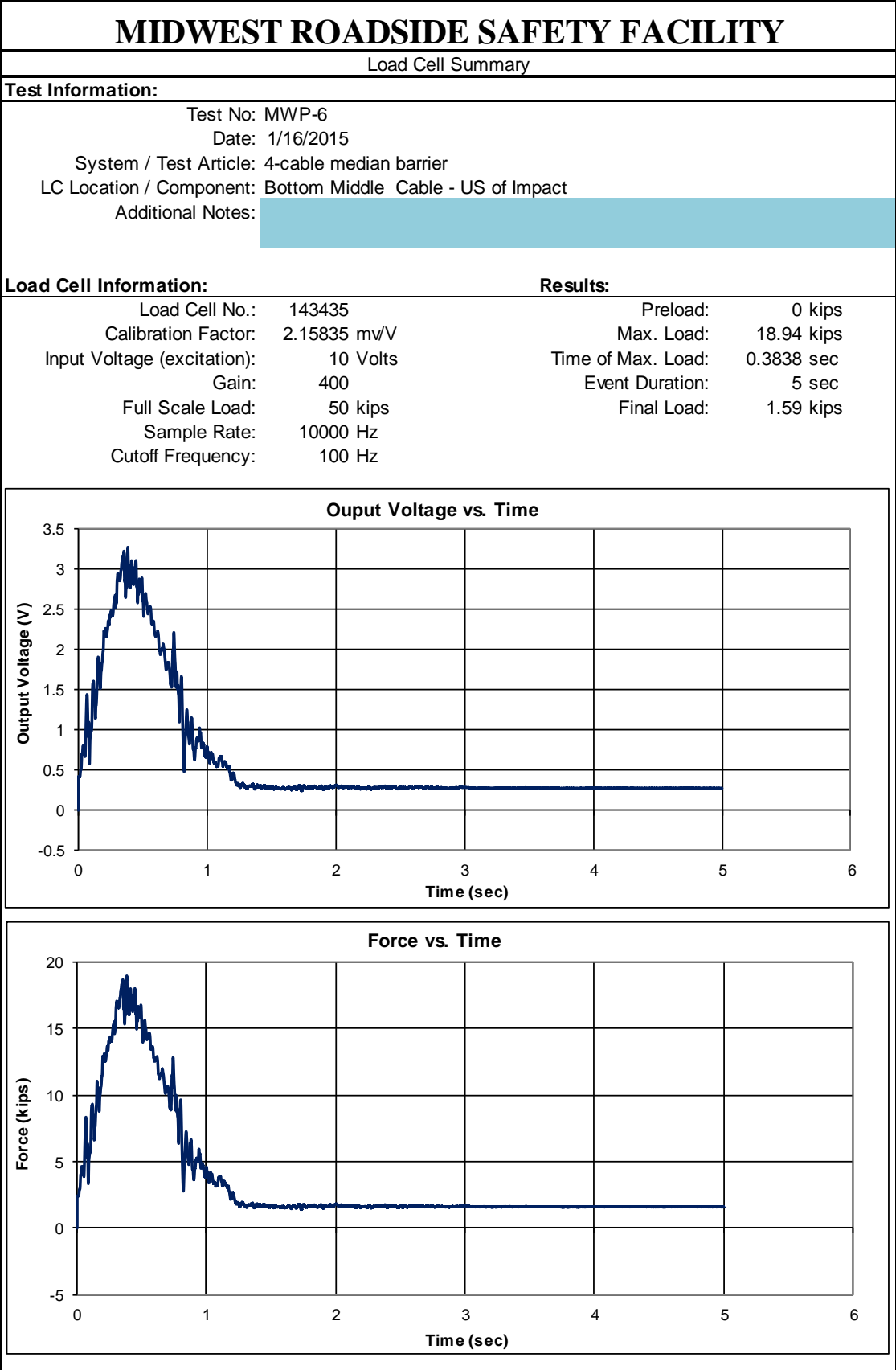


Figure H-4. Load Cell Data, Cable No. 2, Test No. MWP-6

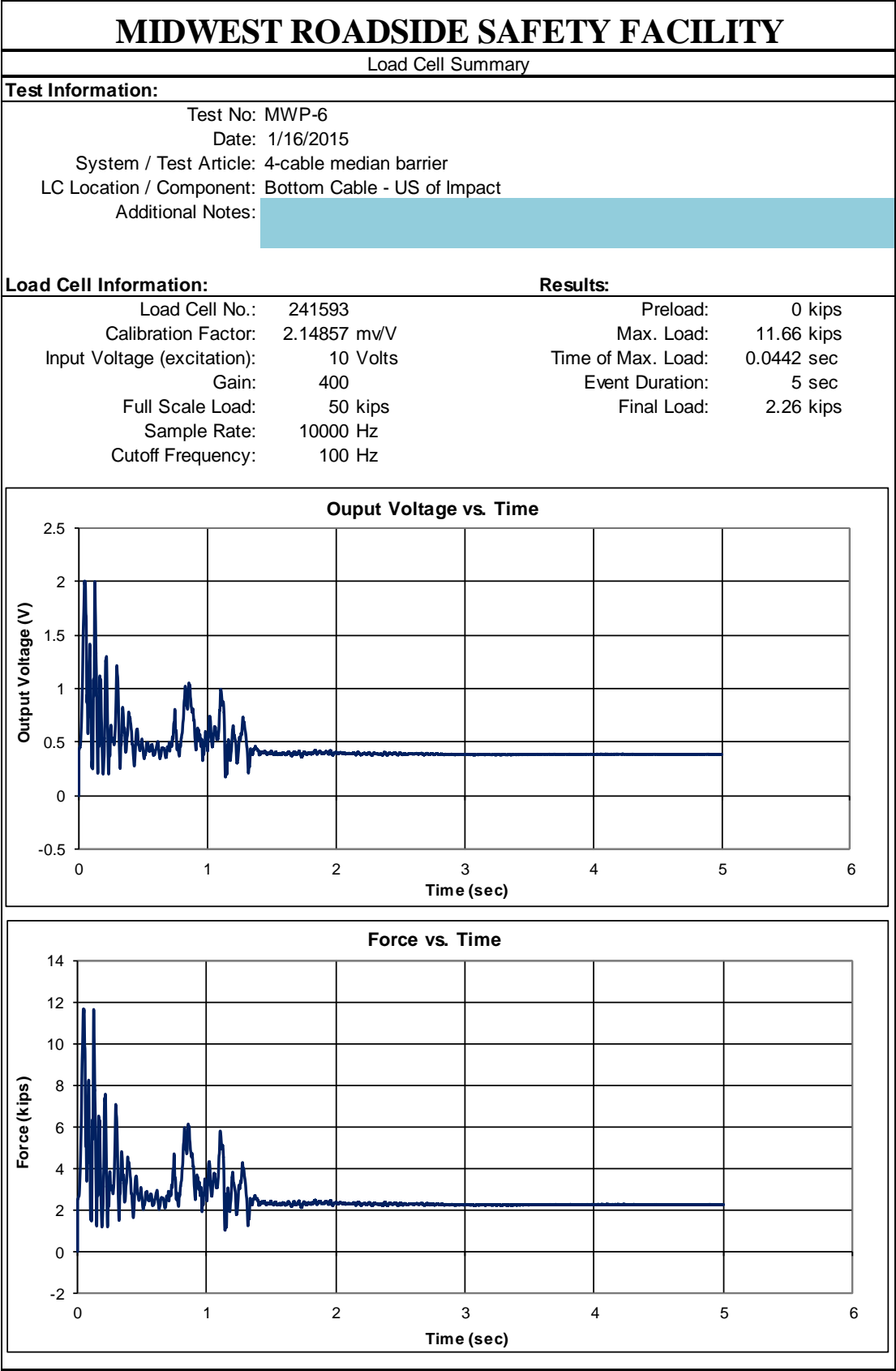


Figure H-5. Load Cell Data, Cable No. 1, Test No. MWP-6

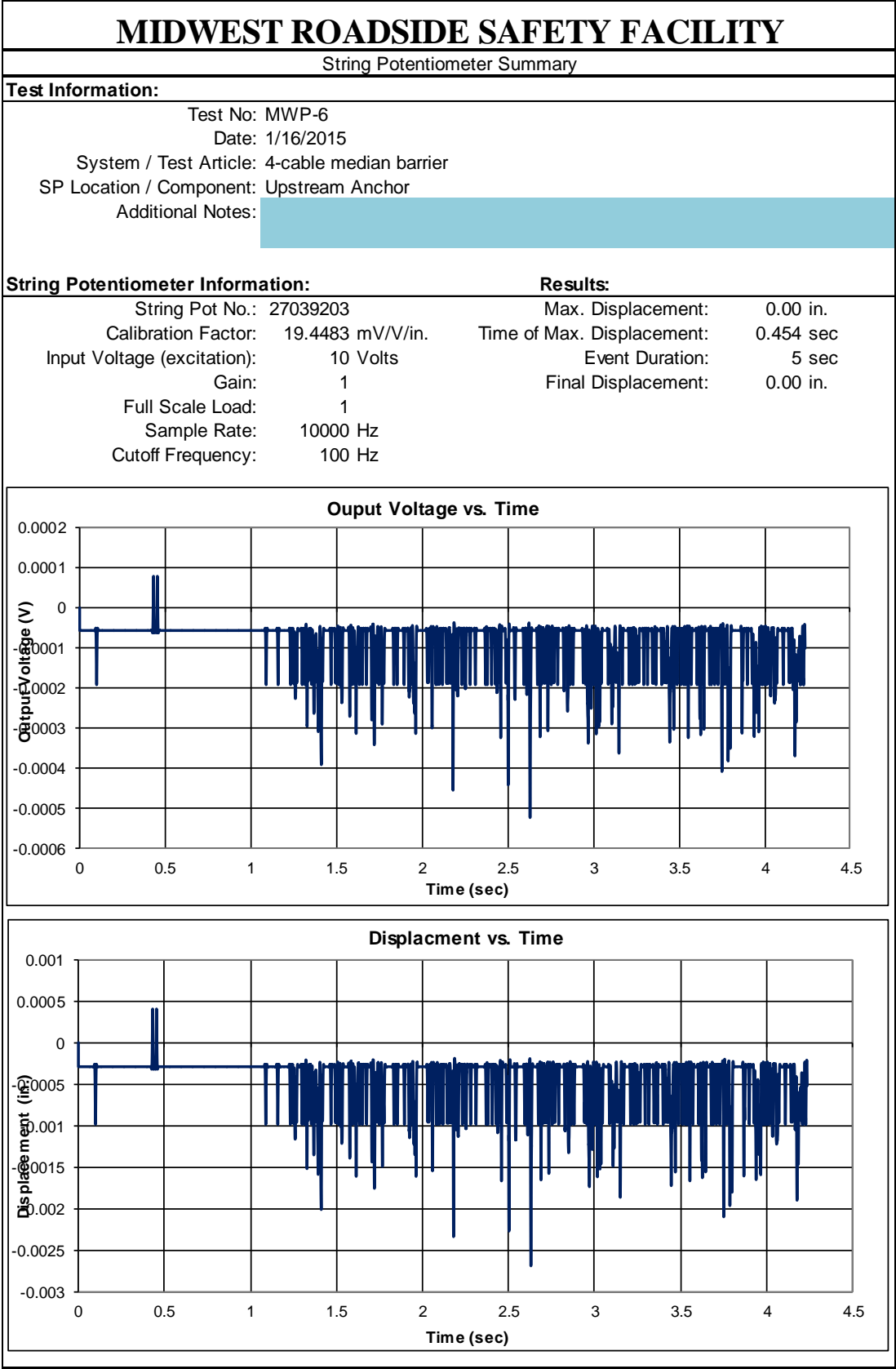


Figure H-6. String Potentiometer Data, Test No. MWP-6

Appendix I. Accelerometer and Rate Transducer Data Plots, Test No. MWP-7

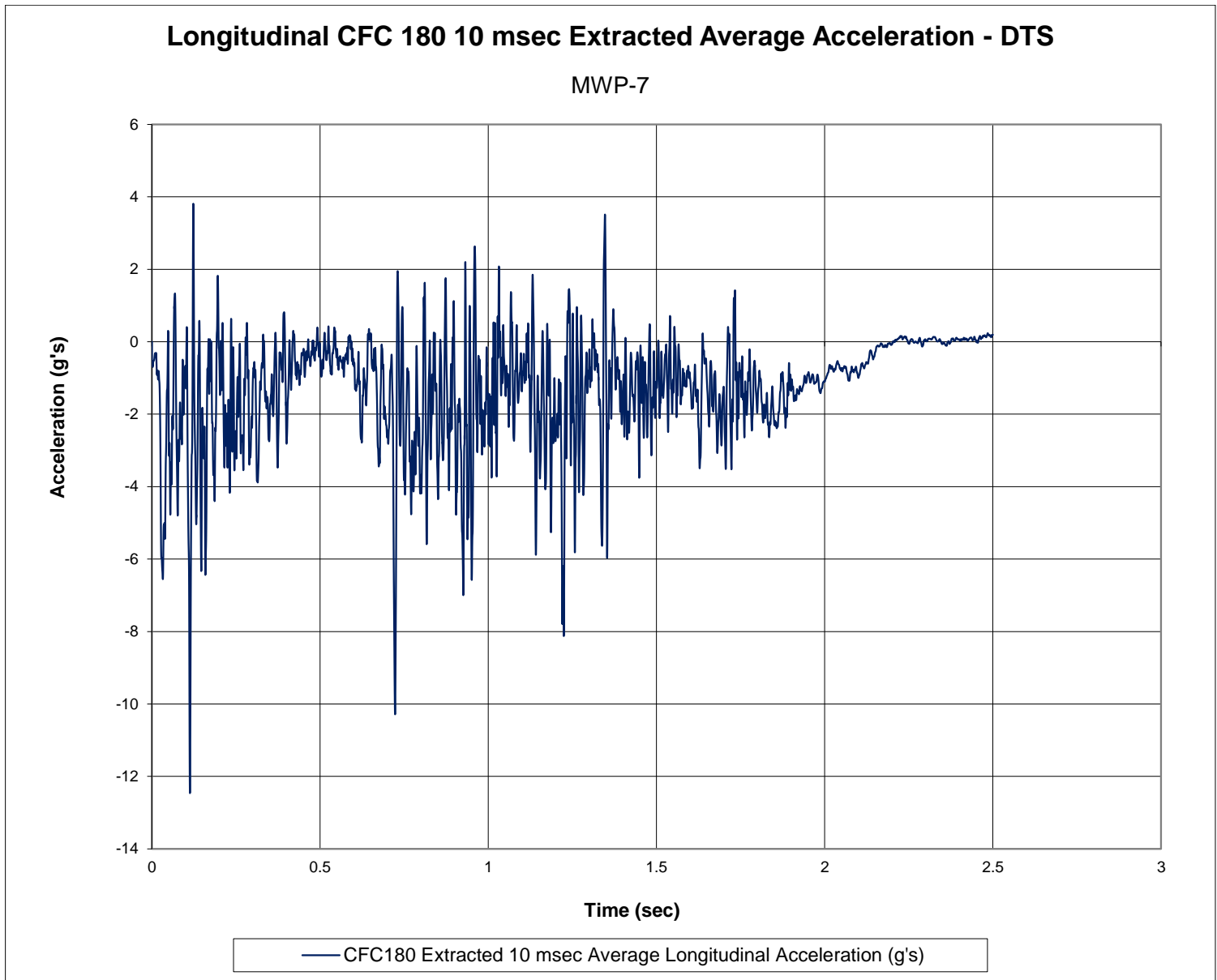


Figure I-1. 10-ms Average Longitudinal Deceleration (SLICE 1), Test No. MWP-7

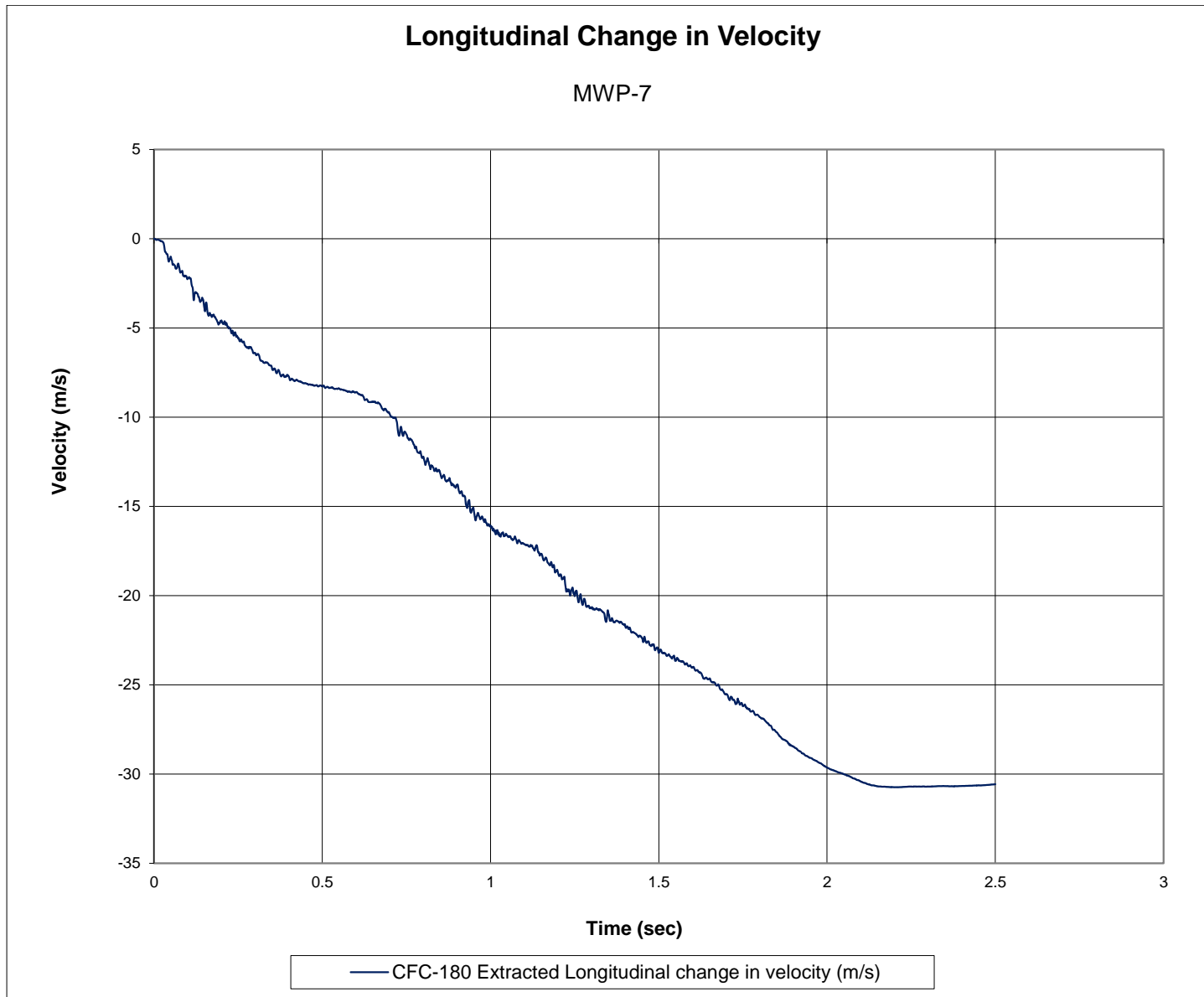


Figure I-2. Longitudinal Occupant Impact Velocity (SLICE 1), Test No. MWP-7

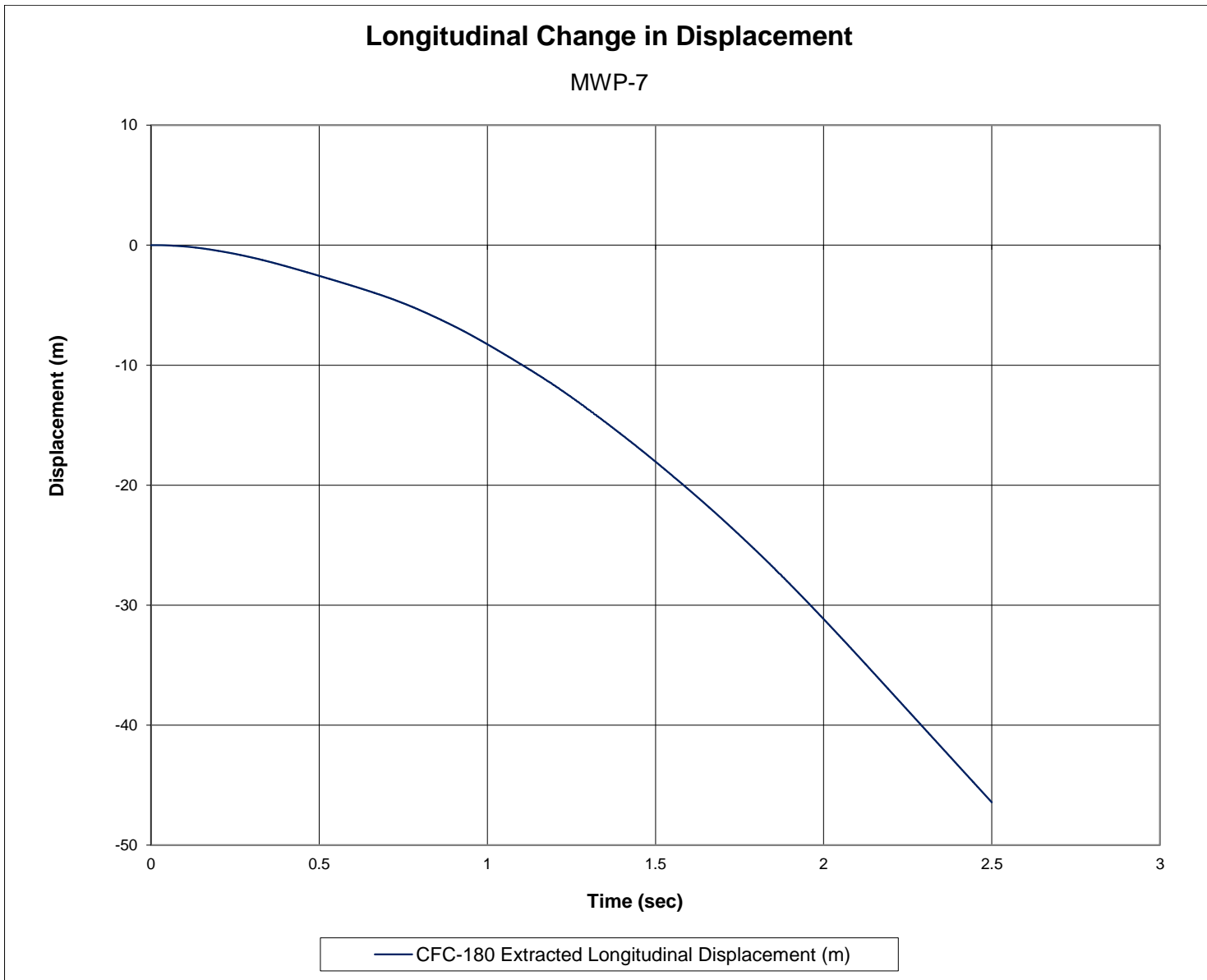


Figure I-3. Longitudinal Occupant Displacement (SLICE 1), Test No. MWP-7

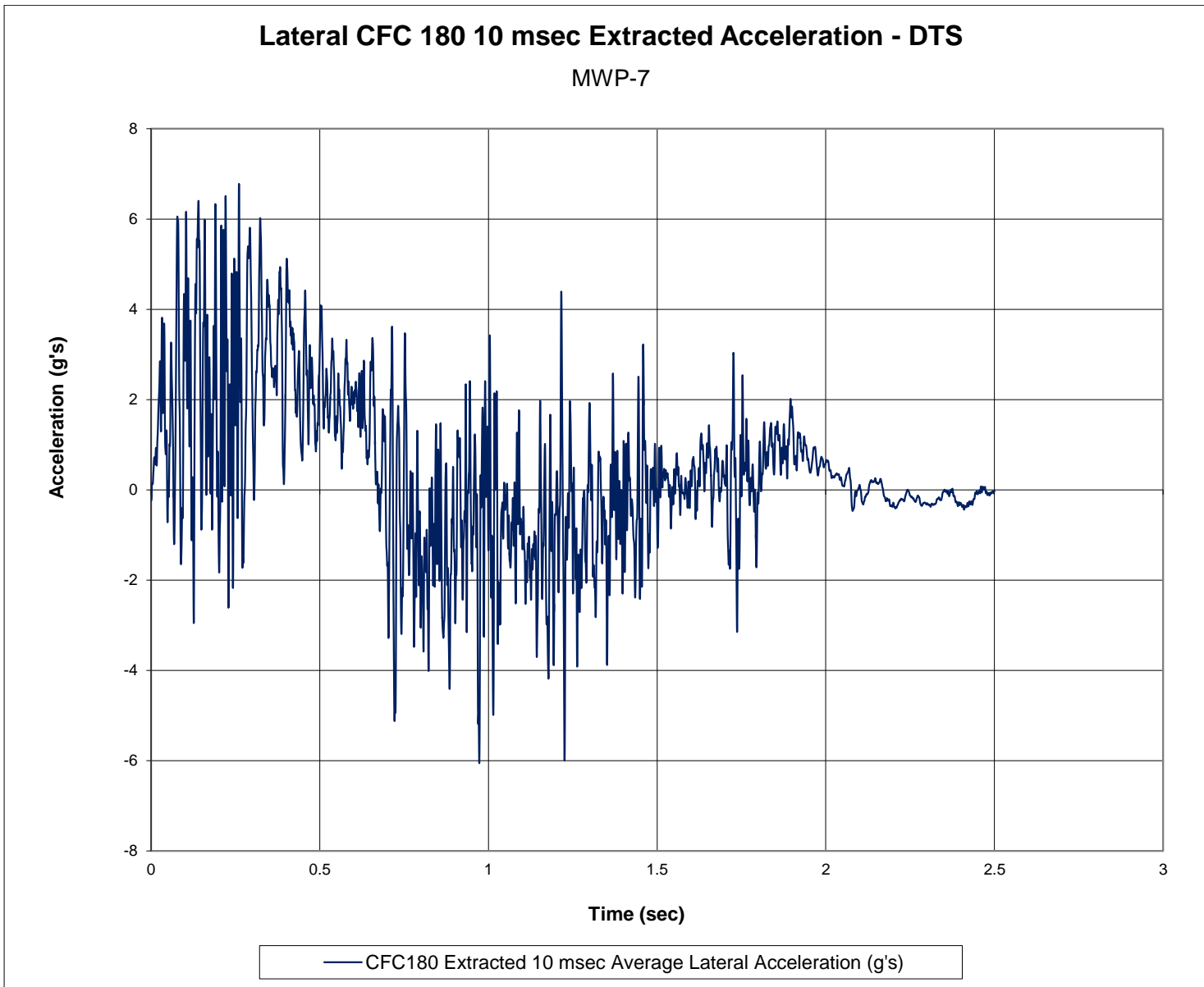


Figure I-4. 10-ms Average Lateral Deceleration (SLICE 1), Test No. MWP-7

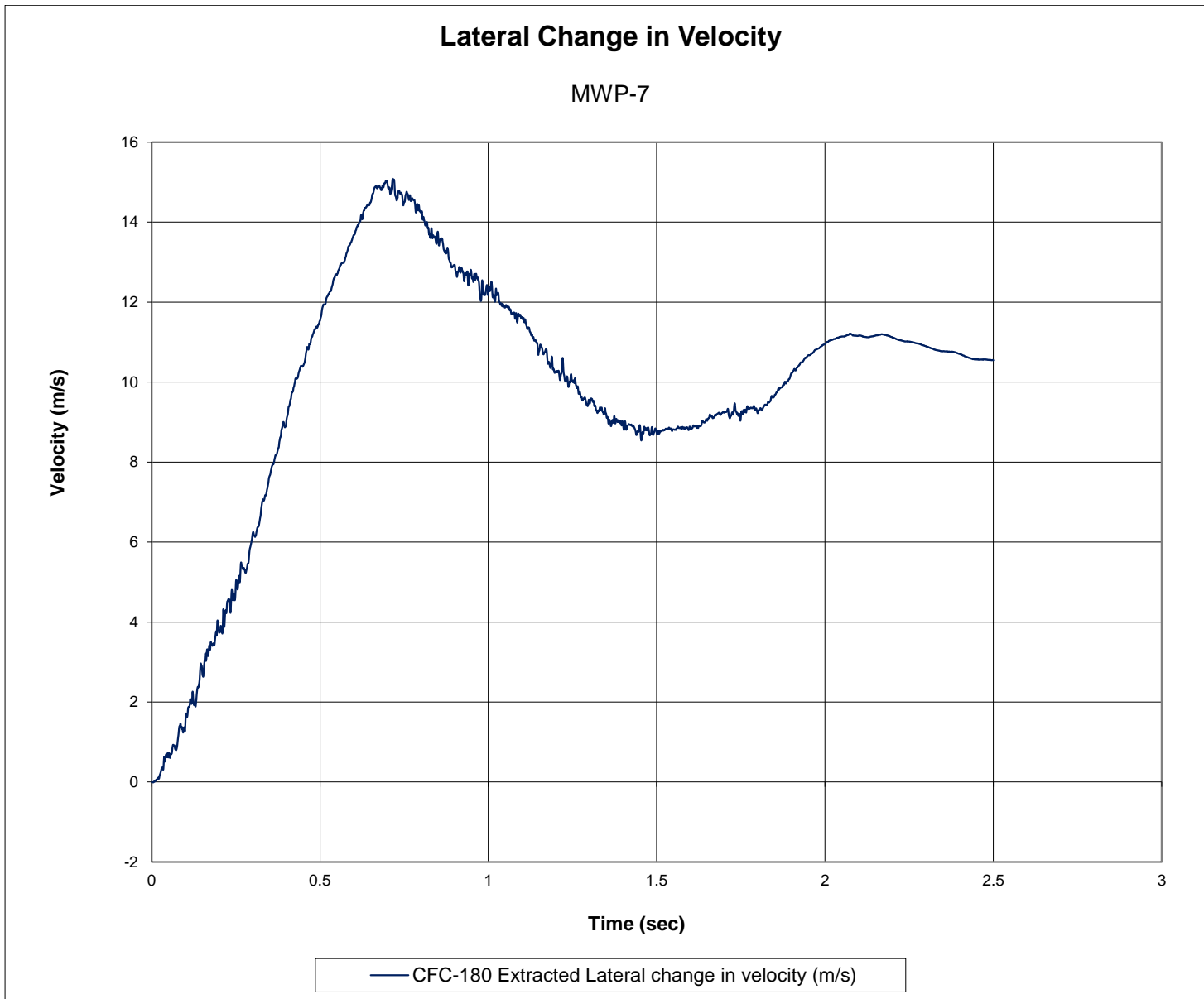


Figure I-5. Lateral Occupant Impact Velocity (SLICE 1), Test No. MWP-7

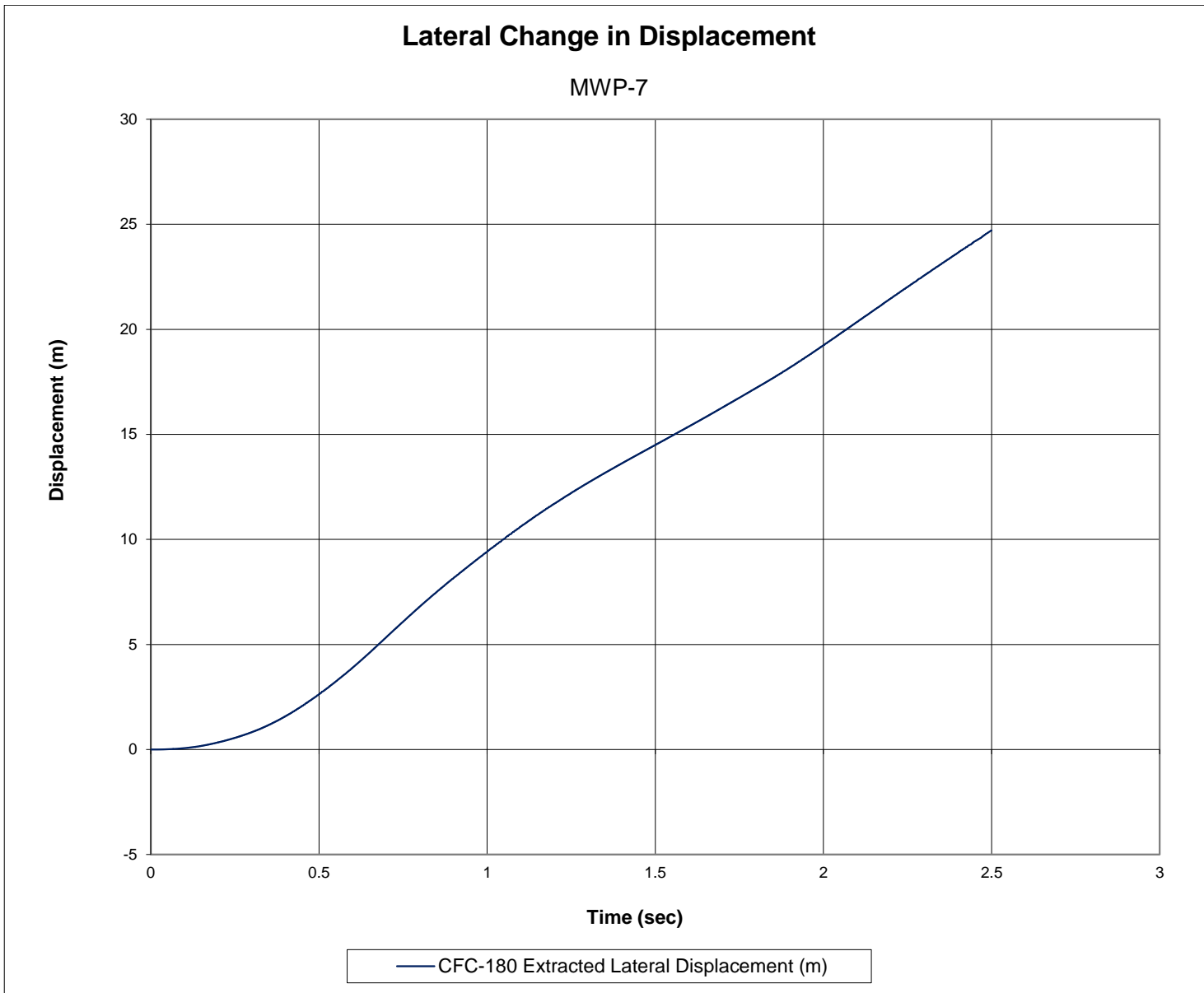


Figure I-6. Lateral Occupant Displacement (SLICE 1), Test No. MWP-7

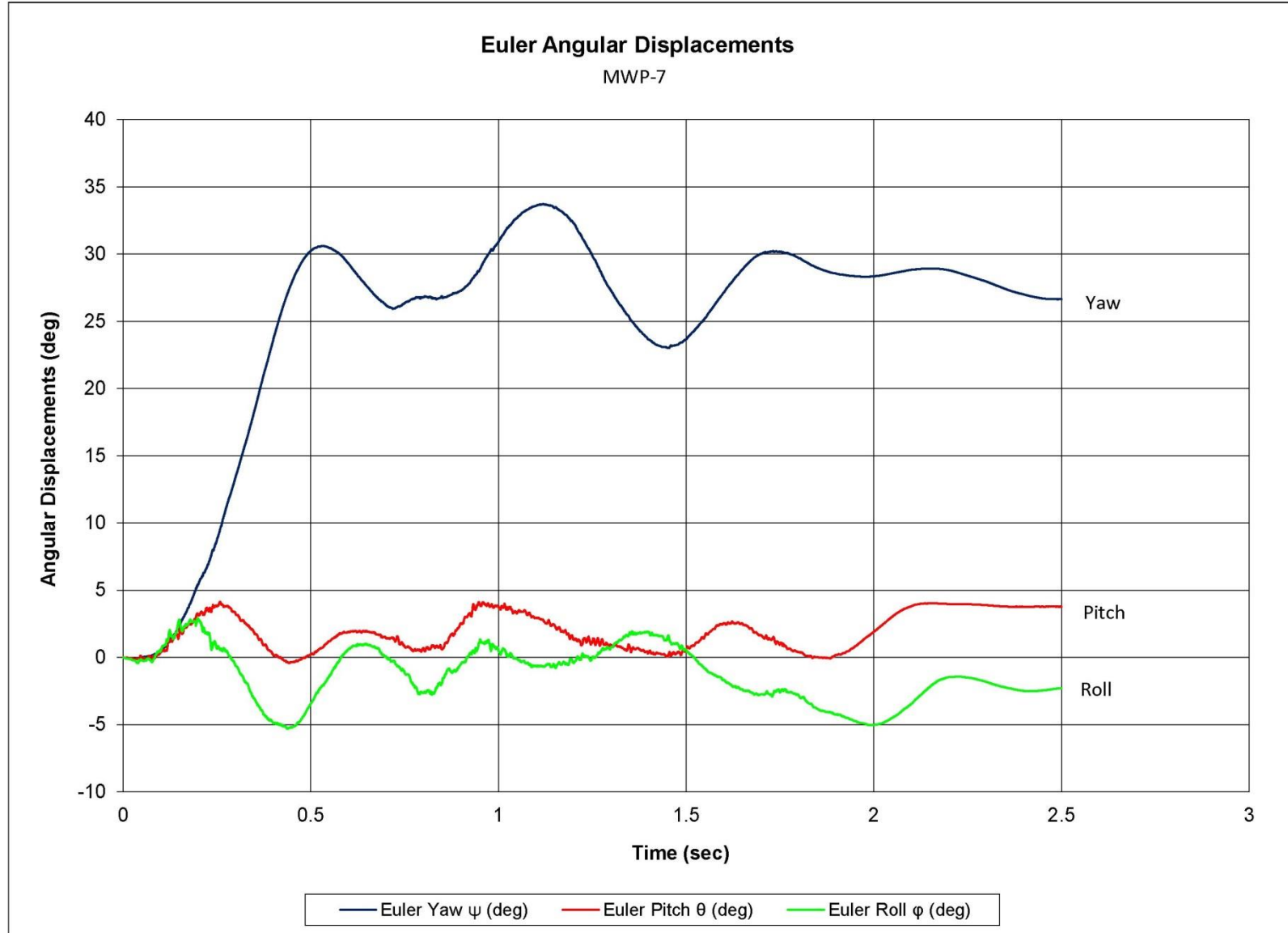


Figure I-7. Vehicle Angular Displacements (SLICE 1), Test No. MWP-7

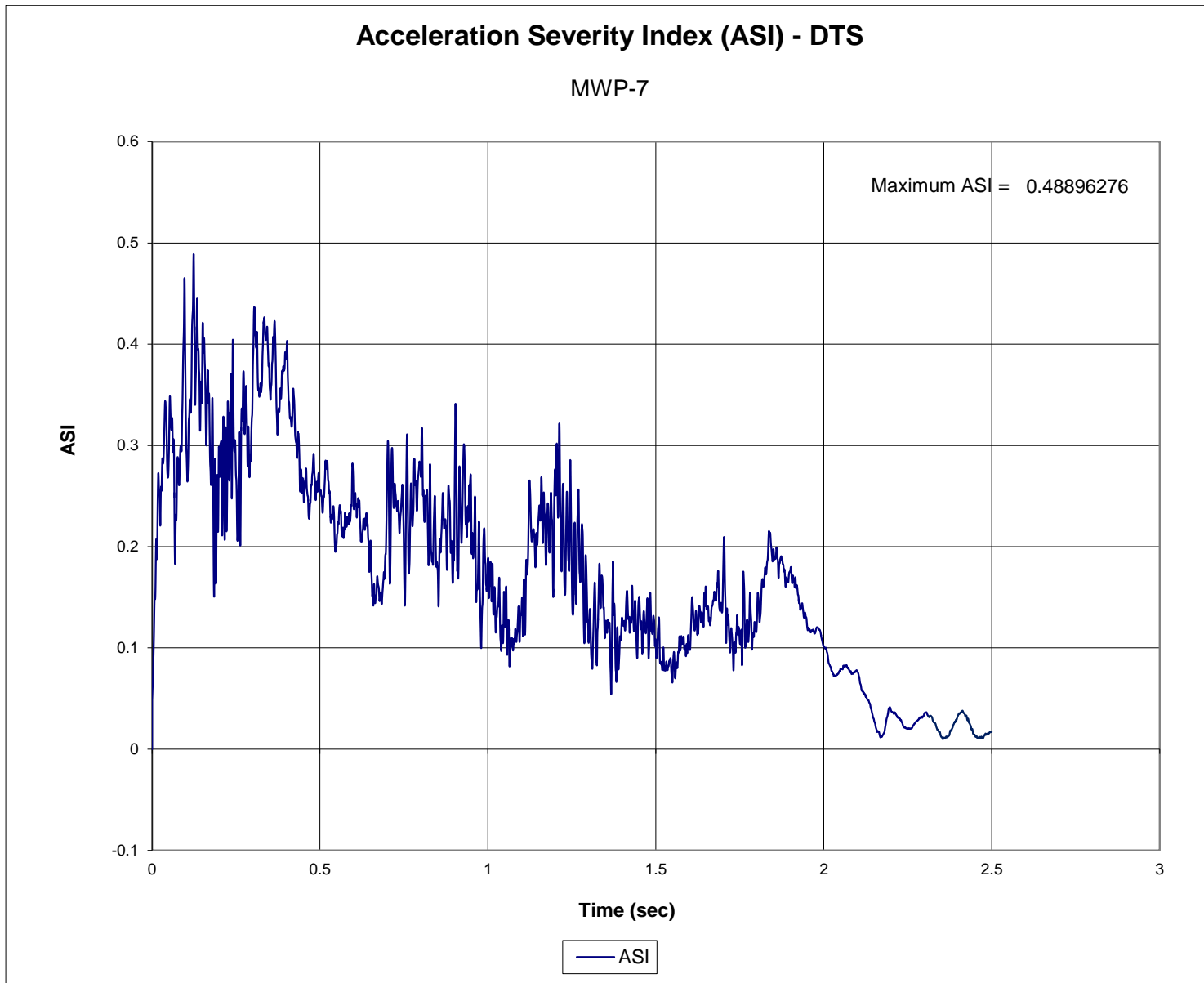


Figure I-8. Acceleration Severity Index (SLICE 1), Test No. MWP-7

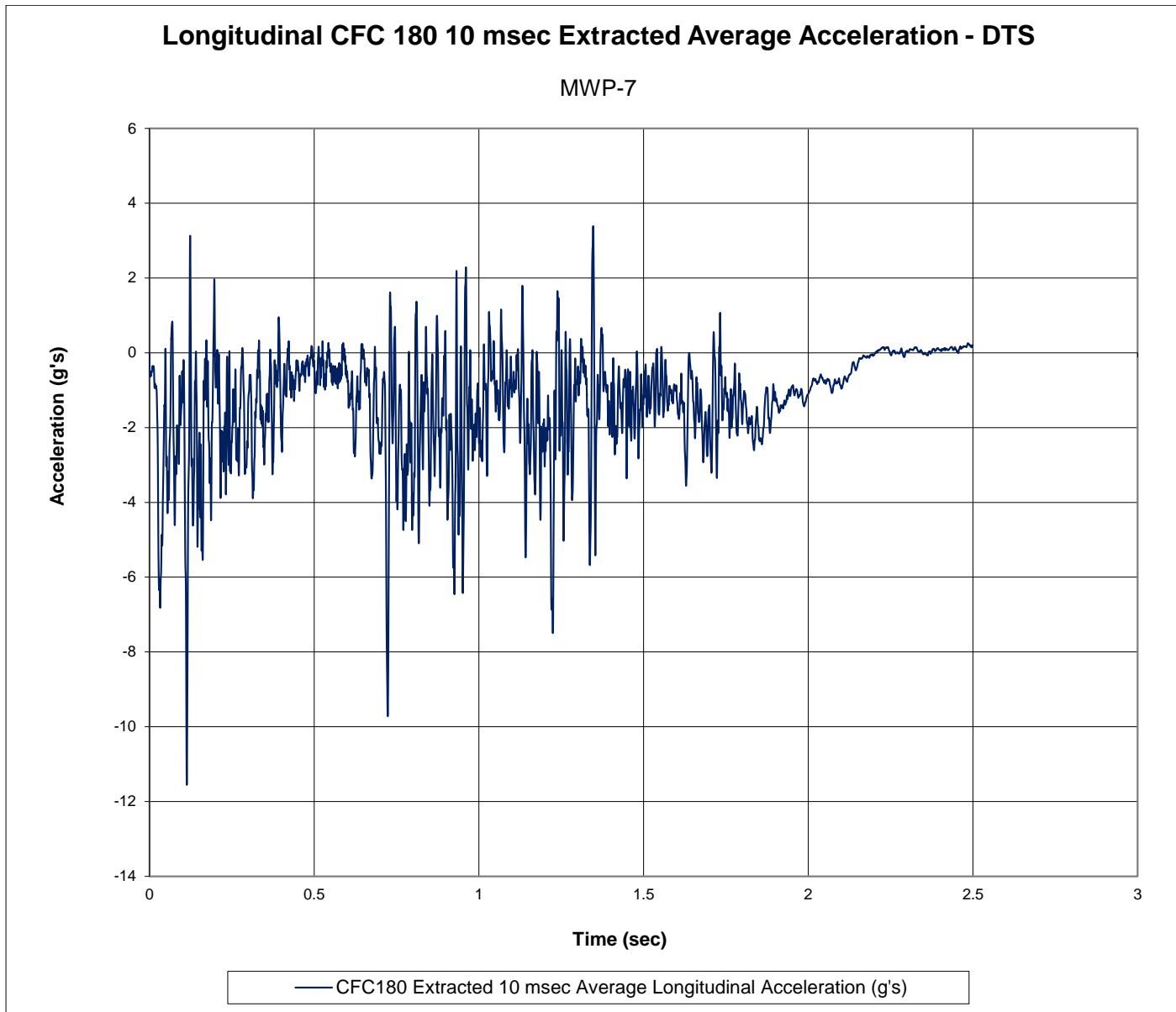


Figure I-9. 10-ms Average Longitudinal Deceleration (SLICE 2), Test No. MWP-7

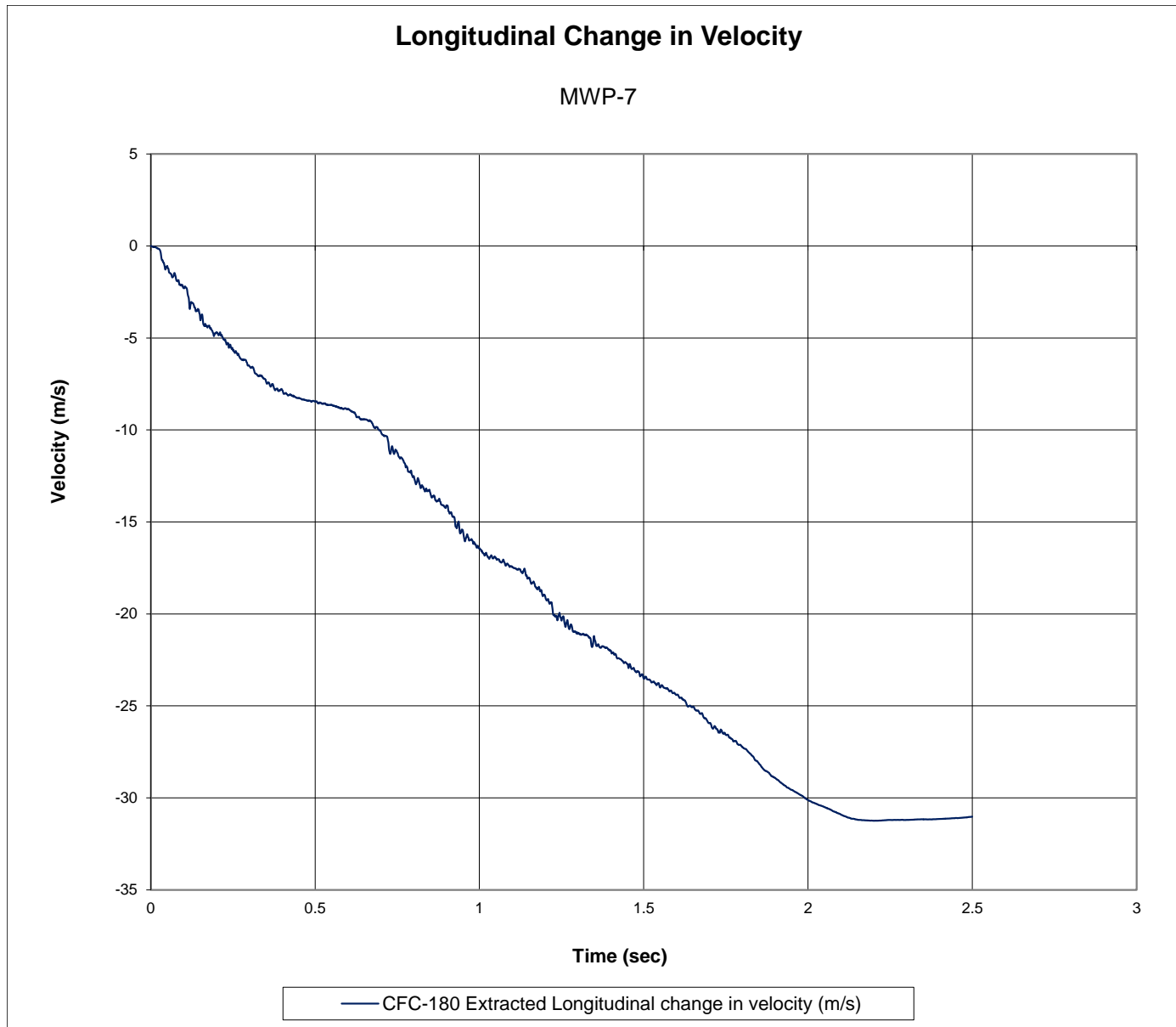


Figure I-10. Longitudinal Occupant Impact Velocity (SLICE 2), Test No. MWP-7

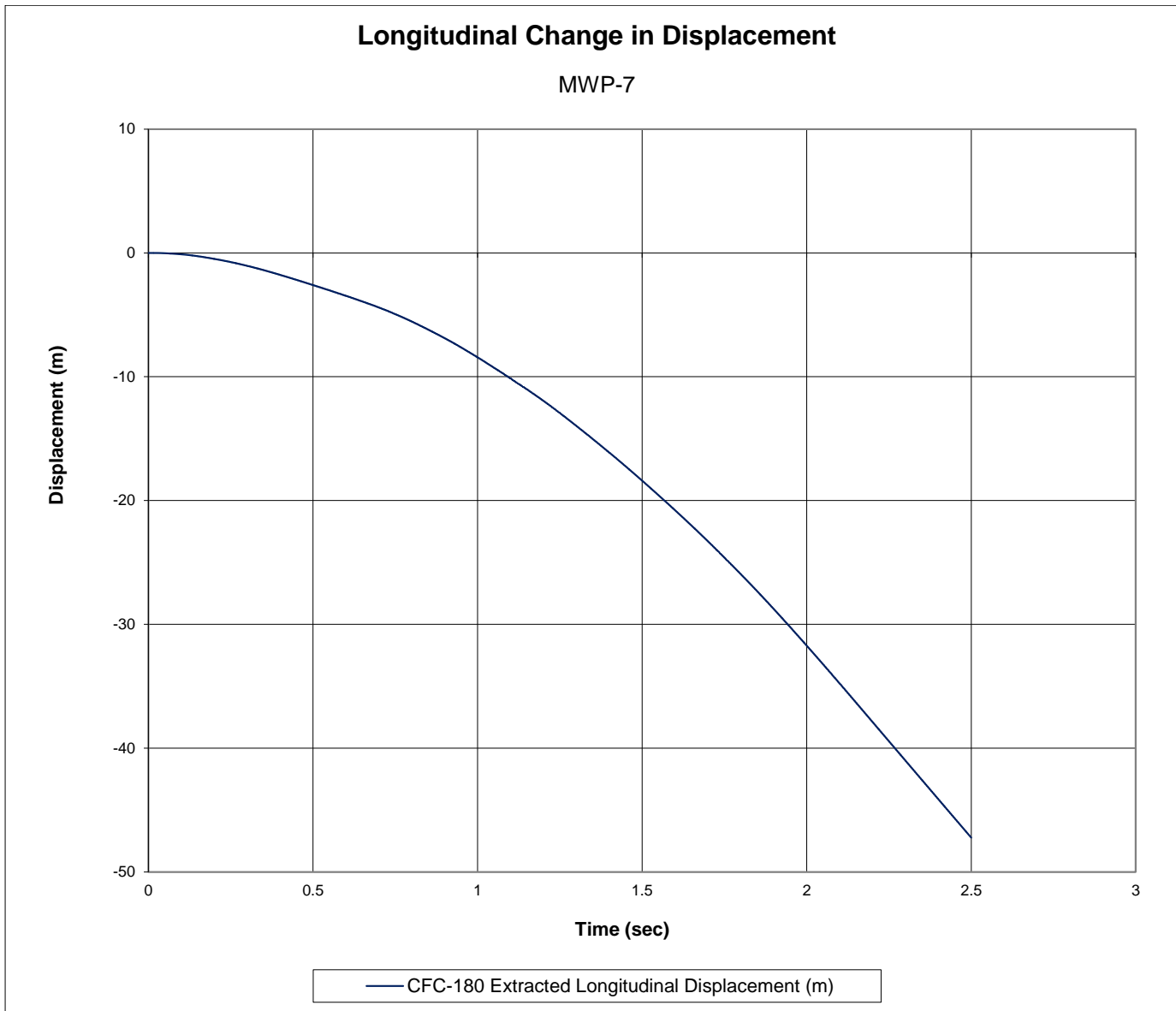


Figure I-11. Longitudinal Occupant Displacement (SLICE 2), Test No. MWP-7

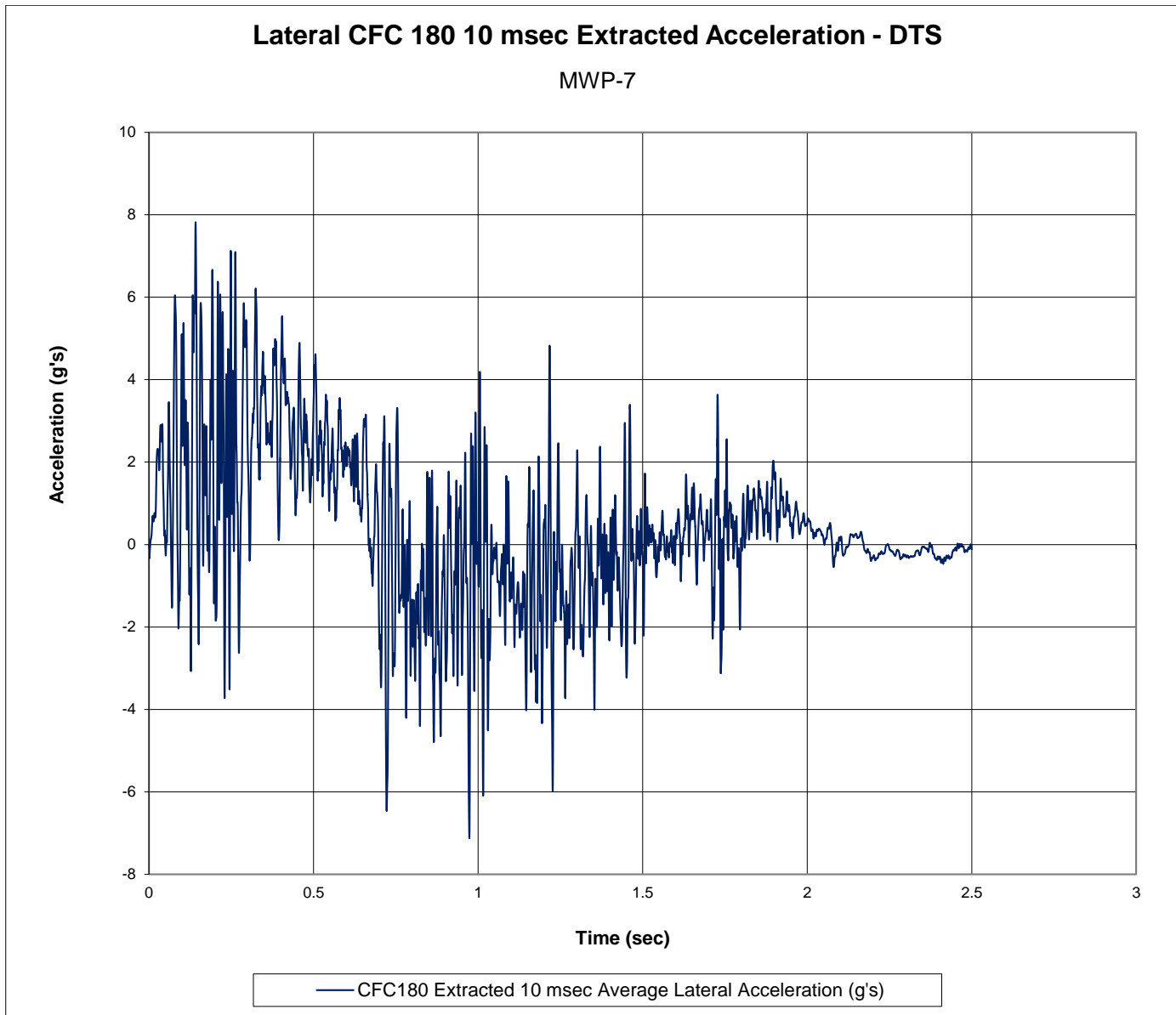


Figure I-12. 10-ms Average Lateral Deceleration (SLICE 2), Test No. MWP-7

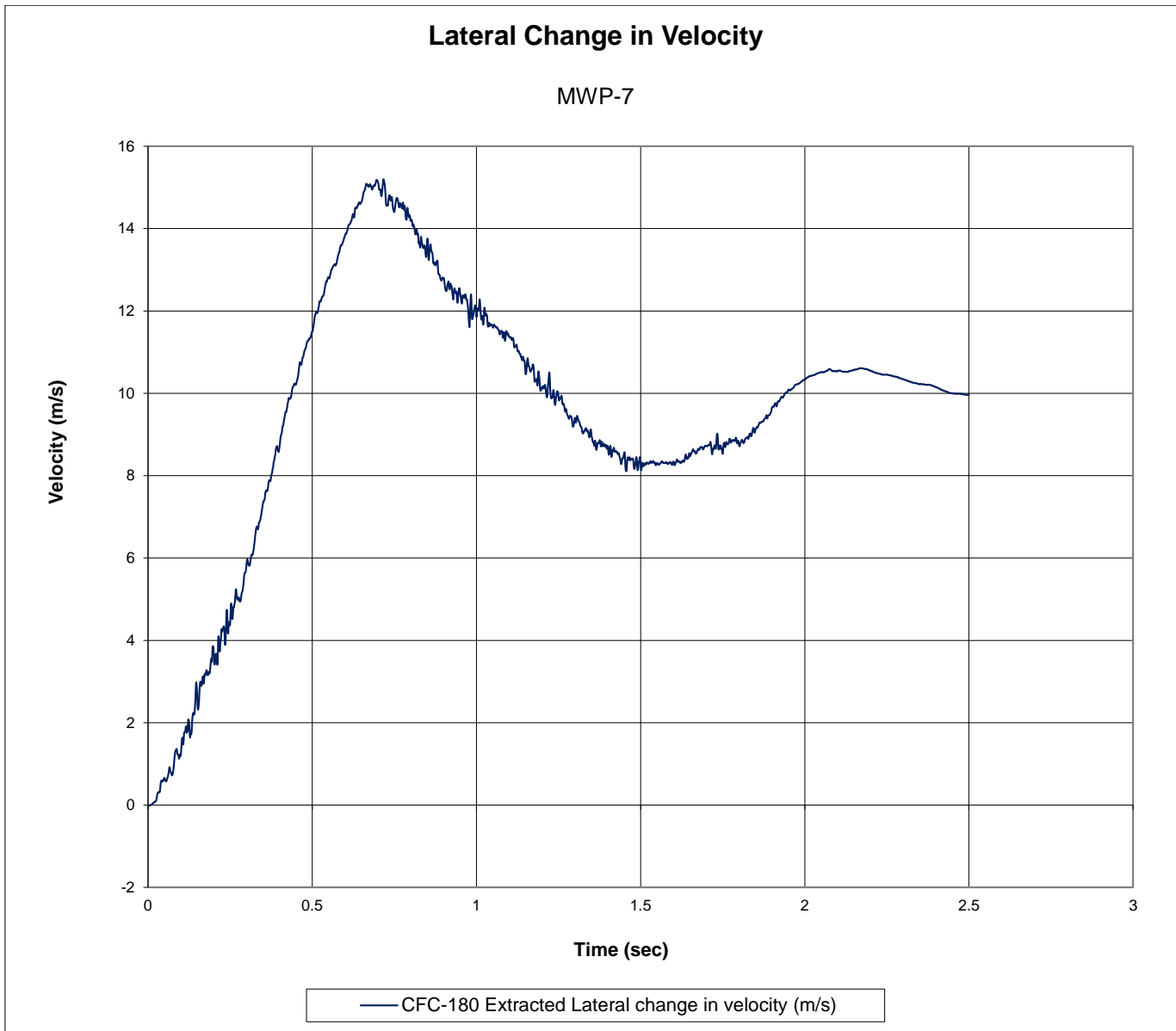


Figure I-13. Lateral Occupant Impact Velocity (SLICE 2), Test No. MWP-7

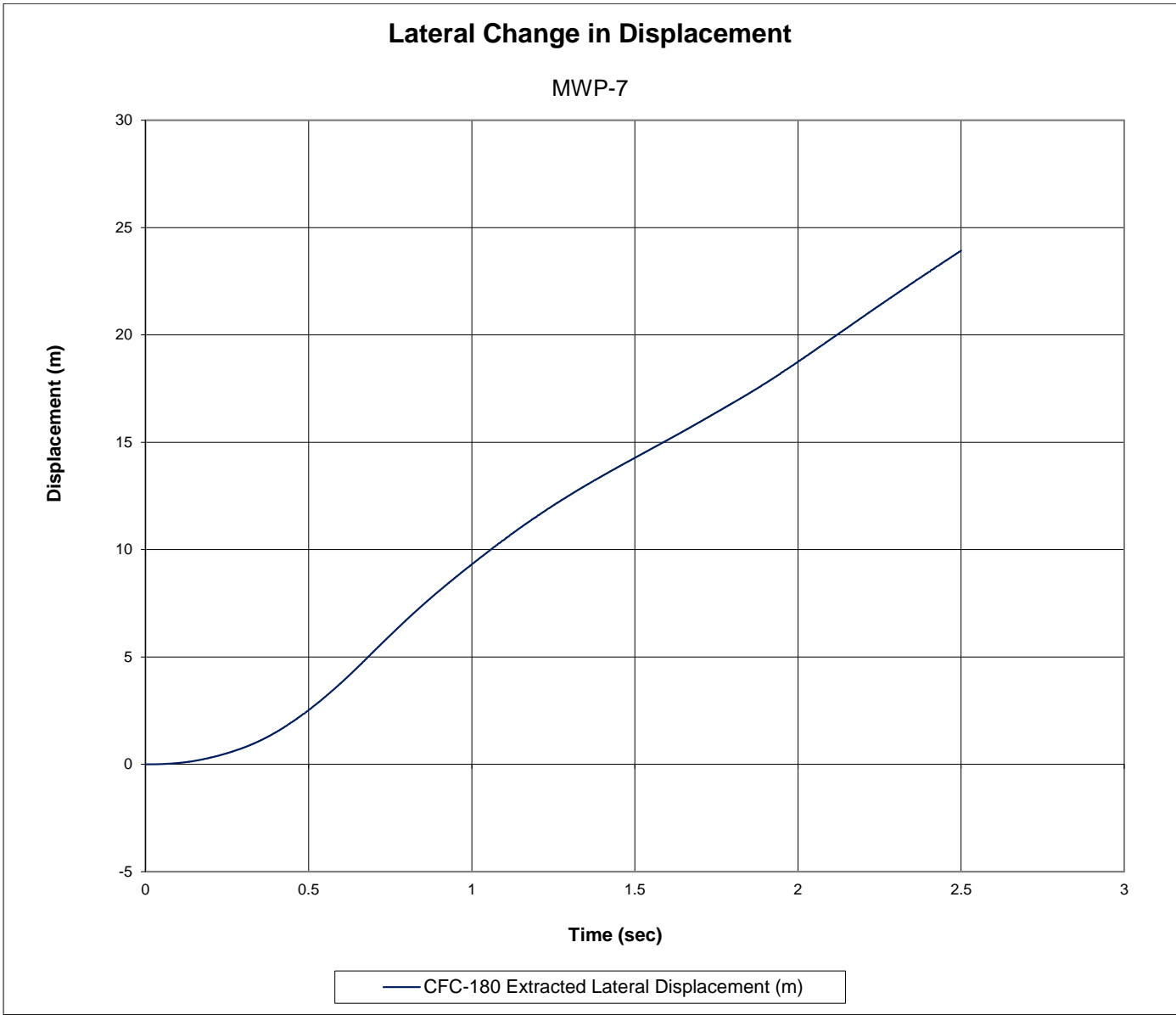


Figure I-14. Lateral Occupant Displacement (SLICE 2), Test No. MWP-7



Figure I-15. Vehicle Angular Displacements (SLICE 2), Test No. MWP-7

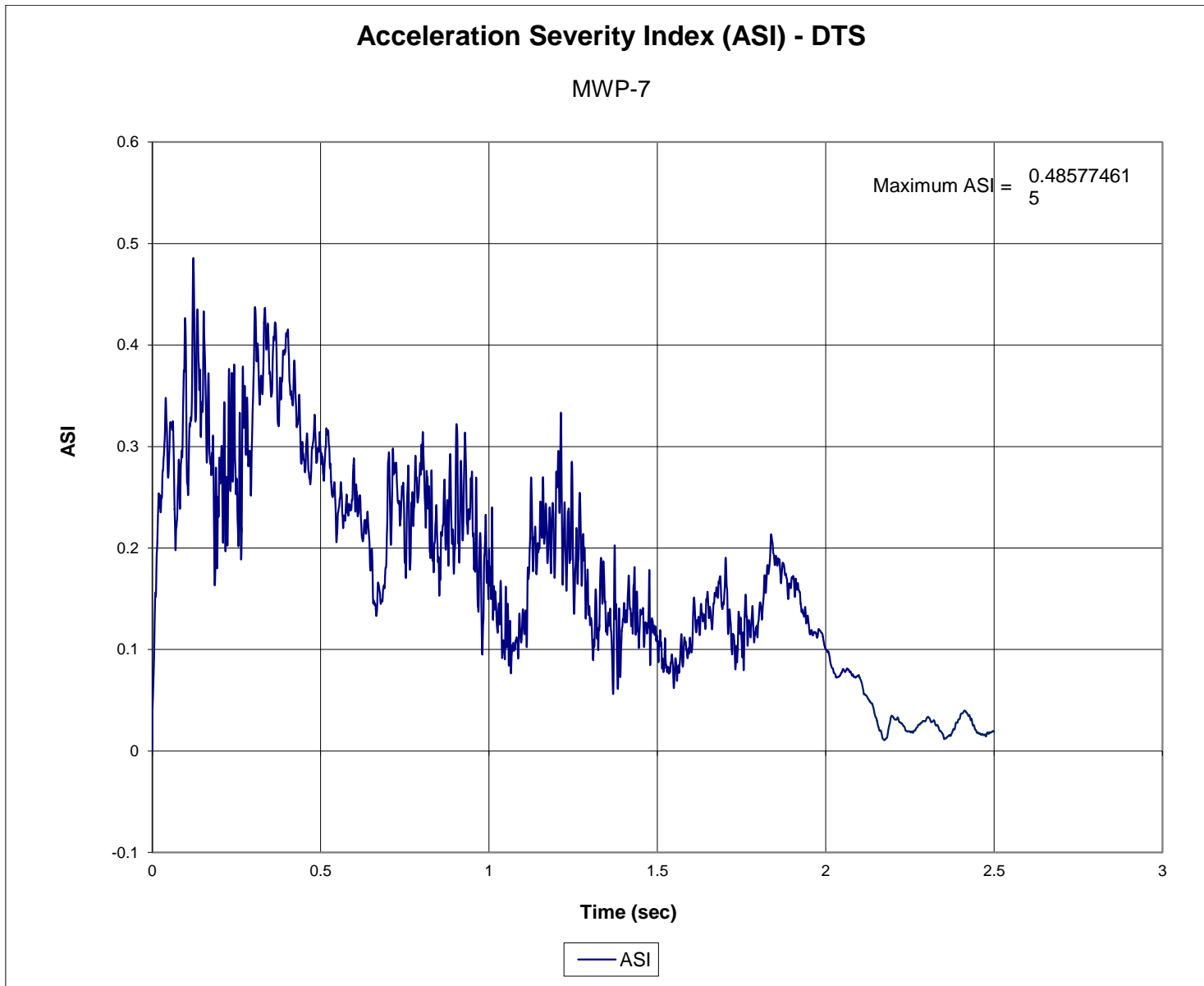


Figure I-16. Acceleration Severity Index (SLICE 2), Test No. MWP-7

Appendix J. Load Cell and String Potentiometer Data, Test No. MWP-7

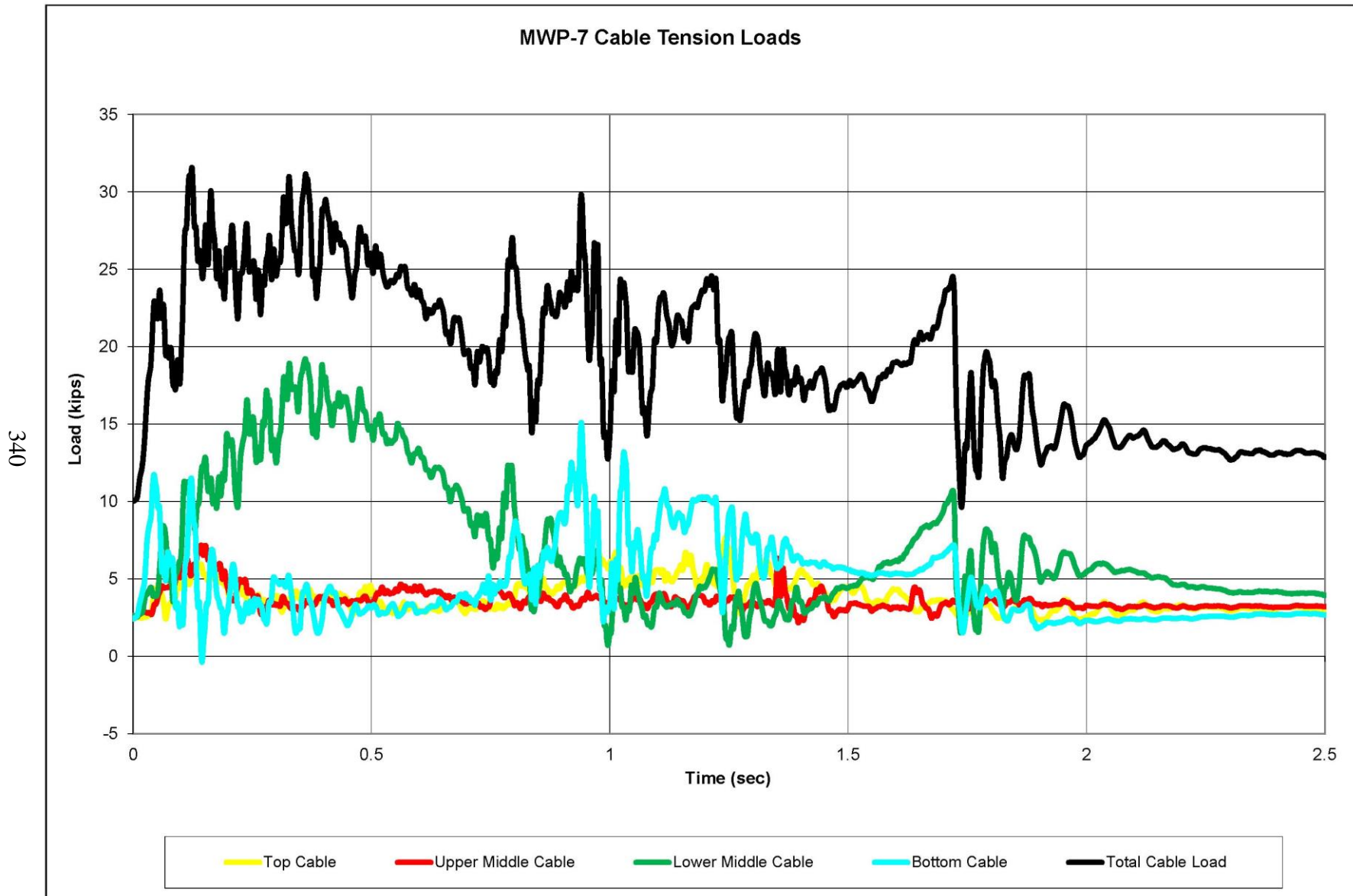


Figure J-1. Combined Load Cell Data, Test No. MWP-7

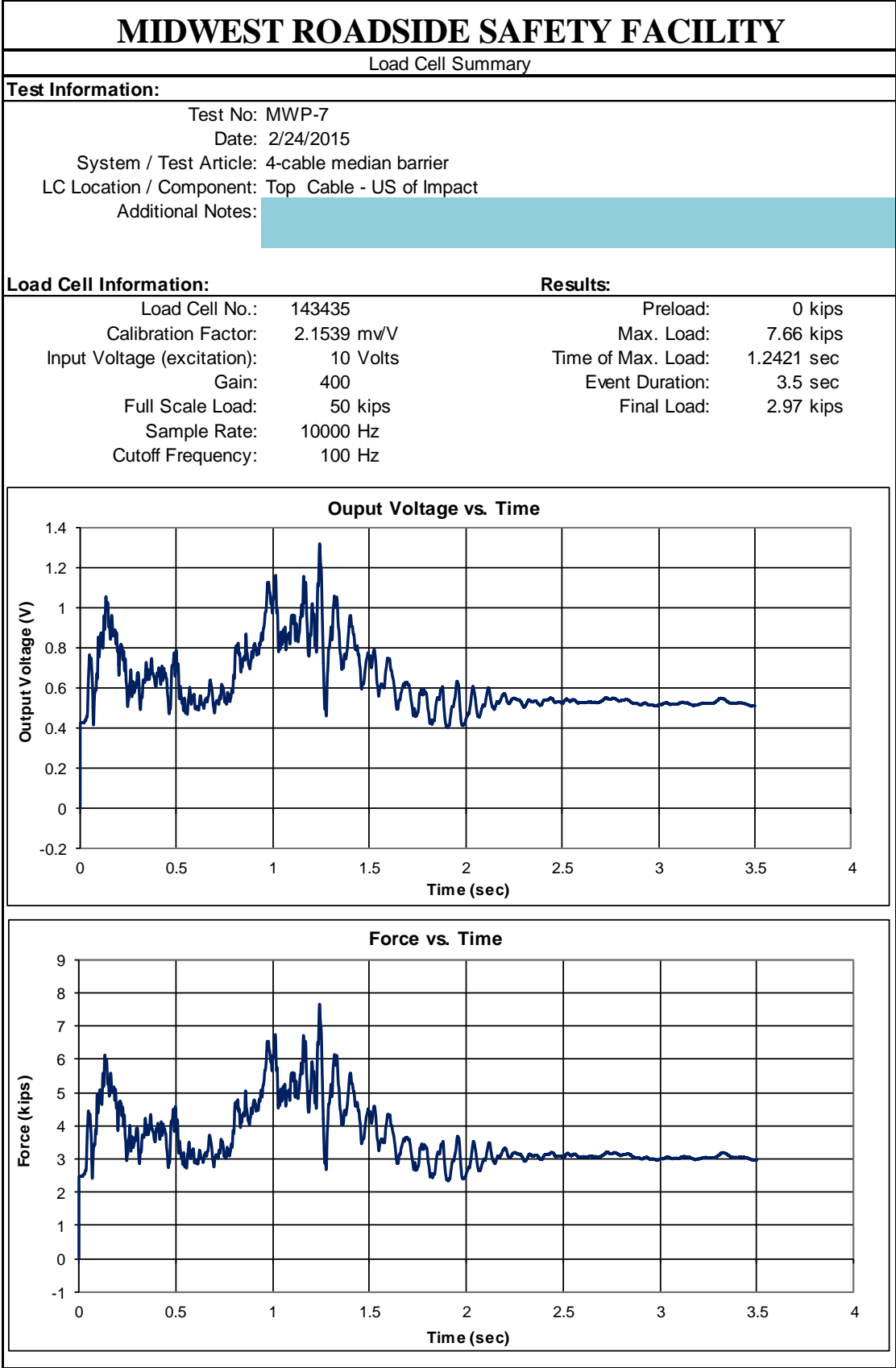


Figure J-2. Load Cell Data, Cable No. 4, Test No. MWP-7

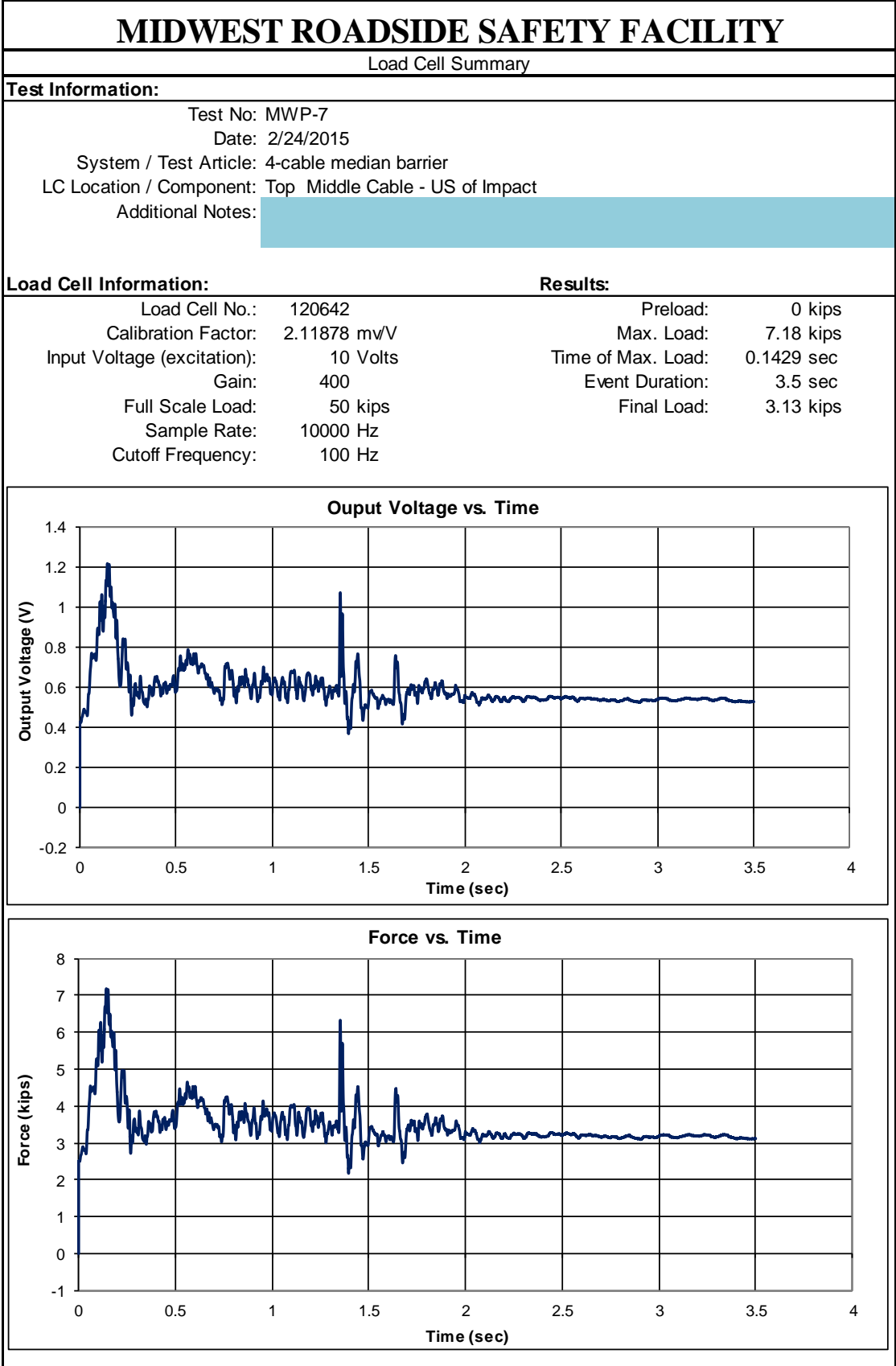


Figure J-3. Load Cell Data, Cable No. 3, Test No. MWP-7

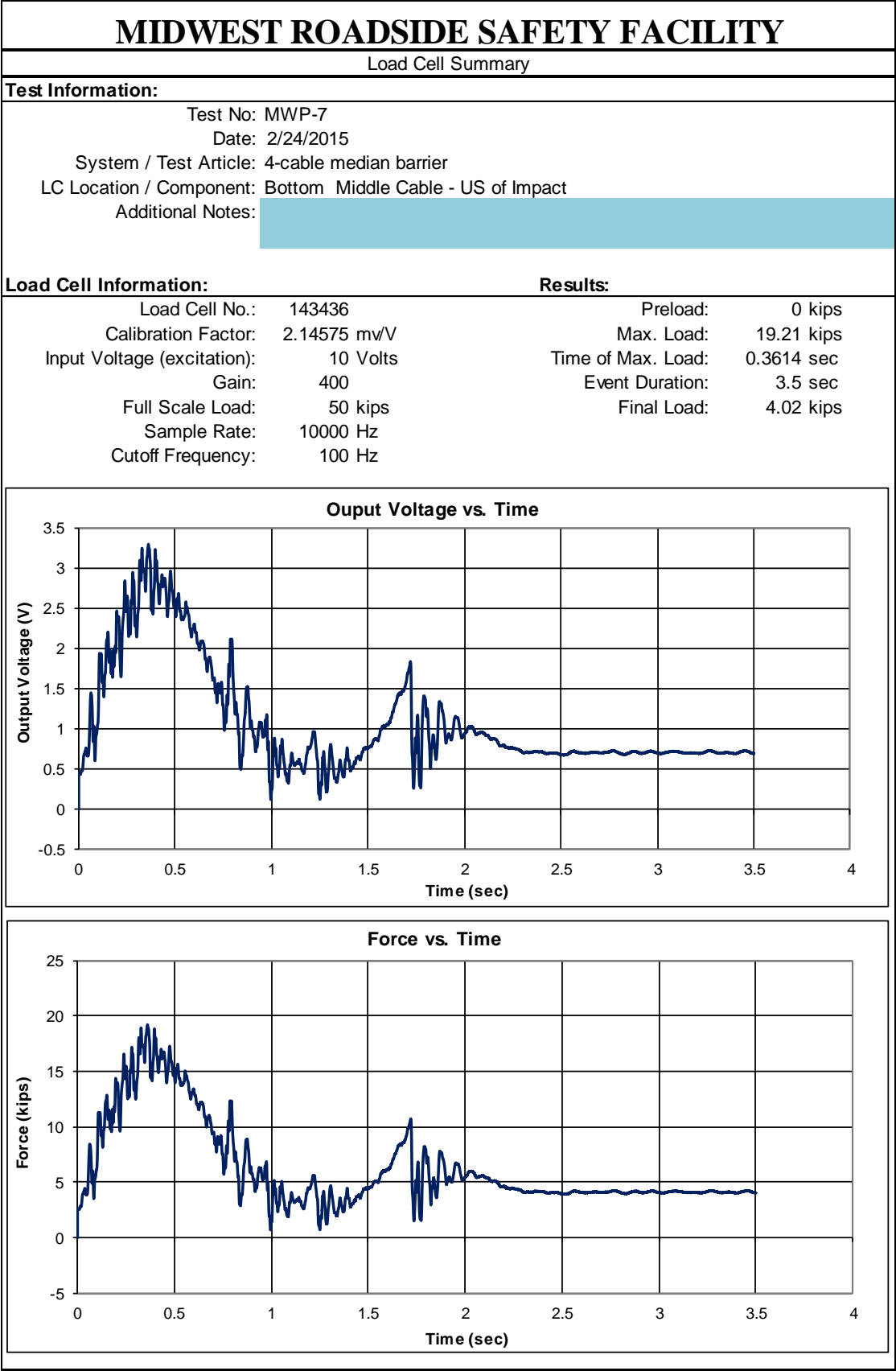


Figure J-4. Load Cell Data, Cable No. 2, Test No. MWP-7

MIDWEST ROADSIDE SAFETY FACILITY

Load Cell Summary

Test Information:

Test No: MWP-7
Date: 2/24/2015
System / Test Article: 4-cable median barrier
LC Location / Component: Bottom Cable - US of Impact
Additional Notes:

Load Cell Information:

Load Cell No.: 241593
Calibration Factor: 2.14857 mV/V
Input Voltage (excitation): 10 Volts
Gain: 400
Full Scale Load: 50 kips
Sample Rate: 10000 Hz
Cutoff Frequency: 100 Hz

Results:

Preload: 0 kips
Max. Load: 15.10 kips
Time of Max. Load: 0.9403 sec
Event Duration: 3.5 sec
Final Load: 2.66 kips

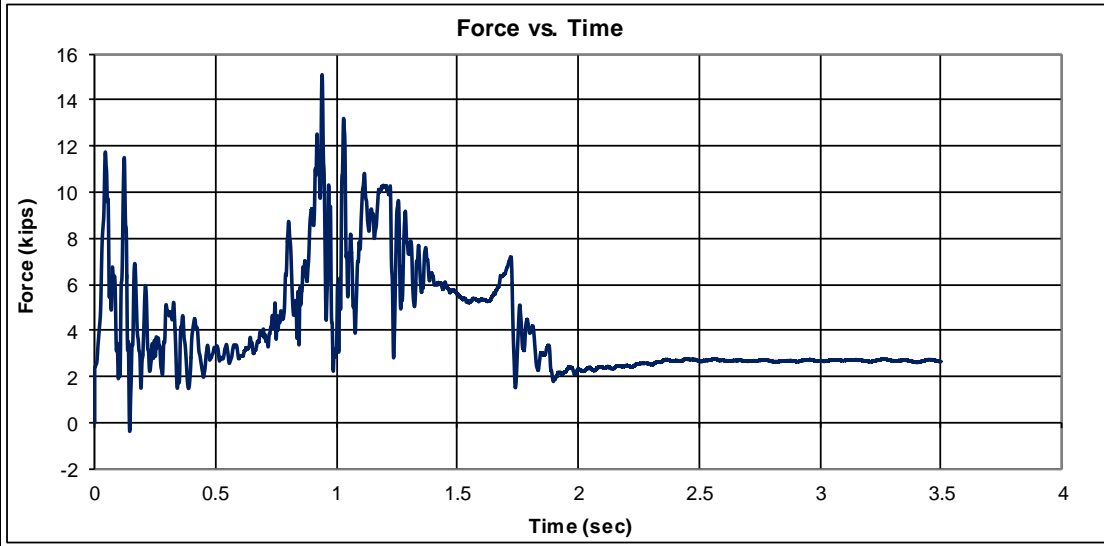
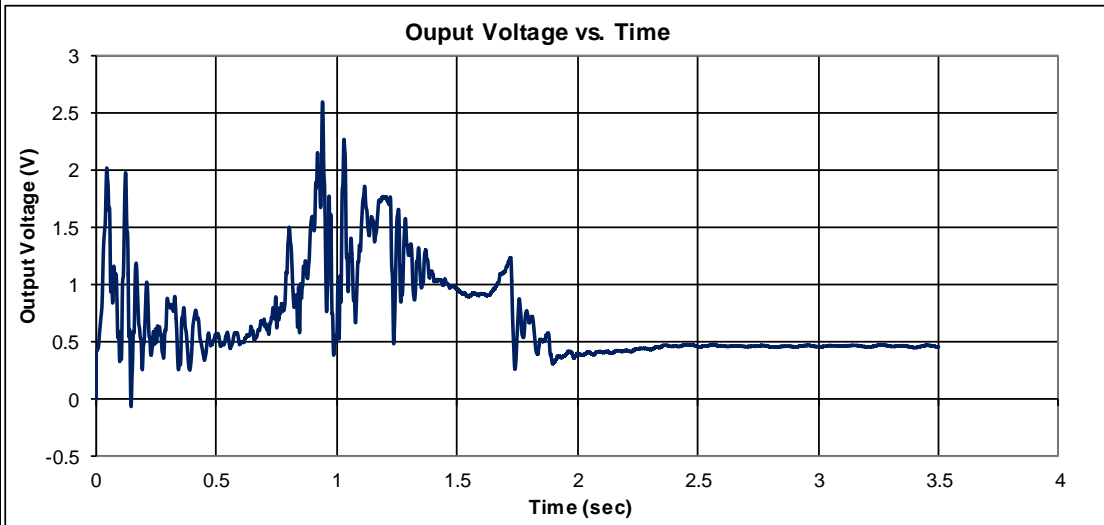


Figure J-5. Load Cell Data, Cable No. 1, Test No. MWP-7

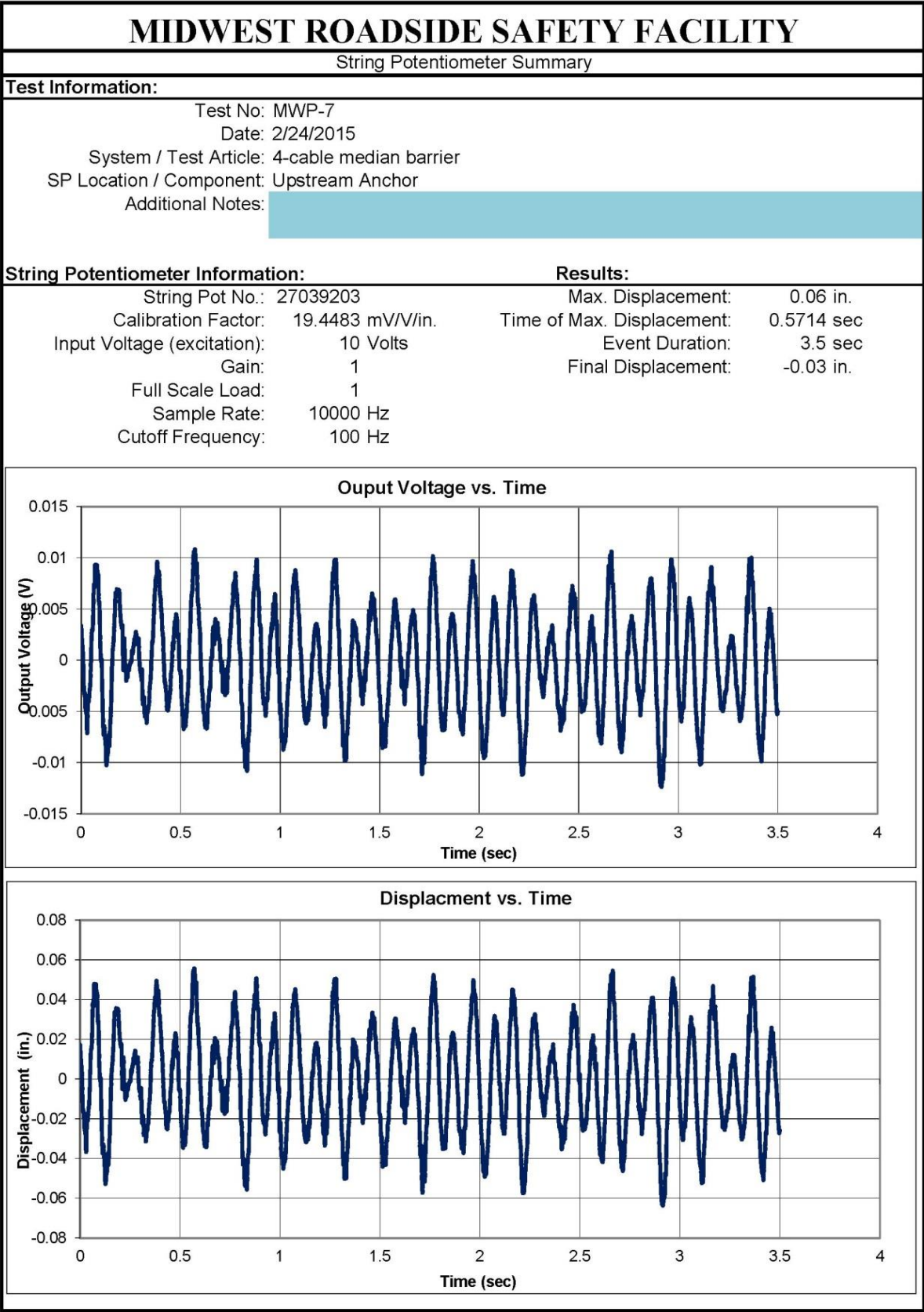


Figure J-6. String Potentiometer Data, Test No. MWP-7

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